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MAXIMIZATION OF ENERGY IN THE OUTPUT OF A LINEAR SYSTEM

D. G. Dudley

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Foreword

D. G. Dudley prepared this report while working as a summer (1971) employee with the Electromagnetic and Systems Research Group of the Electronic's Engineering Department. The work was supported by the Defense Nuclear Agency. Dudley is a professor of electrical engineering at the University of Arizona, Tucson.

MAXIMIZATION OF ENERGY IN THE OUTPUT OF A LINEAR SYSTEM

Abstract

In this report, we consider a time-limited signal which, when passed through a linear system, maximizes the total output energy. Previous work has shown that the solution is given by the eigenfunction associated with the maximum eigenvalue in a Hilbert-Schmidt integral equation. Analytical results are available for the case where the transfer function is a low-pass filter. This work is extended by obtaining a numerical solution to the integral equation which allows results for reasonably general transfer functions.

Introduction

Consider a linear system with input $f(t)$ and output $g(t)$. For $f(t)$ time-limited $[-T, T]$ and of specified energy, Chalk¹ has shown that the total energy in the output is maximized through a consideration of the linear integral equation

$$\lambda f(t) = \int_{-T}^T f(\tau) K(t - \tau) d\tau. \quad (1)$$

The "optimal" $f(t)$ is that particular eigenfunction $f(t)$ associated with the maximum eigenvalue λ_1 obtained in the solution to Eq. (1). Chalk has obtained an analytical solution to Eq. (1) for the case where the transfer function $H(\omega)$ is the first-order Butterworth low-pass filter

$$H(\omega) = \frac{\alpha}{\alpha + i\omega}. \quad (2)$$

Chalk also gives approximate solutions for the case where the transfer function is an ideal low-pass filter

$$H(\omega) = \begin{cases} 1 & |\omega| < \omega_0 \\ 0 & |\omega| > \omega_0 \end{cases} . \quad (3)$$

Slepian and Pollak² have extended the results by noting that for the case of the ideal low-pass filter, Eq. (1) defines certain of the angular prolate spheroidal functions,³ a fact which allows for expression of the ideal low-pass filter results in terms of known functions.

In this report, we take a different point of view, abandoning the search for further analytical solutions in favor of obtaining an efficient numerical solution to Eq. (1). Our reason is that our application is in electromagnetics where the transfer function is often known only in terms of discrete experimental data or discrete data from numerical solutions to the electromagnetic boundary value problem. The results herein are reasonably complete in one sense and only preliminary in another. We have produced an efficient numerical technique for the reduction of Eq. (1) and have compared the results favorably both with Chalk and with Slepian and Pollak. In addition we have produced optimum pulses for the important case of a single-resonance transfer function. On the other hand, the numerical technique affords access to a large range of transfer functions which we have not begun to consider and in this sense the results are only preliminary. We make some specific comments concerning this later in the report.

Background

Let the energy in the input $f(t)$ to a linear system be given by

$$E_I = \int_{-T}^T f^2(t) dt . \quad (4)$$

Let the energy in the output $g(t)$ be given by

$$E_O = \int_{-\infty}^{\infty} g^2(t) dt . \quad (5)$$

By Parseval's theorem,⁴ this result may be given in terms of the frequency spectrum of the output $G(\omega)$, viz:

$$E_0 = \frac{1}{2\pi} \int_{-\infty}^{\infty} |G(\omega)|^2 d\omega, \quad (6)$$

If $F(\omega)$ is the frequency spectrum of the input and $H(\omega)$ the system transfer function,

$$E_0 = \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(\omega) H(\omega)|^2 d\omega, \quad (7)$$

or, in terms of the Fourier transforms of F and F^* ,

$$E_0 = \frac{1}{2\pi} \int_{-\infty}^{\infty} |H(\omega)|^2 \int_{-T}^T f(\tau) e^{-i\omega\tau} d\tau \int_{-T}^T f(s) e^{i\omega x} dx d\omega. \quad (8)$$

An interchange of integration produces the result

$$E_0 = \int_{-T}^T \int_{-T}^T f(\tau) f(x) K(x - \tau) dx d\tau, \quad (9)$$

where

$$K(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} |H(\omega)|^2 e^{i\omega t} d\omega. \quad (10)$$

We wish to find an $f_1(t)$, optimum in the sense that it maximizes the double integral in Eq. (9), subject to the constraint in Eq. (4). This problem is classic in the calculus of variations (see Appendix A) and has the following solution. The function $f_1(t)$ must satisfy the integral equation given by Eq. (1). Specifically,

$$\lambda_1 f_1(t) = \int_{-T}^T f_1(\tau) K(t - \tau) d\tau, \quad (11)$$

where f_1 is the eigenfunction corresponding to the maximum eigenvalue λ_1 . Substitution of Eq. (11) into Eq. (9) yields

$$E_0 = \lambda_1 E_1. \quad (12)$$

A final comment is in order concerning the properties of the solutions to Eq. (1). We note that the expression for the kernel function in Eq. (10) may be written

$$K(t) = \frac{1}{\pi} \int_0^{\infty} |H(\omega)|^2 \cos \omega t \, d\omega, \quad (13)$$

where we have used the even property of $|H(\omega)|^2$. We therefore conclude that the kernel is symmetric, viz:

$$K(t) = K(-t). \quad (14)$$

The result is that the eigenfunctions obtained in the solution to Eq. (1) are orthogonal and corresponding eigenvalues are real.⁵ In addition,

$$\lambda_1 > \lambda_2 > \lambda_3 > \dots \quad (15)$$

so that we may legitimately seek the maximum eigenvalue.

Normalization of Results

In order to produce a convenient normalization of the results to follow, we consider the all-pass transfer function

$$|H(\omega)| = 1. \quad (16)$$

From the Fourier transform pair

$$\delta(t) \longleftrightarrow 1, \quad (17)$$

we obtain in Eq. (1)

$$\lambda f(t) = \int_{-T}^T f(\tau) \delta(t - \tau) \, d\tau \quad (18)$$

with the solution

$$\lambda = 1, \quad (19)$$

We shall therefore adopt the normalization in general that

$$\max |H(\omega)| = 1. \quad (20)$$

This means that

$$E_0 = \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(\omega) H(\omega)|^2 d\omega \leq \frac{1}{2\pi} \int_{-\infty}^{\infty} |F(\omega)|^2 d\omega = E_I \quad (21)$$

so that, with our normalization,

$$\lambda_1 \leq 1, \quad (22)$$

Numerical Reduction of Integral Equation

To obtain a numerical solution to the integral equation in Eq. (1), we utilize the method of moments.⁶ We expand $f(t)$ in a sequence of pulse functions

$$f(t) = \sum_{n=-N}^N a_n p_n(t), \quad (23)$$

where

$$p_n(t) = \left\{ \begin{array}{ll} 1 & n\Delta - \frac{1}{2} < t < n\Delta + \frac{1}{2} \\ 0 & \text{otherwise} \end{array} \right\} \quad (24)$$

and

$$\Delta = \frac{T}{N + \frac{1}{2}}, \quad (25)$$

Substitution into Eq. (1) yields

$$\lambda \sum a_n p_n(t) = \sum a_n q_n(t), \quad (26)$$

where

$$q_n(t) = \int_{n\Delta - \frac{\Delta}{2}}^{n\Delta + \frac{\Delta}{2}} K(t - \tau) d\tau . \quad (27)$$

We next multiply both sides by $\delta(t - m\Delta)$ and integrate $(-T, T)$ to get

$$\lambda \sum a_n \delta_{mn} = \sum a_n q_n(m\Delta) . \quad (28)$$

We recognize Eq. (28) as a matrix equation

$$[\lambda_{mn}][a_n] = \lambda[a_n] , \quad (29)$$

where $[\lambda_{mn}]$ is a square symmetric matrix with elements given by

$$\lambda_{mn} = \int_{(|n-m| - \frac{1}{2})\Delta}^{(|n-m| + \frac{1}{2})\Delta} K(x) dx . \quad (30)$$

The matrix given by Eq. (29) can be solved for its eigenvalues and associated eigenfunctions by utilizing a series of subroutines contained in a package called Eispack.⁷ The appropriate subroutines and their function for this problem are as follows:

- TRED1 - transforms the real symmetric matrix in Eq. (30) to tridiagonal symmetric.
- BSTURM - calculates an interval containing a specified number of largest eigenvalues.
- TSTURM - finds the eigenvalues in the interval calculated by BSTURM and the associated eigenfunctions of the tridiagonal matrix.
- TRBAK1 - back transforms the eigenfunctions of the tridiagonal matrix to find the eigenfunctions of the real symmetric matrix.

A computer program has been written to perform the numerical reduction of the integral equation in Eq. (1). The program can operate in one of two modes. In the first mode, the program accepts numerical data representing a transfer function $H(\omega)$ and performs the inverse Fourier transform indicated in Eq. (13) to produce the kernel function $K(t)$. The cosine form of the transform in Eq. (13) differs only by a multiplicative factor of two from the inverse transform applicable to a causal real function. We therefore use subroutine LFILON⁸ to obtain this result. Once $K(t)$ has been calculated, the square matrix $[k_{mn}]$ is obtained by numerical quadrature. The above subroutines from EISPACK are then employed to give the required maximum eigenvalue and associated eigenfunction. In the second mode, the program depends on the user supplying analytical expressions for $H(\omega)$ and for $K(t)$ in two function subprograms. In this case the necessity of performing a numerical inverse transform is eliminated. Beyond this difference, the remainder of the program functions as in the first mode. A listing of the program is included in Appendix B.

Numerical Results

The program described above was first used to perform checks against the results of Chalk (Ref. 1, p. 89) and Slepian and Poliak (Ref. 2, pp. 47-51). In all cases, the results duplicated theirs and will not be repeated here. Slepian's and Poliak's results are reproduced in a well-known textbook by Papoulis (Ref. 4, p. 69)]. After these checks were performed, we considered the case of a single resonance transfer function, given by

$$H(\omega) = \frac{2\alpha i\omega}{(\alpha + i\omega)^2 + \beta^2} \quad (31)$$

From Eq. (31), the kernel function $K(t)$ may be found analytically by closing the integral given in Eq. (10) along a semicircle through the top half of the complex ω -plane and using the calculus of residues. This procedure gives the result for $t > 0$ only; since $K(t)$ has been shown to be symmetric, however, this is sufficient. The result is

$$K(t) = \alpha e^{-\alpha|t|} \left(\cos\beta|t| - \frac{\alpha}{\beta} \sin\beta|t| \right), \quad (32)$$

where

$$\beta = (\omega_0^2 - \alpha^2)^{\frac{1}{2}}, \quad \omega_0 > \alpha \quad (33)$$

Since the analytical expressions are available in this case, the program operates in the second mode.

In Fig. 1, we show the magnitude of the transfer function in decibels for the single resonant case. We selected parameter values of $\alpha = 9.16 \times 10^6$ and $f_0 = 48.6$ MHz.

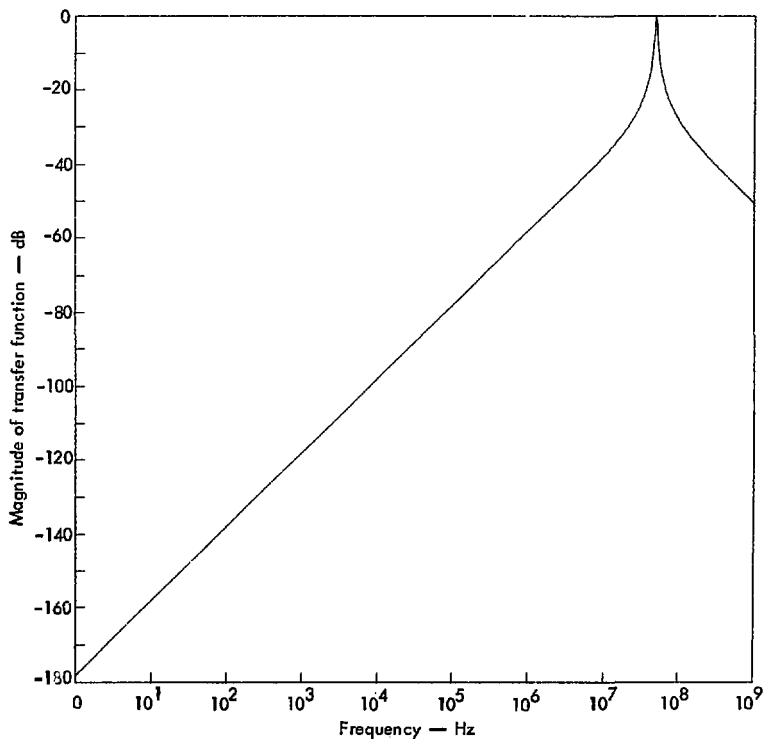


Fig. 1. Magnitude of the transfer function in decibels for the single resonant case.

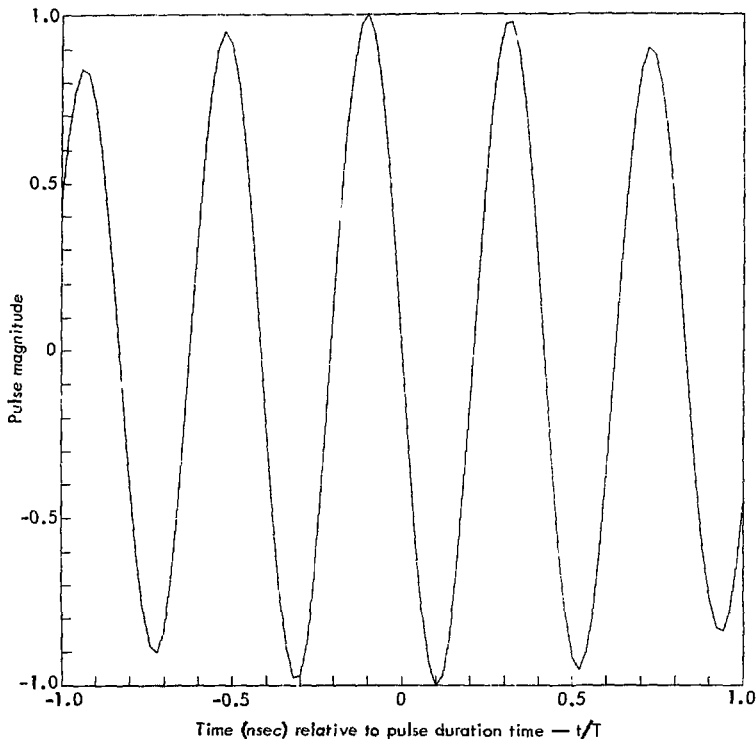


Fig. 2. Optimum pulse for the case where $T = 50$ nsec. Maximum eigenvalue = 0.35.

The reason for the choice was to attempt to match some numerical transfer function data for a long, narrow slot in an infinite ground plane. The resulting optimum pulse for the case $T = 50$ nsec (Fig. 2) is a modulated signal whose period corresponds to the frequency of the resonance of the transfer function. When $T = 100$ nsec (Fig. 3), the period of the ripple stays the same but the decay of the envelope is more pronounced. In

addition the eigenvalue has increased from 0.35 to 0.54 which indicates a strong increase in energy transfer efficiency. When T is increased to 200 nsec (Fig. 4) and then to 300 nsec (Fig. 5), the modulation frequency remains the same but the envelope decay continues to increase. In addition, the eigenvalue increases to 0.68 and then to 0.74.

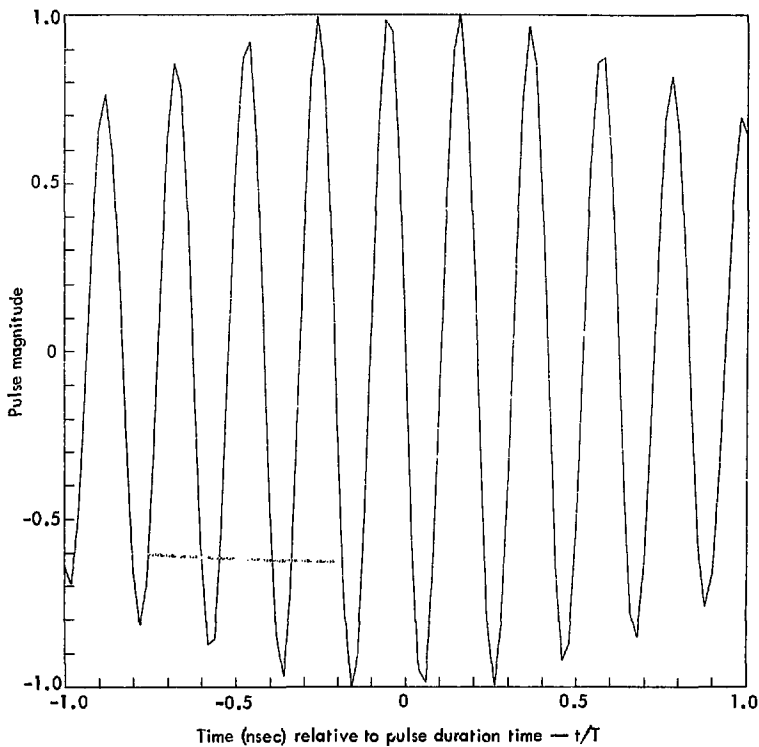


Fig. 3. Optimum pulse for the case where $T = 100$ nsec. Maximum eigenvalue = 0.54.

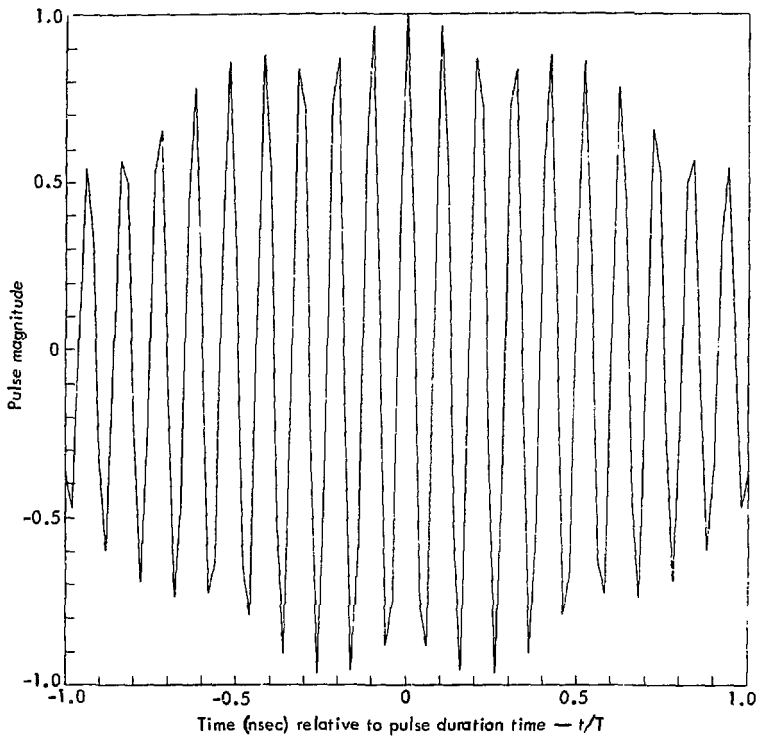


Fig. 4. Optimum pulse for the case where $T = 200$ nsec. Maximum eigenvalue = 0.68

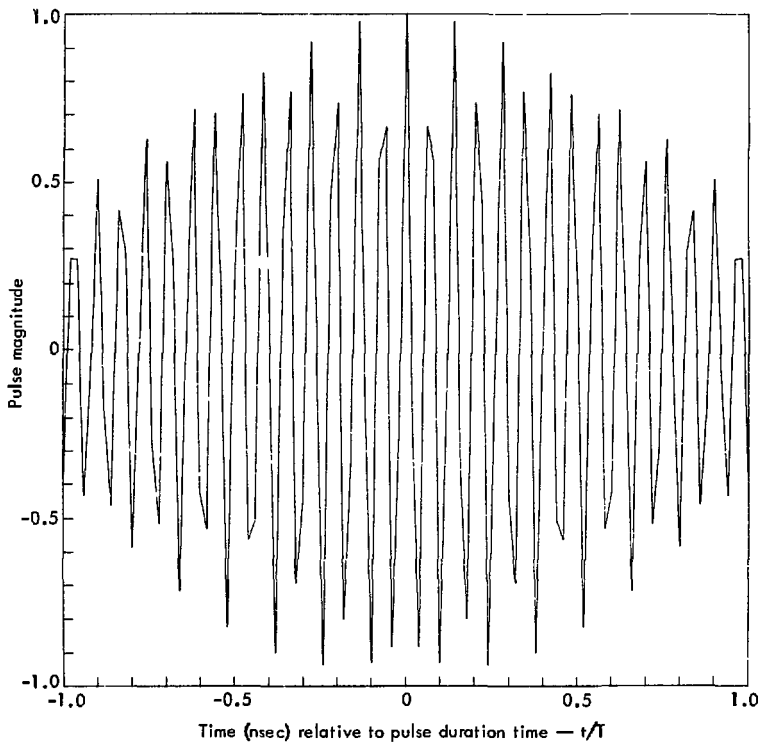


Fig. 5. Optimum pulse for the case where $T = 300$ nsec. Maximum eigenvalue ≈ 0.74 .

Conclusions and Recommendations for Further Work

There are few surprises in the numerical results for the single resonance case. The optimum pulse contains a modulation rate which favors the frequency at which the transfer function has its peak. In addition the pulse becomes more efficient as the length of time $(-T, T)$ of application

of the incident pulse is increased. The shape of the envelope is qualitatively similar to the shape of the entire pulse for the low-pass filter investigated by Chalk and by Slepian and Pollak. This is in keeping with the ideas common in equivalent low-pass filter analysis of band-pass filters (Ref. 4, p. 122). (Here, we regard the single-resonant model as a band-pass filter.)

We noted earlier that the results are only preliminary. However, now that the computer program has been written, a large range of transfer functions can be investigated. Such an investigation should produce some trends in the transfer of energy which should make possible some generalizations concerning the process.

In addition, there seems to be no fundamental limitation on the infinite limits in the integral of Eq. (6). If the limits were finite, the analysis would proceed as before with the exception that the kernel function in Eq. (10) would be calculated from an integral over finite limits. This is an important observation because it raises the possibility of maximizing the energy in a finite bandwidth in the output to the linear system. Fortunately, if we agree to add the energy contribution in the finite bandwidth (ω_1, ω_2) and the energy in the same band over the mirror negative frequencies, the symmetry of the kernel function is not destroyed and we may proceed with the numerical reduction as before.

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Appendix A – Maximization with a Constraint

We wish to maximize the double integral

$$E_0 = \int_{-T}^T f(\tau) \int_{-T}^T f(x) K(|x - \tau|) dx d\tau \quad (A-1)$$

subject to the constraint

$$E_I = \int_{-T}^T f^2(t) dt . \quad (A-2)$$

We form the functional $E(f)$

$$E = E_0 - \lambda E_I , \quad (A-3)$$

where λ is a Lagrange multiplier. We therefore have

$$E = \int_{-T}^T f(\tau) \int_{-T}^T f(x) K(|x - \tau|) dx d\tau - \lambda \int_{-T}^T f^2(t) dt . \quad (A-4)$$

Let f take on a variation δ so that

$$\begin{aligned} E(f + \alpha\delta) = & \int_{-T}^T [f(\tau) + \alpha\delta(\tau)] \int_{-T}^T [f(x) + \alpha\delta(x)] K(|x - \tau|) dx d\tau \\ & - \alpha \int_{-T}^T [f(x) + \alpha\delta(x)]^2 dx . \quad (A-5) \end{aligned}$$

Expanding and collecting terms, we obtain

$$E(f + \alpha\delta) = E(f) + \partial\alpha G + \alpha^2 H - \partial\alpha\lambda I - \alpha^2\lambda J , \quad (A-6)$$

where

$$G = \int_{-T}^T \delta(\tau) \int_{-T}^T f(x) K(|x - \tau|) dx d\tau \quad (A-7)$$

$$H = \int_{-T}^T \delta(\tau) \int_{-T}^T \delta(x) K(|x - \tau|) dx d\tau \quad (A-8)$$

$$I = \int_{-T}^T f(x) \delta(x) dx \quad (A-9)$$

$$J = \int_{-T}^T \delta^2(x) dx. \quad (A-10)$$

To maximize (or minimize), take

$$\left. \frac{\partial}{\partial \alpha} [E(f + \alpha \delta)] \right|_{\alpha=0} = 0 \quad (A-11)$$

with the result

$$G = \lambda I, \quad (A-12)$$

or,

$$\int_{-T}^T \delta(\tau) \int_{-T}^T f(x) K(|x - \tau|) dx d\tau = \lambda \int_{-T}^T \delta(\tau) d\tau. \quad (A-13)$$

This may be written

$$\int_{-T}^T \delta(\tau) \left\{ \left[\int_{-T}^T f(x) K(|x - \tau|) dx \right] - \lambda f(\tau) \right\} d\tau = 0 \quad (A-14)$$

and since δ is arbitrary

$$\lambda f(\tau) = \int_{-T}^T f(x) K(|x - \tau|) dx, \quad (A-15)$$

which is a verification of Eq. (11).

Appendix B - Computer Program Listing

```

1      PROGRAM LOPAS (INPUT,DUDPUT,TAPES=INPUT,TAPES=DUDPUT)
2 C    THE PURPOSE OF PROGRAM LOPAS IS TO CALCULATE A TIME - LIMITED INPUT
3 C    PULSE TO A GIVEN TRANSFER FUNCTION WHICH IS OPTIMUM IN THE SENSE
4 C    THAT FOR A SPECIFIED ENERGY IN THE INPUT IT MAXIMIZES THE TOTAL
5 C    ENERGY IN THE OUTPUT. THE PROGRAM OPERATES IN TWO MODE OPTIONS
6 C    DEPENDING ON WHETHER THE TRANSFER FUNCTION IS SUPPLIED ANALYTICALLY
7 C    OR NUMERICALLY BY THE USER. THE READ-IN SEQUENCE IS AS FOLLOWS.
8 C    FOR BOTH MODES OF OPERATION, THE FIRST DATA CARD IS READ IN BY
9 C
10 C      READ (5,60) MAX,IREAD,WT
11 C      60 FORMAT (2I10,F10.0)
12 C
13 C    WHERE
14 C
15 C      MAX - THE SIZE OF THE MATRIX WHOSE EIGENFUNCTIONS AND EIGEN-
16 C            VALUES ARE TO BE DETERMINED. THE PROGRAM CALCULATES THE
17 C            TWO HIGHEST EIGENVALUES AND CORRESPONDING EIGENVECTORS.
18 C            THE HIGHEST EIGENVALUE IS THE EFFICIENCY OF ENERGY TRANS-
19 C            FER AND THE CORRESPONDING EIGENVECTOR IS THE OPTIMUM
20 C            PULSE
21 C
22 C      IREAD - THE MODE NUMBER. IF IREAD = 0, TRANSFER FUNCTION DATA
23 C            IS SUPPLIED ANALYTICALLY IN TWO FUNCTION SUBPROGRAMS
24 C            WHICH MUST BE SUPPLIED BY THE USER. FUNCTION FCTF(X)
25 C            MUST CALCULATE AND RETURN THE MAGNITUDE-SQUARED OF THE
26 C            TRANSFER FUNCTION AS A FUNCTION OF THE RADIAN FREQUENCY.
27 C            FUNCTION FCTI(X) MUST CALCULATE AND RETURN THE INVERSE
28 C            FOURIER TRANSFORM OF THE TRANSFER FUNCTION MAGNITUDE
29 C            SQUARED. IF IREAD = 1, TRANSFER FUNCTION DATA IS SUP-
30 C            PLIED NUMERICALLY BY THE USER AND THE INVERSE TRANSFORM
31 C            OF THE MAGNITUDE SQUARED IS SUBSEQUENTLY CALCULATED BY
32 C            THE PROGRAM THROUGH SUBROUTINE LFILOM.
33 C
34 C      WT - THE EXTENT OF THE TIME-LIMITED PULSE IS PLUS OR MINUS WT.
35 C
36 C    THE ABOVE DATA CARD IS COMMON TO BOTH MODE 0 AND MODE 1. THE
37 C    REMAINING CARDS FOR MODE 0 ARE AS FOLLOWS.
38 C
39 C      READ (5,50) NOEC
40 C      READ (5,260) (THS(KK),KK=1,NDEC)
41 C      50 FORMAT (I10)
42 C      260 FORMAT (15I5)
43 C
44 C    WHERE THE FREQUENCIES ARE CALCULATED IN DECADE BLOCKS AND
45 C
46 C      NDEC - THE NUMBER OF FREQUENCY DECADES
47 C
48 C      THS(KK) - AN ARRAY CONTAINING THE NUMBER OF POINTS IN EACH DECADE.
49 C
50 C    FOR MODE 1, THE REMAINING DATA CARDS ARE READ IN AS FOLLOWS.
51 C
52 C      READ (5,240) NFP,HZ
53 C      READ (5,210) (H(K),F(K),K=1,NFP)
54 C      240 FORMAT (10,5X,2E15.6)
55 C      210 FORMAT (2E15.6,10X,E15.6)
56 C
57 C    WHERE
58 C
59 C      NFP - THE NUMBER OF FREQUENCY POINTS AT WHICH DATA IS SUPPLIED
60 C
61 C      HZ - THE TRANSFER FUNCTION (COMPLEX) AT ZERO FREQUENCY
62 C
63 C      H(K) - THE TRANSFER FUNCTION (COMPLEX) AT EACH FREQUENCY POINT
64 C

```

65 C F(K) - THE FREQUENCY POINTS

66 C

67 C -----

68 C

```
69 CALL DEVICE (6HCREATE,6HOUTPUT,50000)
70 INTEGER THS
71 COMPLEX I,B,H,HZ
72 COMMON A(101,101),E(101) W(2),Z(101,2),R1(101),R2(101),
73 1 R3(101),R4(101),R5(101),R6(101),E2(101),EMIN(2),EMAX(2),D(101)
74 2 U(101),V(101),VOFF(100),T( 700),FT( 700),FTA( 700),IND( 700),
75 3 F(500),H( 500),B(500),HMD(500),HT( 700),THS(15),PLD(5,10)
76 READ (5,60) MAX,IREAD,WT
77 NPTS = 5
78 MXL = (MAX - 1) / 2
79 DEL = WT / (MXL + .5)
80 WRITE (6,20) MAX,WT,NPTS
81 XINC = DEL / (2. * (NPTS - 1))
82 ITF = 0
83 NT = (2 * MAX - 1) * (NPTS - 1) + 1
84 DO 131 N = 1,NT
85 131 T(N) = (N - 1) * XINC
86 WRITE (6,110) T(NT),XINC
87 TZ = 0.
88 IF (IREAD .EQ. 1) GO TO 201
89 WRITE (6,140)
90 READ (5,50) NDEC
91 READ (5,260) (THS(KK),KK=1,NDEC)
92 PI = 3.1415926
93 K = 0
94 HZ = CMPLX(FCTF(0.),0.)
95 DO 211 KK = 1,NDEC
96 KL = KK - 1
97 COU = 10 ** KL
98 XI = 9. / THS(KK)
99 NMX = THS(KK)
100 DO 241 L = 1,NMX
101 NL = L - 1
102 K = K + 1
103 F(K) = COU * (1. + NL * XI)
104 W = 2. * PI * F(K)
105 H(K) = CMPLX(FCTF(W),0.)
106 HZ = CMPLX(FCTF(0.),0.)
107 HMD(K) = 10. * ALOG10(CABS(H(K)))
108 241 CONTINUE
109 211 CONTINUE
110 NFP = K
111 DO 261 K = 1,NT
112 FT(K) = FCTT(T(K))
113 261 CONTINUE
114 GO TO 202
115 201 CONTINUE
116 WRITE (6,150)
117 READ (5,240) NFP,HZ
118 READ (5,210) (H(K),F(K),K=1,NFP)
119 HZ = HZ * CONJG(HZ)
120 DO 221 K = 1,NFP
121 H(K) = H(K) * CONJG(H(K))
122 HMD(K) = 10. * ALOG10(CABS(H(K)))
123 221 CONTINUE
124 NTM = NT - 1
125 DO 281 N = 1,NTM
126 NP = N + 1
127 281 HT(N) = T(NP)
128 TZ = 0.
```



```

129 CALL LFILON (TZ,H1,FT,FTA,NTM,F,HZ,H,NFP,B,(NO,(TF)
130 DO 231 K = 1,NTM
131 KR = NT - K + 1
132 KRL = KR - 1
133 231 FT(KR) = F(KRL) / 2.
134 NFPM = NFP - 1
135 FT(1) = HZ * F(1) + H(1) * F(2) + H(NFP) * (F(NFP) - F(NFPM))
136 DO 271 K = 2,NFPM
137 KP = K + 1
138 KM = K - 1
139 FT(1) = FT(1) + H(K) * (F(KP) - F(KM))
140 271 CONTINUE
141 202 CONTINUE
142 WRITE (6,250) HZ
143 DO 61 K = 1,NFP
144 61 WRITE (6,230) F(K),H(K)
145 WRITE (6,120)
146 WRITE (6,130) T(K),FT(K),K=1,NT)
147 CALL QSF (XINC,FT,V,NPTS)
148 VZ = V(NPTS)
149 NPTS2 = 2 * NPTS - 1
150 MAXL = MAX - 1
151 DO 111 M = 1,MAXL
152 MS = (2 * M - 1) * NPTS - 2 * M + 2
153 DO 121 N = 1,NPTS2
154 NA = N - 1 + MS
155 121 U(N) = FT(NA)
156 CALL QSF (XINC,U,V,NPTS2)
157 VOFF(M) = V(NPTS2)
158 111 CONTINUE
159 DO 81 M = 1,MAX
160 81 A(M,M) = 2. * VZ
161 DO 11 M = 1,MAXL
162 MP = M + 1
163 DO 21 N = MP,MAX
164 NL = N - M
165 21 A(N,NL) = VOFF(M)
166 11 CONTINUE
167 CALL TRED1 (10),MAX,A,D,E,E2)
168 IFLAG = 3
169 CALL BSTURM (MAX,2,10),IFLAG,XL,XU,D,E,E2)
170 IF (IFLAG .EQ. -1) WRITE (6,10)
171 XXQ = -1.
172 CALL TSTURM (101,MAX,XXQ,D,E,E2,XL,XU,10),ME,W,Z,IEER,R1,R2,R3,R4,
173 1 R5,R6)
174 IF (IEER .NE. 0) WRITE (6,30) IEER
175 CALL TRBAK1 (101,MAX,A,E,ME,Z)
176 DO 51 N = 1,MAX
177 R1(N) = Z(N,1)
178 51 R2(N) = Z(N,2)
179 CALL AMNMX (MAX,R1,EMIN(1),EMAX(1))
180 CALL AMNMX (MAX,R2,EMIN(2),EMAX(2))
181 WRITE (6,80)
182 DO 31 M = 1,ME
183 IF (ABS(EMIN(M)) .GT. ABS(EMAX(M))) GO TO 2
184 GO TO 1
185 2 STO = EMAX(M)
186 EMAX(M) = EMIN(M)
187 EMIN(M) = STO
188 1 CONTINUE
189 WRITE (6,90) W(4)
190 DO 41 N = 1,MAX
191 Z1(N,M) = Z1(N,M) / EMAX(M)
192 41 WRITE (6,40) Z1(N,M)

```

```

193 31 CONTINUE
194 DO 71 N = 1,MAX
195 71 PLO(1,N) = Z(N,2)
196 WRITE (6,100) W(2)
197 CALL PLOTS (PLO,1,MAX,999)
198 10 FORMAT (/// * WARNING -- ERRORS IN BSTURN INPUT*///)
199 20 FORMAT (1H), * ENERGY MAXIMIZATION*/// * MATRIX SIZE = *
200 116/* TIME WINDOW (NS) = *E14.3/* NO. OF INTEGRATION PTS = *
201 215//)
202 30 FORMAT (/// * WARNING -- IERR = *15//)
203 40 FORMAT (8X,E15.5)
204 50 FORMAT (11C)
205 60 FORMAT (2110,F10.0)
206 80 FORMAT (./* TWO HIGHEST EIGENVALUES WITH ASSOCIATED EIGENVECTORS*
207 1)
208 90 FORMAT (/// * EIGENVALUE = *E15.5//12X *EIGENVECTOR*///)
209 100 FORMAT (//////// * THE FOLLOWING PLOT IS OF THE EIGENVECTOR ASSOCIA
210 1TED WITH THE MAXIMUM EIGENVALUE LAMBDA = *E11.3//)
211 110 FORMAT (* TIME GOES FROM 0. TO *E10.3* SECONDS IN *E10.3* SECOND
212 1INCREMENTS*///)
213 120 FDMAT (/// * INVERSE TRANSFORM OF H(F) MAG SQUARED*//5X*1(K)*13X
214 1*FT(K)*///)
215 130 FORMAT (2C15.5)
216 140 FORMAT (* INVERSE TRANSFORM IS PERFORMED ANALYTICALLY BY USER*///)
217 150 FORMAT (* INVERSE TRANSFORM IS SUPPLIED NUMERICALLY BY USER*///)
218 210 FORMAT (2E15.6,10X,E15.5)
219 230 FORMAT (6E15.5)
220 240 FORMAT (110,5X,2E15.6)
221 250 FORMAT (* TRANSFER FUNCTION MAGNITUDE SQUARED*//4X*0.*9X,2E15.5)
222 1*H(F)*//4X*0.*9X,2E15.5)
223 260 FORMAT (1515)
224 CALL EXIT
225 END

```

```
1      SUBROUTINE AMNMX (MAX,A,AMN,AMX)
2      DIMENSION A(1)
3      AMN = A(1)
4      AMX = AMN
5      DO 11 M = 2,MAX
6      IF (A(M) .GT. AMX) AMX = A(M)
7      IF (A(M) .LT. AMN) AMN = A(M)
8  11 CONTINUE
9      RETURN
10     END
```

```
1  FUNCTION FCTT(X)
2  F = 4.857E7
3  W = 2. * 3.1415926 * F
4  A = .03 * W
5  B = SQRT(W * W - A * A)
6  FCTT = A * EXP(-A * X) * (COS(B * X) - A * SIN(B * X) / B)
7  RETURN
8  END
```

```

1      FUNCTION FCTF(X)
2      COMPLEX I,Z
3      F = 4.857E7
4      W = 2. * 3.1415926 * F
5      A = .03 * W
6      I = CMPLX(0.,1.)
7      B = SQRT(W * W - A * A)
8      Z = 2. * A * I * X / ((A + I * X) ^ (A + I * X) + B * B)
9      FCTF = REAL(Z * CONJG(Z))
10     RETURN
11     END

```

```

1 C                                     93215001
2 C ----- 93215002
3 C                                     93215003
4 SUBROUTINE TSTURM(NM,N,EP1,D,E,E2,UB,MM,M,W,Z, 93215004
5 X IERR,RV1,RV2,RV3,RV4,RV5,RV6) 93215005
6 C*NMS:MATHLIB:NATS:EISPACK:SOURCE:TSTURM TSTURM E2.V2 11/28/73 LLL2
7 C                                     93215006
8 INTEGER I,J,K,M,N,P,Q,R,S,II,IP,JJ,MM,I1,M2,NM,ITS, 93215007
9 X IERR,GROUP,ISTURM 93215008
10 REAL D(N1,E(N),E2(N),W(MM),Z(NM,MM), 93215009
11 X RV1(N),RV2(N),RV3(N),RV4(N),RV5(N),RV6(N) 93215010
12 REAL U,V,LB,T1,T2,UB,UK,XU,X0,X1,EP1,EP2,EP3,EP4, 93215011
13 X NORM,MACHEP 93215012
14 C REAL SQRT,ABS,AMAX1,AMIN1,FLOAT LLL25013
15 C                                     93215014
16 C THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE TRISTURM 93215015
17 C BY PETERS AND WILKINSON. 93215016
18 C HANDBOOK FOR AUTO. COMP., VOL. II--LINEAR ALGEBRA, 418-439(1971). 93215017
19 C                                     93215018
20 C THIS SUBROUTINE FINDS THOSE EIGENVALUES OF A TRIDIAGONAL 93215019
21 C SYMMETRIC MATRIX WHICH LIE IN A SPECIFIED INTERVAL AND THEIR 93215020
22 C ASSOCIATED EIGENVECTORS, USING BISECTION AND INVERSE ITERATION. 93215021
23 C                                     93215022
24 C ON INPUT- 93215023
25 C                                     93215024
26 C NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL 93215025
27 C ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM 93215026
28 C DIMENSION STATEMENT. 93215027
29 C                                     93215028
30 C N IS THE ORDER OF THE MATRIX. 93215029
31 C                                     93215030
32 C EP1 IS AN ABSOLUTE ERROR TOLERANCE FOR THE COMPUTED 93215031
33 C EIGENVALUES. IT SHOULD BE CHOSEN COMMENSURATE WITH 93215032
34 C RELATIVE PERTURBATIONS IN THE MATRIX ELEMENTS OF THE 93215033
35 C ORDER OF THE RELATIVE MACHINE PRECISION. IF THE 93215034
36 C INPUT EP1 IS NON-POSITIVE, IT IS RESET FOR EACH 93215035
37 C SUBMATRIX TO A DEFAULT VALUE, NAMELY, MINUS THE 93215036
38 C PRODUCT OF THE RELATIVE MACHINE PRECISION AND THE 93215037
39 C 1-NORM OF THE SUBMATRIX. 93215038
40 C                                     93215039
41 C D CONTAINS THE DIAGONAL ELEMENTS OF THE INPUT MATRIX. 93215040
42 C                                     93215041
43 C E CONTAINS THE SUBDIAGONAL ELEMENTS OF THE INPUT MATRIX 93215042
44 C IN ITS LAST N-1 POSITIONS. E(1) IS ARBITRARY. 93215043
45 C                                     93215044
46 C E2 CONTAINS THE SQUARES OF THE CORRESPONDING ELEMENTS OF E. 93215045
47 C E2(1) IS ARBITRARY. 93215046
48 C                                     93215047
49 C LB AND UB DEFINE THE INTERVAL TO BE SEARCHED FOR EIGENVALUES. 93215048
50 C IF LB IS NOT LESS THAN UB, NO EIGENVALUES WILL BE FOUND. 93215049
51 C                                     93215050
52 C MM SHOULD BE SET TO AN UPPER BOUND FOR THE NUMBER OF 93215051
53 C EIGENVALUES IN THE INTERVAL. WARNING- IF MORE THAN 93215052
54 C MM EIGENVALUES ARE DETERMINED TO LIE IN THE INTERVAL, 93215053
55 C AN ERROR RETURN IS MADE WITH NO VALUES OR VECTORS FOUND. 93215054
56 C                                     93215055
57 C ON OUTPUT- 93215056
58 C                                     93215057
59 C EP1 IS UNALTERED UNLESS IT HAS BEEN RESET TO ITS 93215058
60 C (LAST) DEFAULT VALUE. 93215059
61 C                                     93215060
62 C D AND E ARE UNALTERED. 93215061
63 C                                     93215062
64 C ELEMENTS OF E2, CORRESPONDING TO ELEMENTS OF E REGARDED 93215063

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65 C AS NEGLIGIBLE, HAVE BEEN REPLACED BY ZERO CAUSING THE 93215064
66 C MATRIX TO SPLIT INTO A DIRECT SUM OF SUBMATRICES. 93215065
67 C E2(1) IS ALSO SET TO ZERO. 93215066
68 C 93215067
69 C M IS THE NUMBER OF EIGENVALUES DETERMINED TO LIE IN (LB,UB). 93215068
70 C 93215069
71 C W CONTAINS THE M EIGENVALUES IN ASCENDING ORDER IF THE MATRIX 93215070
72 C DOES NOT SPLIT. IF THE MATRIX SPLITS, THE EIGENVALUES ARE 93215071
73 C IN ASCENDING ORDER FOR EACH SUBMATRIX. IF A VECTOR ERROR 93215072
74 C EXIT IS MADE, W CONTAINS THOSE VALUES ALREADY FOUND. 93215073
75 C 93215074
76 C Z CONTAINS THE ASSOCIATED SET OF ORTHONORMAL EIGENVECTORS. 93215075
77 C IF AN ERROR EXIT IS MADE, Z CONTAINS THOSE VECTORS 93215076
78 C ALREADY FOUND. 93215077
79 C 93215078
80 C IERR IS SET TO 93215079
81 C ZERO FOR NORMAL RETURN. 93215080
82 C 3*N+1 IF M EXCEEDS MM. 93215081
83 C 4*N+R IF THE EIGENVECTOR CORRESPONDING TO THE R-TH 93215082
84 C EIGENVALUE FAILS TO CONVERGE IN 5 ITERATIONS. 93215083
85 C 93215084
86 C RV1, RV2, RV3, RV4, RV5, AND RV6 ARE TEMPORARY STORAGE ARRAYS. 93215085
87 C 93215086
88 C THE ALGOL PROCEDURE STURMCN* CONTAINED IN TRISTURM 93215087
89 C APPEARS IN TSTURM IN-LINE. 93215088
90 C 93215089
91 C NOTE THAT SUBROUTINE TQL2 OR IMTQL2 IS GENERALLY FASTER THAN 93215090
92 C TSTURM. IF MORE THAN N/4 EIGENVALUES AND VECTORS ARE TO BE FOUND. 93215091
93 C 93215092
94 C QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW, 93215093
95 C APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY 93215094
96 C 93215095
97 C LLL CONSULTANT... R. P. DICKINSON 93215096
98 C VERSION 2 = CORRECT DECLARATIONS FOR PUT 93215097
99 C 93215098
100 C ----- 93215099
101 C 93215100
102 C ***** MACHEP IS A MACHINE DEPENDENT PARAMETER SPECIFYING 93215101
103 C THE RELATIVE PRECISION OF FLOATING POINT ARITHMETIC. 93215102
104 C 93215103
105 C ***** 93215104
106 MACHEP = 2.**(-47) 93215105
107 C 93215106
108 IERR = 0 93215107
109 I1 = LB 93215108
110 I2 = UB 93215109
111 C ***** LOOK FOR SMALL SUB-DIAGONAL ENTRIES ***** 93215110
112 DO 40 I = 1, N 93215111
113 IF (I .EQ. 1) GO TO 20 93215112
114 IF (ABS(E(I)) .GT. MACHEP * (ABS(D(I)) + ABS(D(I-1)))) 93215113
115 X GO TO 40 93215114
116 20 E2(I) = 0.0 93215115
117 40 CONTINUE 93215116
118 C ***** DETERMINE THE NUMBER OF EIGENVALUES 93215117
119 C IN THE INTERVAL ***** 93215118
120 P = 1 93215119
121 Q = N 93215120
122 XI = UB 93215121
123 ISTURM = 1 93215122
124 GO TO 320 93215123
125 60 M = 5 93215124
126 XI = LB 93215125
127 ISTURM = 2 93215126
128 GO TO 320 93215127

```

129	80	M = M - 5	93215125
130		IF (M .GT. MM) GO TO 980	93215126
131		Q = 0	93215127
132		R = 0	93215128
133	C	***** ESTABLISH AND PROCESS NEXT SUBMATRIX, REFINING	93215129
134	C	INTERVAL BY THE GERSCHGORIN BOUNDS *****	93215130
135	100	IF (R .EQ. M) GO TO 1001	93215131
136		P = Q + 1	93215132
137		XU = D(P)	93215133
138		X0 = D(P)	93215134
139		U = 0.0	93215135
140	C		93215136
141		DO 120 Q = P, N	93215137
142		X1 = U	93215138
143		U = 0.0	93215139
144		V = 0.0	93215140
145		IF (Q .EQ. N) GO TO 110	93215141
146		U = ABS(E(Q+1))	93215142
147		V = E2(Q+1)	93215143
148	110	XU = AMIN1(D(Q)-(X1+U),XU)	93215144
149		X0 = AMAX1(D(Q)+(X1+U),X0)	93215145
150		IF (V .EQ. 0.0) GO TO 140	93215146
151	120	CONTINUE	93215147
152	C		93215148
153	140	X1 = AMAX1(ABS(XU),ABS(X0)) * MACHEP	93215149
154		IF (EPS1 .LE. 0.0) EPS1 = -X1	93215150
155		IF (P .NE. Q) GO TO 180	93215151
156	C	***** CHECK FOR ISOLATED ROOT WITHIN INTERVAL *****	93215152
157		IF (T1 .GT. D(P) .OR. D(P) .GE. T2) GO TO 940	93215153
158		R = R + 1	93215154
159	C		93215155
160		DO 160 I = 1, N	93215156
161	160	Z(I,R) = 0.0	93215157
162	C		93215158
163		W(R) = D(P)	93215159
164		Z(P,R) = 1.0	93215160
165		GO TO 940	93215161
166	180	X1 = X1 * FLOAT(Q-P+1)	93215162
167		LB = AMAX1(T1,XU-X1)	93215163
168		UB = AMIN1(T2,X0+X1)	93215164
169		X1 = LB	93215165
170		ISTURM = 3	93215166
171		GO TO 320	93215167
172	200	M1 = S + 1	93215168
173		X1 = UB	93215169
174		ISTURM = 4	93215170
175		GO TO 320	93215171
176	220	M2 = S	93215172
177		IF (M1 .GT. M2) GO TO 940	93215173
178	C	***** FIND ROOTS BY BISECTION *****	93215174
179		X0 = UB	93215175
180		ISTURM = 5	93215176
181	C		93215177
182		DO 240 I = M1, M2	93215178
183		RV5(I) = UB	93215179
184		RV4(I) = LB	93215180
185	240	CONTINUE	93215181
186	C	***** LOOP FOR K-TH EIGENVALUE	93215182
187	C	FOR K=M2 STEP -1 UNTIL M1 DO --	93215183
188	C	(--DO- NOT USED TO LEGALIZE COMPUTEE-GO-TO) *****	93215184
189		K = M2	93215185
190	250	XU = LB	93215186
191	C	***** FOR I=K STEP -1 UNTIL M1 DO -- *****	93215187
192		DO 260 II = M1, K	93215188


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193          I = NI + K - 1  93215189
194          IF (XU .GE. RV4(I)) GO TO 260 93215190
195          XU = RV4(I) 93215191
196          GO TO 280 93215192
197 260 CONTINUE 93215193
198 C 93215194
199 280 IF (X0 .GT. RV5(K)) X0 = RV5(K) 93215195
200 C ***** NEXT BISECTION STEP ***** 93215196
201 300 X1 = (XU + X0) * 0.5 93215197
202 IF ((X0 - XU) .LE. (2.0 * MACHEP * 93215198
203 X (ABS(XU) + ABS(X0)) + ABS(EPS1))) GO TO 420 93215199
204 C ***** IN-LINE PROCEDURE FOR STURM SEQUENCE ***** 93215200
205 320 S = P - 1 93215201
206 U = 1.0 93215202
207 C 93215203
208 DO 340 I = P, 0 93215204
209 IF (U .NE. 0.0) GO TO 325 93215205
210 V = ABS(E(I)) / MACHEP 93215206
211 GO TO 330 93215207
212 325 V = E2(I) / U 93215208
213 330 U = D(I) - X1 - V 93215209
214 IF (U .LT. 0.0) S = S + 1 93215210
215 340 CONTINUE 93215211
216 C 93215212
217 GO TO (60,80,200,220,360), 1STURM 93215213
218 C ***** REFINE INTERVALS ***** 93215214
219 360 IF (S .GE. K) GO TO 400 93215215
220 XU = X1 93215216
221 IF (S .GE. M1) GO TO 380 93215217
222 RV4(M1) = X1 93215218
223 GO TO 300 93215219
224 380 RV4(S+1) = X1 93215220
225 IF (RV5(S) .GT. X1) RV5(S) = X1 93215221
226 GO TO 300 93215222
227 400 X0 = X1 93215223
228 GO TO 300 93215224
229 C ***** K-TH EIGENVALUE FOUND ***** 93215225
230 420 RV5(K) = X1 93215226
231 K = K - 1 93215227
232 IF (K .GE. M1) GO TO 250 93215228
233 C ***** FIND VECTORS BY INVERSE ITERATION ***** 93215229
234 NORM = ABS(D(P)) 93215230
235 IP = P + 1 93215231
236 C 93215232
237 DO 500 I = IP, 0 93215233
238 500 NORM = NORM + ABS(D(I)) + ABS(E(I)) 93215234
239 C ***** EPS2 IS THE CRITERION FOR GROUPING, 93215235
240 C EPS3 REPLACES ZERO PIVOTS AND EQUAL 93215236
241 C ROOTS ARE MODIFIED BY EPS3, 93215237
242 C EPS4 IS TAKEN VERY SMALL TO AVOID OVERFLOW ***** 93215238
243 EPS2 = 1.0E-3 * NORM 93215239
244 EPS3 = MACHEP * NORM 93215240
245 UK = FLOAT(IP+1) 93215241
246 EPS4 = UK * EPS3 93215242
247 UK = EPS4 / SQRT(UK) 93215243
248 GROUP = 0 93215244
249 S = P 93215245
250 C 93215246
251 DO 920 K = M1, M2 93215247
252 R = R + 1 93215248
253 ITS = 1 93215249
254 W(R) = RV5(K) 93215250
255 X1 = RV5(K) 93215251
256 C ***** LOOK FOR CLOSE OR COINCIDENT ROOTS ***** 93215252

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257      IF (K .EQ. M1) GO TO 520 93215253
258      IF (X) - X0 .GE. EPS2) GROUP = -1 93215254
259      GROUP = GROUP * I 93215255
260      IF (X) .LE. X0) X1 = X0 * EPS3 93215256
261 C      ***** ELIMINATION WITH INTERCHANGES AND 93215257
262 C      INITIALIZATION OF VECTOR ***** 93215258
263 C      520 V = 0.0 93215259
264 C 93215260
265      DO 580 I = P, Q 93215261
266          RV6(I) = UK 93215262
267          IF (I .EQ. P) GO TO 560 93215263
268          IF (ABS(E(I))) .LT. ABS(U)) GO TO 540 93215264
269          XU = U / E(I) 93215265
270          RV4(I) = XU 93215266
271          RV1(I-1) = E(I) 93215267
272          RV2(I-1) = D(I) - X1 93215268
273          RV3(I-1) = 0.0 93215269
274          IF (I .NE. Q) RV3(I-1) = E(I+1) 93215270
275          U = V - XU * RV2(I-1) 93215271
276          V = -XU * RV3(I-1) 93215272
277          GO TO 580 93215273
278 C      540 XU = E(I) / U 93215274
279          RV4(I) = XU 93215275
280          RV1(I-1) = U 93215276
281          RV2(I-1) = V 93215277
282          RV3(I-1) = 0.0 93215278
283 C      560 U = D(I) - X1 - XU * V 93215279
284          IF (I .NE. Q) V = E(I+1) 93215280
285 C      580 CONTINUE 93215281
286 C 93215282
287      IF (U .EQ. 0.0) U = EPS3 93215283
288      RV1(Q) = U 93215284
289      RV2(Q) = 0.0 93215285
290      RV3(Q) = 0.0 93215286
291 C      ***** BACK SUBSTITUTION 93215287
292 C      FOR I=Q STEP -1 UNTIL P DO -- ***** 93215288
293 C      600 DO 620 I = P, Q 93215289
294          I = P + Q - I 93215290
295          RV6(I) = (RV6(I) - U * RV2(I) - V * RV3(I)) / RV1(I) 93215291
296          V = U 93215292
297          U = RV6(I) 93215293
298 C      620 CONTINUE 93215294
299 C      ***** ORTHOGONALIZE WITH RESPECT TO PREVIOUS 93215295
300 C      MEMBERS OF GROUP ***** 93215296
301      IF (GROUP .EQ. 0) GO TO 700 93215297
302 C 93215298
303      DO 680 JJ = 1, GROUP 93215299
304          J = R - GROUP - I + JJ 93215300
305          XU = 0.0 93215301
306 C 93215302
307          DO 640 I = P, Q 93215303
308 C      640 XU = XU + RV6(I) * Z(I,J) 93215304
309 C 93215305
310          DO 660 I = P, Q 93215306
311 C      660 RV6(I) = RV6(I) - XU * Z(I,J) 93215307
312 C 93215308
313 C      680 CONTINUE 93215309
314 C 93215310
315 C      700 NORM = 0.0 93215311
316 C 93215312
317      DO 720 I = P, Q 93215313
318 C      720 NORM = NORM + ABS(RV6(I)) 93215314
319 C 93215315
320      IF (NORM .GE. 1.0) GO TO 840 93215316

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321 C	***** FORWARD SUBSTITUTION *****	93215317
322	IF (ITS .EQ. 5) GO TO 960	93215318
323	IF (NORM .NE. 0.0) GO TO 740	93215319
324	RV6(5) = EPS4	93215320
325	S = S + 1	93215321
326	IF (S .GT. 0) S = P	93215322
327	GO TO 780	93215323
328 740	XU = EPS4 / NORM	93215324
329 C		93215325
330	DO 760 I = P, Q	93215326
331 760	RV6(I) = RV6(I) + XU	93215327
332 C	***** ELIMINATION OPERATIONS ON NEXT VECTOR	93215328
333 C	ITERATE *****	93215329
334 780	DO 820 I = IP, Q	93215330
335	U = RV6(I)	93215331
336 C	***** IF RV(I:-1) .EQ. E(I), A ROW INTERCHANGE	93215332
337 C	WAS PERFORMED EARLIER IN THE	93215333
338 C	TRIANGULARIZATION PROCESS *****	93215334
339	IF (RV(I:-1) .NE. E(I)) GO TO 800	93215335
340	U = RV6(I:-1)	93215336
341	RV6(I:-1) = RV6(I)	93215337
342 800	RV6(I) = U - RV4(I) * RV6(I:-1)	93215338
343 820	CONTINUE	93215339
344 C		93215340
345	ITS = ITS + 1	93215341
346	GO TO 600	93215342
347 C	***** NORMALIZE SO THAT SUM OF SQUARES IS	93215343
348 C	1 AND EXPAND TO FULL ORDER *****	93215344
349 840	U = 0.0	93215345
350 C		93215346
351	DO 860 I = P, Q	93215347
352 860	U = U + RV6(I)**2	93215348
353 C		93215349
354	XU = 1.0 / SQRT(U)	93215350
355 C		93215351
356	DO 880 I = 1, N	93215352
357 880	Z(I,R) = 0.0	93215353
358 C		93215354
359	DO 900 I = P, Q	93215355
360 900	Z(I,R) = RV6(I) * XU	93215356
361 C		93215357
362	X0 = X1	93215358
363 920	CONTINUE	93215359
364 C		93215360
365 940	IF (Q .LT. N) GO TO 100	93215361
366	GO TO 1001	93215362
367 C	***** SET ERROR -- NON-CONVERGED EIGENVECTOR *****	93215363
368 960	IERR = 4 * N + R	93215364
369	GO TO 1001	93215365
370 C	***** SET ERROR -- UNDERESTIMATE OF NUMBER OF	93215366
371 C	EIGENVALUES IN INTERVAL *****	93215367
372 980	IERR = 3 * N + 1	93215368
373 1001	LB = T1	93215369
374	UB = T2	93215370
375	RETURN	93215371
376 C	***** LAST CARD OF TSTURM *****	93215372
377	END	93215373

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1 C          77215001
2 C          -----77215002
3 C          77215003
4 SUBROUTINE TRED1(NM,N,A,D,E,E2) 77215004
5 C*MS:MATHLIB:NATS:EISPACK:SOURCE:TRED1 TRED1.F2.V2:11-28/73 LLL2
6 C          77215005
7 INTEGER I,J,K,L,N,II,NM,JP1 77215006
8 REAL A(NM,N),D(N),E(N),E2(N) 77215007
9 REAL F,G,H,SCALE 77215008
10 C REAL SQRT,ABS,SIGN LLL25009
11 C          77215010
12 C THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE TRED1, 77215011
13 C NUM. MATH. 11, 181-195(1968) BY MARTIN, REINSCH, AND WILKINSON. 77215012
14 C HANDBOOK FOR AUTO. COMP., VOL.11-LINEAR ALGEBRA, 212-226(1971). 77215013
15 C          77215014
16 C THIS SUBROUTINE REDUCES A REAL SYMMETRIC MATRIX 77215015
17 C TO A SYMMETRIC TRIDIAGONAL MATRIX USING 77215016
18 C ORTHOGONAL SIMILARITY TRANSFORMATIONS. 77215017
19 C          77215018
20 C ON INPUT- 77215019
21 C          77215020
22 C NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL 77215021
23 C ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM 77215022
24 C DIMENSION STATEMENT, 77215023
25 C          77215024
26 C N IS THE ORDER OF THE MATRIX, 77215025
27 C          77215026
28 C A CONTAINS THE REAL SYMMETRIC INPUT MATRIX. ONLY THE 77215027
29 C LOWER TRIANGLE OF THE MATRIX NEED BE SUPPLIED. 77215028
30 C          77215029
31 C ON OUTPUT- 77215030
32 C          77215031
33 C A CONTAINS INFORMATION ABOUT THE ORTHOGONAL TRANS- 77215032
34 C FORMATIONS USED IN THE REDUCTION IN ITS STRICT LOWER 77215033
35 C TRIANGLE. THE FULL UPPER TRIANGLE OF A IS UNALTERED. 77215034
36 C          77215035
37 C D CONTAINS THE DIAGONAL ELEMENTS OF THE TRIDIAGONAL MATRIX, 77215036
38 C          77215037
39 C E CONTAINS THE SUBDIAGONAL ELEMENTS OF THE TRIDIAGONAL 77215038
40 C MATRIX IN ITS LAST N-1 POSITIONS. E(1) IS SET TO ZERO, 77215039
41 C          77215040
42 C E2 CONTAINS THE SQUARES OF THE CORRESPONDING ELEMENTS OF E. 77215041
43 C E2 MAY COINCIDE WITH E IF THE SQUARES ARE NOT NEEDED. 77215042
44 C          77215043
45 C QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW. 77215044
46 C APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY 77215045
47 C          LLL1
48 C LLL CONSULTANT... R. P. DICKINSON LLL1
49 C VERSION 2 = CORRECT DECLARATIONS FOR PUTT LLL2
50 C          77215046
51 C          -----77215047
52 C          77215048
53 DO 100 I = 1, N 77215049
54 100 D(I) = A(I,I) 77215050
55 C ***** FOR J=N STEP -1 UNTIL 1 DO -- ***** 77215051
56 DO 300 II = 1, N 77215052
57 I = N + II - 1 77215053
58 L = I - 1 77215054
59 H = 0.0 77215055
60 SCALE = 0.0 77215056
61 IF (L .GT. 1) GO TO 130 77215057
62 C ***** SCALE ROW (ALGOL TOL THEN NOT NEEDED) ***** 77215058
63 DO 120 K = 1, L 77215059
64 120 SCALE = SCALE + ABS(A(I,K)) 77215060

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65	C			77215061
66		IF (SCALE .NE. 0.0) GO TO 140		77215062
67	130	E(1) = 0.0		77215063
68		E(2)) = 0.0		77215064
69		GO TO 290		77215065
70	C			77215066
71	140	DO 150 K = 1, L		77215067
72		A(I,K) = A(I,K) / SCALE		77215068
73		H = H + A(I,K) * A(I,K)		77215069
74	150	CONTINUE		77215070
75	C			77215071
76		E2(1) = SCALE * SCALE * H		77215072
77		F = A(I,L)		77215073
78		G = -SIGN(SQRT(H),F)		77215074
79		E(1) = SCALE * G		77215075
80		H = H - F * G		77215076
81		A(I,L) = F - G		77215077
82		IF (L .EQ. 1) GO TO 270		77215078
83		F = 0.0		77215079
84	C			77215080
85		DO 240 J = 1, L		77215081
86		G = 0.0		77215082
87	C	***** FORM ELEMENT OF A*U *****		77215083
88		DO 180 K = 1, J		77215084
89	180	G = G + A(J,K) * A(I,K)		77215085
90	C			77215086
91		JP1 = J + 1		77215087
92		IF (L .LT. JP1) GO TO 220		77215088
93	C			77215089
94		DO 200 K = JP1, L		77215090
95	200	G = G + A(K,J) * A(I,K)		77215091
96	C	***** FORM ELEMENT OF P *****		77215092
97	220	E(J) = G / H		77215093
98		F = F + E(J) * A(I,J)		77215094
99	240	CONTINUE		77215095
100	C			77215096
101		H = F / (H + H)		77215097
102	C	***** FORM REDUCED A *****		77215098
103		DO 260 J = 1, L		77215099
104		F = A(I,J)		77215100
105		G = E(J) - H * F		77215101
106		E(J) = G		77215102
107	C			77215103
108		DO 260 K = 1, J		77215104
109		A(J,K) = A(J,K) - F * E(K) - G * A(I,K)		77215105
110	260	CONTINUE		77215106
111	C			77215107
112	270	DO 280 K = 1, L		77215108
113	280	A(I,K) = SCALE * A(I,K)		77215109
114	C			77215110
115	290	H = D(1)		77215111
116		D(1) = A(I,1)		77215112
117		A(I,1) = H		77215113
118	300	CONTINUE		77215114
119	C			77215115
120		RETURN		77215116
121	C	***** LAST CARD OF TRED1 *****		77215117
122		END		77215118

1	SUBROUTINE BSTURM(N1,K1,IC1,IFLAG,XL,XU,D,E,E2)	BSTU	0
2	C*NMS:MATHL:B:NATS:EISPACK:SOURCE:BSTURM	BSTURM E1.V2	10/09/73
3	C	LLL2	10
4	INTEGER N1,K1,IC1,IFLAG	BSTU	20
5	REAL XL,XU, MACHEP	LLL1	30
6	REAL D(N1),E(N1),E2(N1)	LLL1	40
7	C	LLL1	50
8	C	BSTU	60
9	C	-----	BSTU 70
10	C	BSTU	80
11	C	BSTURM CALCULATES AN INTERVAL FOR A REAL SYMMETRIC TRIDIAGONAL	BSTU 90
12	C	MATRIX. THIS INTERVAL WILL CONTAIN AT LEAST A SPECIFIED NUMBER OF	BSTU 100
13	C	SMALLEST OR LARGEST EIGENVALUES, WHICHEVER IS DESIRED.	BSTU 110
14	C	THE POSSIBILITY OF GAINING MORE EIGENVALUES THAN DESIRED IN THE	BSTU 120
15	C	INTERVAL IS CAUSED BY CERTAIN EIGENVALUES HAVING MULTIPLICITIES	BSTU 130
16	C	GREATER THAN ONE.	BSTU 140
17	C	THIS SUBROUTINE CAN ALSO BE USED TO EVALUATE THE STURM COUNT FOR	BSTU 150
18	C	ANY REAL NUMBER, WHERE THE STURM COUNT IS THE NUMBER OF	BSTU 160
19	C	EIGENVALUES, COUNTING MULTIPLICITIES, STRICTLY TO THE LEFT OF THE	BSTU 170
20	C	GIVEN INPUT NUMBER.	BSTU 180
21	C	BSTU	190
22	C	BSTURM WAS DESIGNED TO SUPPLEMENT THE EISPACK PACKAGE.	BSTU 200
23	C	THIS SUBROUTINE WAS WRITTEN AT LAWRENCE LIVERMORE LABORATORY	BSTU 210
24	C	DURING AUGUST 1973 BY ROBERT DICKINSON OF N.M.S.	BSTU 220
25	C	BSTU	230
26	C	-----	BSTU 240
27	C	BSTU	250
28	C	ON INPUT:	BSTU 260
29	C	BSTU	270
30	C	N1 IS THE ORDER OF THE MATRIX A.	BSTU 280
31	C	BSTU	290
32	C	K1 IS THE NUMBER OF EXTREME EIGENVALUES DESIRED, IF IFLAG IS 2	BSTU 300
33	C	OR 3.	BSTU 310
34	C	BSTU	320
35	C	IFLAG MAY HAVE THREE VALUES.	BSTU 330
36	C	IF IFLAG IS 1 THE USER WANTS THE STURM COUNT AT THE INPUT	BSTU 340
37	C	VALUE XL.	BSTU 350
38	C	IF IFLAG IS 2 THE USER WANTS AN INTERVAL WHICH CONTAINS	BSTU 360
39	C	THE K1 SMALLEST EIGENVALUES OF A.	BSTU 370
40	C	IF IFLAG IS 3 THE USER WANTS AN INTERVAL WHICH CONTAINS	BSTU 380
41	C	THE K1 LARGEST EIGENVALUES OF A.	BSTU 390
42	C	BSTU	400
43	C	XL IS AN INPUT NUMBER IF IFLAG IS 1, AND IN THIS CASE THE	BSTU 410
44	C	NUMBER OF EIGENVALUES, COUNTING MULTIPLICITIES, STRICTLY TO	BSTU 420
45	C	THE LEFT OF XL IS TO BE COMPUTED.	BSTU 430
46	C	BSTU	440
47	C	D IS A LINEAR ARRAY OF DIMENSION N1 WHICH CONTAINS THE	BSTU 450
48	C	DIAGONAL ELEMENTS OF A. D(I)=A(I,I) FOR I=1 THROUGH N1.	BSTU 460
49	C	BSTU	470
50	C	E IS A LINEAR ARRAY OF DIMENSION N1 WHICH CONTAINS THE	BSTU 480
51	C	SUBDIAGONAL ELEMENTS OF A. E(I)=0, AND E(I)=A(I,I-1) FOR	BSTU 490
52	C	I=2 THROUGH N1.	BSTU 500
53	C	BSTU	510
54	C	E2 IS A LINEAR ARRAY OF DIMENSION N1 WHICH CONTAINS THE SQUARES	BSTU 520
55	C	OF ELEMENTS OF THE E ARRAY. THAT IS E2(I)=E(I)*E(I) FOR I=1	BSTU 530
56	C	THROUGH N1.	BSTU 540
57	C	BSTU	550
58	C	ON OUTPUT:	BSTU 560
59	C	BSTU	570
60	C	XL AND XU ARE THE LOWER AND UPPER ENDPOINTS, RESPECTIVELY, OF	BSTU 580
61	C	THE DESIRED INTERVAL IF THE INPUT VALUE OF IFLAG IS 2 OR 3.	BSTU 590
62	C	BSTU	600
63	C	IC1 IS THE STURM COUNT IF THE INPUT VALUE OF IFLAG IS 1.	BSTU 610
64	C	IC1 IS THE NUMBER OF EIGENVALUES IN THE INTERVAL IF THE INPUT	BSTU 620
		BSTU	630

65 C	VALUE OF IFLAG IS 2 OR 3.	BSTU 640
66 C		BSTU 650
67 C	IFLAG IS SET TO 0 IF THERE WERE NO ERRORS IN INPUT PARAMETERS;	BSTU 660
68 C	OTHERWISE IFLAG IS SET TO -1.	BSTU 670
69 C	NOTE.. IFLAG IS ALWAYS AN INTEGER.	BSTU 680
70 C		BSTU 690
71 C	LLL CONSULTANT... R. P. DICKINSON	BSTU 700
72 C		BSTU 710
73 C	-----	BSTU 720
74 C	LATEST REVISION - OCTOBER 9, 1973	LLL2 730
75 C	VERSION 2 = CHANGES FOR ANSI AND NMS STANDARDS -- F.N.F.	LLL2 740
76 C		BSTU 750
77 C	***** FPER GUARANTEES THAT BSTURN WILL RETURN AN	BSTU 751
78 C	INTERVAL OF NONZERO LENGTH.	BSTU 752
79	DATA ISET/0/, FPER/.01/	LLL2 760
80	KFLAG=IFLAG	BSTU 770
81	IF((KFLAG.LT.1).OR.(KFLAG.GT.3)) GO TO 30	LLL2 780
82	IF(ISET.NE.0) GO TO 2	LLL2 790
83 C		BSTU 800
84 C	***** MACHEP IS A MACHINE DEPENDENT PARAMETER SPECIFYING	BSTU 810
85 C	THE RELATIVE PRECISION OF FLOATING POINT ARITHMETIC.	BSTU 820
86 C		BSTU 830
87 C	*****	BSTU 840
88	MACHEP=2.**(-47)	BSTU 850
89 C	***** RMACHEP = 1./MACHEP *****	BSTU 860
90	RMACHEP=2.**(47)	BSTU 870
91	ISET=1	BSTU 880
92 C		BSTU 890
93	2 N=N1	BSTU 900
94	K=K1	BSTU 910
95	IF(N.LE.1) GO TO 30	LLL2 920
96	E2(1)=E(1)=0.	LLL2 930
97	DO 3 I=2,N	LLL2 940
98	IF(ABS(E(I)).GT.MACHEP*(ABS(D(I))+ABS(D(I-1)))) GO TO 3	LLL2 950
99	E2(I)=0.	LLL2 960
100	3 CONTINUE	LLL2 970
101	IF(KFLAG.NE.1) GO TO 12	BSTU1036
102	IPAS=1	BSTU1040
103	XC=XL	BSTU1050
104	5 IC=0	LLL21060
105	DO 10 I=1,N	BSTU1070
106	IF(E2(I).NE.0.) GO TO 7	LLL21080
107	U=D(I)-XC	LLL21090
108	IF(U.LT.0.) IC=IC+1	LLL21100
109	GO TO 10	LLL21110
110	7 IF(U.NE.0.) GO TO 8	LLL21120
111	V=ABS(E(I))*RMACHEP	LLL21130
112	GO TO 9	LLL21140
113	8 V=E2(I)/U	LLL21150
114	9 U=D(I)-XC-V	LLL21160
115	IF(U.LT.0.) IC=IC+1	LLL21170
116	10 CONTINUE	BSTU1180
117	GO TO (11,14,20),IPAS	BSTU1190
118	11 IFLAG=1	BSTU1200
119	IC=IC	BSTU1210
120	RETURN	BSTU1220
121 C		BSTU1230
122	12 IF((K.LT.1).OR.(K.GT.N)) GO TO 30	LLL21240
123 C	***** CALCULATE GERSHGORIN BOUNDS *****	BSTU1250
124	XT=ABS(E(N))	BSTU1260
125	XL1=D(N)-XT	BSTU1270
126	XU1=D(N)+XT	BSTU1280
127	NM1=N-1	BSTU1285
128	DO 13 I=1,NM1	BSTU1290

129	XT=ABS(E(1))+ABS(L(1+1))	LLL21300
130	XL2=D(1)-XT	LLL21310
131	XU2=D(1)+XT	LLL21320
132	IF(XL2.LT.XL) XL1=XL2	LLL21330
133	IF(XU2.GT.XU) XU1=XU2	LLL21340
134	13 CONTINUE	BSTU1350
135 C	***** EVALUATE UPPER COUNT *****	BSTU1360
136	XC=XU1	BSTU1370
137	IPAS=2	BSTU1380
138	GO TO 5	LLL21390
139	14 IPAS=3	BSTU1400
140	ICU=IC	BSTU1410
141	ICL=0	BSTU1420
142	IFLAG=0	BSTU1430
143	IF(KFLAG.NE.2) GO TO 17	LLL21440
144	XL=AMINI(XL1-FPER*ABS(XL1),-FPER)	LLL21450
145	EPS1=AMAX1(ABS(XL),ABS(XU1))*MACHEP	BSTU1455
146	ITEST=K	BSTU1460
147	IF(K.LT.IC) GO TO 19	LLL21470
148	XU=AMAX1(XU1+FPER*ABS(XU1),FPER)	LLL21480
149	IC=N	BSTU1490
150	RETURN	BSTU1500
151 C		BSTU1510
152	17 XU=AMAX1(XU1+FPER*ABS(XU1),FPER)	BSTU1520
153	EPS1=AMAX1(ABS(XL1),ABS(XU1))*MACHEP	BSTU1525
154	ITEST=N-K	BSTU1530
155	IF((N-IC).LT.K) GO TO 19	LLL21540
156	XL=XU1	LLL21550
157	IC=N-IC	BSTU1550
158	RETURN	BSTU1570
159 C		BSTU1580
160	19 XC=(XL)+XU1)*.5	BSTU1590
161	GO TO 5	BSTU1600
162	20 IF((XU1-XL1).LE.(2.*MACHEP*(ABS(XU1)+ABS(XL1))+EPS1)) GO TO 24	BSTU1610
163	IF(IC.LE.ITEST) GO TO 22	LLL21620
164	XU1=XC	LLL21630
165	ICU=IC	BSTU1640
166	GO TO 19	BSTU1650
167	22 IF(IC.GE.ITEST) GO TO 27	LLL21660
168	XL1=XC	LLL21670
169	ICL=IC	BSTU1680
170	GO TO 19	BSTU1690
171	24 IF(KFLAG.NE.2) GO TO 26	LLL21700
172	XU=XU1	LLL21710
173	IC1=ICU	BSTU1720
174	RETURN	BSTU1730
175 C		BSTU1740
176	26 XL=XL1	BSTU1750
177	IC1=N-ICL	BSTU1760
178	RETURN	BSTU1770
179 C		BSTU1780
180	27 IF(KFLAG.NE.2) GO TO 29	LLL21790
181	XU=XC	LLL21800
182	IC1=IC	BSTU1810
183	RETURN	BSTU1820
184 C		BSTU1830
185	29 XL=XC	BSTU1840
186	IC1=N-IC	BSTU1850
187	RETURN	BSTU1860
188 C		BSTU1870
189 C	***** ERROR RETURN *****	BSTU1880
190	30 IFLAG=-1	BSTU1890
191	RETURN	BSTU1900
192 C	***** LAST CARD OF BSTURN *****	BSTU1910

BSTU1920

I END

1 C		79215001
2 C	-----	79215002
3 C		79215003
4	SUBROUTINE TRBAK1(NM,N,A,E,M,Z)	79215004
5 C	*NMS:MATHLIB:NATS:EISPACK:SOURCE:TRBAK1	TRBAK1 E2.V1 09/19/73 LLL1
6 C		79215005
7	INTEGER I,J,K,L,M,N,NM	79215006
8	REAL A(NM,N),E(N),Z(NM,M)	79215007
9	REAL H,S	79215008
10 C		79215009
11 C	THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE TRBAK1,	79215010
12 C	NUM. MATH. 11, 181-195(1968) BY MARTIN, REINSCH, AND WILKINSON.	79215011
13 C	HANDBOOK FOR AUTO. COMP., VOL.11-LINEAR ALGEBRA, 212-226(1971).	79215012
14 C		79215013
15 C	THIS SUBROUTINE FORMS THE EIGENVECTORS OF A REAL SYMMETRIC	79215014
16 C	MATRIX BY BACK TRANSFORMING THOSE OF THE CORRESPONDING	79215015
17 C	SYMMETRIC TRIDIAGONAL MATRIX DETERMINED BY TRED1.	79215016
18 C		79215017
19 C	ON INPUT-	79215018
20 C		79215019
21 C	NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL	79215020
22 C	ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM	79215021
23 C	DIMENSION STATEMENT,	79215022
24 C		79215023
25 C	N IS THE ORDER OF THE MATRIX.	79215024
26 C		79215025
27 C	A CONTAINS INFORMATION ABOUT THE ORTHOGONAL TRANS-	79215026
28 C	FORMATIONS USED IN THE REDUCTION BY TRED1	79215027
29 C	IN ITS STRICT LOWER TRIANGLE.	79215028
30 C		79215029
31 C	E CONTAINS THE SUBDIAGONAL ELEMENTS OF THE TRIDIAGONAL	79215030
32 C	MATRIX IN ITS LAST N-1 POSITIONS. E(1) IS ARBITRARY.	79215031
33 C		79215032
34 C	M IS THE NUMBER OF EIGENVECTORS TO BE BACK TRANSFORMED.	79215033
35 C		79215034
36 C	Z CONTAINS THE EIGENVECTORS TO BE BACK TRANSFORMED	79215035
37 C	IN ITS FIRST M COLUMNS.	79215036
38 C		79215037
39 C	ON OUTPUT-	79215038
40 C		79215039
41 C	Z CONTAINS THE TRANSFORMED EIGENVECTORS	79215040
42 C	IN ITS FIRST M COLUMNS.	79215041
43 C		79215042
44 C	NOTE THAT TRBAK1 PRESERVES VECTOR EUCLIDEAN NORMS.	79215043
45 C		79215044
46 C	QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW,	79215045
47 C	APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY	79215046
48 C		LLL1
49 C	LLL CONSULTANT... R. P. DICKINSON	LLL1
50 C		79215047
51 C	-----	79215048
52 C		79215049
53	IF (N .EQ. 1) GO TO 200	79215050
54 C		79215051
55	DO 140 I = 2, N	79215052
56	L = I - 1	79215053
57 C	***** H BELOW IS NEGATIVE OF H FORMED IN TRED1 *****	79215054
58	H = E(I) * A(I,L)	79215055
59	IF (H .EQ. 0.0) GO TO 140	79215056
60 C		79215057
61	DO 130 J = 1, M	79215058
62	S = 0.0	79215059
63 C		79215060
64	DO 110 K = 1, L	79215061

65	110	S = S + A(I,K) * Z(K,J)	79215062
66	C		79215063
67		S = S / H	79215064
68	C		79215065
69		DO 120 K = 1, L	79215066
70	120	Z(K,J) = Z(K,J) + S * A(I,K)	79215067
71	C		79215068
72	130	CONTINUE	79215069
73	C		79215070
74	140	CONTINUE	79215071
75	C		79215072
76	200	RETURN	79215073
77	C	***** LAST CARD OF TRBAK: *****	79215074
78		END	79215075

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1 SUBROUTINE QSF (H,Y,Z,NDIM)
2 C
3 C
4 C
5 C SUBROUTINE QSF
6 C
7 C PURPOSE
8 C TO COMPUTE THE VECTOR OF INTEGRAL VALUES FOR A GIVEN
9 C EQUIDISTANT TABLE OF FUNCTION VALUES.
10 C
11 C USAGE
12 C CALL QSF (H,Y,Z,NDIM)
13 C
14 C DESCRIPTION OF PARAMETERS
15 C H - THE INCREMENT OF ARGUMENT VALUES.
16 C Y - THE INPUT VECTOR OF FUNCTION VALUES.
17 C Z - THE RESULTING VECTOR OF INTEGRAL VALUES. Z MAY BE
18 C IDENTICAL WITH Y.
19 C NDIM - THE DIMENSION OF VECTORS Y AND Z.
20 C
21 C REMARKS
22 C NO ACTION IN CASE NDIM LESS THAN 3.
23 C
24 C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
25 C NONE
26 C
27 C METHOD
28 C BEGINNING WITH Z(1)=0, EVALUATION OF VECTOR Z IS DONE BY
29 C MEANS OF SIMPSONS RULE TOGETHER WITH NEWTONS 3/8 RULE OR A
30 C COMBINATION OF THESE TWO RULES. TRUNCATION ERROR IS OF
31 C ORDER H**5 (I.E. FOURTH ORDER METHOD). ONLY IN CASE NDIM=3
32 C TRUNCATION ERROR OF Z(2) IS OF ORDER H**4.
33 C FOR REFERENCE, SEE
34 C (1) F.B.HILDEBRAND, INTRODUCTION TO NUMERICAL ANALYSIS,
35 C MCGRAW-HILL, NEW YORK/TORONTO/LONDON, 1956, PP.71-76.
36 C (2) R.ZURMUEHL, PRAKTIISCHE MATHEMATIK FUER INGENIEURE UND
37 C PHYSIKER, SPRINGER, BERLIN/GOETTINGEN/HEIDELBERG, 1963,
38 C PP.214-221.
39 C
40 C
41 C
42 C
43 C
44 DIMENSION Y(1),Z(1)
45 C
46 HT=.33333333*H
47 IF(NDIM-5)7,B,1
48 C
49 C NDIM IS GREATER THAN 5. PREPARATIONS OF INTEGRATION LOOP
50 I SUM1=Y(2)+Y(2)
51 SUM1=SUM1+SUM1
52 SUM1=HT*(Y(1)+SUM1+Y(3))
53 AUX1=Y(4)+Y(4)
54 AUX1=AUX1-.5X1
55 AUX1=SUM1+HT*(Y(3)+AUX1+Y(5))
56 AUX2=HT*(Y(1)+3.875*(Y(2)+Y(5))+2.625*(Y(3)+Y(4))+Y(6))
57 SUM2=Y(5)+Y(5)
58 SUM2=SUM2+SUM2
59 SUM2=AUX2-HT*(Y(4)+SUM2+Y(6))
60 Z(1)=0.
61 AUX=Y(3)+Y(3)
62 AUX=AUX+AUX
63 Z(2)=SUM2-HT*(Y(2)+AUX+Y(4))
64 Z(3)=SUM1

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65     Z(4)=SUM2
66     IF (NDIM-6)5,5,2
67 C
68 C     INTEGRATION LOOP
69     2 DO 4 I=7,NDIM,2
70     SUM1=AUX1
71     SUM2=AUX2
72     AUX1=Y(I)-)))+Y(I)-1))
73     AUX1=AUX1+AUX1
74     AUX1+SUM1+HT*(Y(I-2)+AUX1+Y(I))
75     Z(I-2)=SUM1
76     IF (I-NDIM)3,6,6
77     3 AUX2=Y(I)+Y(I)
78     AUX2=AUX2+AUX2
79     AUX2=SUM2+HT*(Y(I-1)+AUX2+Y(I+1))
80     4 Z(I-1)=SUM2
81     5 Z(NDIM-1)=AUX1
82     Z(NDIM)=AUX2
83     RETURN
84     6 Z(NDIM-1)=SUM2
85     Z(NDIM)=AUX1
86     RETURN
87 C     END OF INTEGRATION LOOP
88 C
89     7 IF (NDIM-3)12,11,8
90 C
91 C     NDIM IS EQUAL TO 4 OR 5
92     8 SUM2=1.125+HT*(Y(1)+Y(2)+Y(2)+Y(2)+Y(3)+Y(3)+Y(3)+Y(4))
93     SUM1=Y(2)+Y(2)
94     SUM1=SUM1+SUM1
95     SUM1=HT*(Y(1)+SUM1+Y(3))
96     Z(1)=0.
97     AUX1=Y(3)+Y(3)
98     AUX1=AUX1+AUX1
99     Z(2)=SUM2-HT*(Y(2)+AUX1+Y(4))
100    IF (NDIM-5)10,9,9
101    9 AUX1=Y(4)+Y(4)
102    AUX1=AUX1+AUX1
103    Z(5)=SUM1+HT*(Y(3)+AUX1+Y(5))
104    10 Z(3)=SUM1
105    Z(4)=SUM2
106    RETURN
107 C
108 C     NDJM IS EQUAL TO 3
109    11 SUM1=HT*(1.25+Y(1)+Y(2)+Y(2)-.25*Y(3))
110    SUM2=Y(2)+Y(2)
111    SUM2=SUM2+SUM2
112    Z(3)=HT*(Y(1)+SUM2+Y(3))
113    Z(1)=0.
114    Z(2)=SUM1
115    12 RETURN
116    END

```

```

1 SUBROUTINE PLOTS(Y,M,NF,NSX)
2 DIMENSION Y(5,100), LINE(101),L(11),JL(5)
3 DATA JL(1), JL(2), JL(3), JL(4), JL(5)
4 I
5 /IHA,IHB,IHC,IHD,IHE/,JN,JP,JI,JBLANK,JZ/
6 I1H-,I1H+,I1I,I1H-,I1H+/
7 NS=NSX
8 WRITE(6,45)
9 45 FORMAT (I1I)
10 IF (NS.NE.999) GO TO 95
11 NS=100
12 DO 70 J=1,M
13 YMAX=-1.E+50
14 YMIN=1.E+50
15 DO 55 I=1,NF
16 IF (Y(J,I).GT.YMAX) YMAX=Y(J,I)
17 IF (Y(J,I).LT.YMIN) YMIN=Y(J,I)
18 55 CONTINUE
19 RANGE=YMAX-YMIN
20 TEMP=100./RANGE
21 DO 60 I=1,NF
22 Y(J,I)=(Y(J,I)-YMIN)*TEMP
23 WRITE (6, 65) JL(J), YMIN, YMAX, RANGE
24 65 FORMAT (IX,5HPLOT ,A1,5H FROM,E10.3,3H TO,
25 I E10.3,9H, RANGE =,E10.3)
26 70 CONTINUE
27 WRITE (6, 75)
28 75 FORMAT ( )
29 95 DO 99 I=1,101
30 LINE(I)=JBLANK
31 99 CONTINUE
32 N=0
33 DO 101 I=1,11
34 L(I)=10*I-110+NS
35 101 CONTINUE
36 WRITE (6, 105) (L(I), I = 1, 11)
37 105 FORMAT (3X,11(14,6X),6HY(1,1))
38 GO TO 115
39 110 IF (N/10-(N-1)/10) 125,125,115
40 115 ND=0
41 DO 120 I=1,10
42 ND=ND+1
43 LINE(ND)=JP
44 DO 120 J=1,9
45 ND=ND+1
46 120 LINE(ND)=JN
47 LINE(101)=JP
48 IF (N) 135,121,135
49 121 WRITE (6, 170) N, LINE
50 GO TO 185
51 125 DO 130 I=1,101,10
52 LINE(I)=JI
53 130 CONTINUE
54 135 DO 160 I=1,M
55 XNS=NS
56 JA=Y(1,N)+101.49999-XNS
57 IF (JA-101) 140,155,145
58 140 IF (JA) 150,150,155
59 145 LINE(101)=JZ
60 GO TO 160
61 150 LINE(I)=JZ
62 GO TO 160
63 155 LINE(JA)=JL(I)
64 160 CONTINUE
65 IF (N/10-(N-1)/10) 175,175,165

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65	165 WRITE (6, 170) N, LINE, Y(1, N)	
66	170 FORMAT (1X,14,101A1,1X, E12.5)	HUELSMAN
67	GO TO 185	HUELSMAN
68	175 WRITE (6, 180) LINE, Y(1, N)	
69	180 FORMAT (5X,101A1,1X,E12.5)	HUELSMAN
70	185 DO 190 J=1,101	HUELSMAN
71	LINE(J)=JBLANK	HUELSMAN
72	190 CONTINUE	HUELSMAN
73	195 N=N+1	HUELSMAN
74	IF (N-NF) 110,110,200	HUELSMAN
75	200 RETURN	HUELSMAN
76	END	HUELSMAN

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1      SUBROUTINE LFILON (TZERO,T,FT,FTA,NT,F,FFZERO,FF,NF,B,IND,ITF)
2 C
3 C
4 C THIS SUBROUTINE PERFORMS THE FOURIER TRANSFORM EITHER FROM TIME TO FREQUENCY
5 C OR FREQUENCY TO TIME. LIMITATIONS ARE THAT THE TIME FUNCTION MUST BE REAL
6 C AND THE TIME FUNCTION MUST BE CAUSAL.
7 C
8 C DESCRIPTION OF ARGUMENTS
9 C
10 C    TZERO - INITIAL VALUE OF TIME. THE CORRESPONDING FUNCTION OF TIME IS
11 C          SET TO ZERO BY THE SUBROUTINE
12 C
13 C    T      - ARRAY CONTAINING TIME VALUES IN ASCENDING ORDER
14 C
15 C    FT     - ARRAY CONTAINING FUNCTION OF TIME VALUES (REAL)
16 C
17 C    FTA    - ADDITIONAL ARRAY CONTAINING FUNCTION OF TIME VALUES. USED
18 C          ONLY IN FREQUENCY TO TIME MODE
19 C
20 C    NT     - NUMBER OF TIME POINTS, EXCLUDING TZERO
21 C
22 C    F      - ARRAY CONTAINING FREQUENCY VALUES IN ASCENDING ORDER
23 C
24 C    FFZERO - FUNCTION OF FREQUENCY VALUE (COMPLEX) AT ZERO FREQUENCY
25 C
26 C    FF     - ARRAY (COMPLEX) CONTAINING FUNCTION OF FREQUENCY VALUES
27 C
28 C    NF     - NUMBER OF FREQUENCY POINTS, EXCLUSIVE OF ZERO FREQUENCY POINT
29 C          ASSOCIATED WITH FFZERO
30 C
31 C    B      - AUXILIARY ARRAY USED INTERNALLY ONLY BUT DIMENSIONED IN MAIN
32 C          PROGRAM
33 C
34 C    IND    - AUXILIARY ARRAY USED INTERNALLY ONLY BUT DIMENSIONED IN MAIN
35 C          PROGRAM
36 C
37 C    ITF    - INTEGER INDICATOR SELECTING EITHER TIME TO FREQUENCY OR
38 C          FREQUENCY TO TIME TRANSFORM
39 C
40 C
41 C TO USE SUBROUTINE FOR TIME TO FREQUENCY TRANSFORM, PERFORM THE FOLLOWING
42 C IN THE MAIN PROGRAM --
43 C
44 C    1) SET ITF TO 1
45 C    2) SET NT AND NF TO NUMBER OF TIME POINTS AND NUMBER OF FREQUENCY
46 C       POINTS RESPECTIVELY
47 C    3) DIMENSION T, FT, AND B WITH VALUE OF NT (FTA IS NOT USED AND MAY
48 C       BE DIMENSIONED 1)
49 C    4) NAME FFZERO, FF, AND B, AS COMPLEX
50 C    5) DIMENSION F, FF, AND IND WITH VALUE OF NF
51 C    6) SUPPLY VALUES FOR TZERO, T, FT, NT, F, NF, AND ITF. SUBROUTINE WILL
52 C       RETURN FFZERO AND FF VALUES
53 C
54 C TO USE SUBROUTINE FOR FREQUENCY TO TIME TRANSFORM, PERFORM FOLLOWING IN
55 C MAIN PROGRAM --
56 C
57 C    1) SET ITF TO 0
58 C    2) SET NT AND NF TO NUMBER OF TIME POINTS AND NUMBER OF FREQUENCY
59 C       POINTS, RESPECTIVELY
60 C    3) DIMENSION T, FT, FTA, AND IND WITH VALUE OF NT
61 C    4) NAME FFZERO, FF, AND B COMPLEX
62 C    5) DIMENSION F, FF, AND B WITH VALUE OF NF
63 C    6) SUPPLY VALUES FOR T, NT, F, FFZERO, FF, NF, AND ITF. SUBROUTINE
64 C       WILL RETURN FT AND FTA VALUES. THE TRANSFORM IS COMPUTED TWO WAYS.

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65 C      FT CONTAINS THE RESULT OF THE TRANSFORM USING THE REAL PART OF FF
66 C      MULTIPLIED BY COSINE OF RADIAN FREQUENCY TIMES TIME.  FTA CONTAINS
67 C      THE RESULT OF THE TRANSFORM USING THE IMAGINARY PART OF FF MULTIPLIED
68 C      BY SINE OF RADIAN FREQUENCY TIMES TIME.  USER SHOULD CHECK FOR
69 C      CORRESPONDENCE OF THE TWO ANSWERS
70 C
71 C
72      DIMENSION T(1),FT(1),F(1),FF(1),B(1),IND(1),FTA(1)
73      COMPLEX FF,1,FSTORE,B,FFZERO,TSTORE
74      TOP1 = 6.283185308
75      I = CMPLX(0.,1.)
76      IF (ITF .EQ. 0) GO TO 303
77 C      TIME TO FREQUENCY TRANSFORM
78 C      DO LINEAR SEARCH FOR NUMBER TO DIVIDE TRAPAZOIDAL FROM FILONS METHOD
79      NTP = NT - 1
80      DO 51 M = 1,NF
81      TAU = .1 / F(M)
82      N = 1
83      IF (TAU .LT. TZERO) GO TO 1
84      DO 41 N = 1,NT
85      IF (TAU .LT. T(N)) GO TO 1
86      41 CONTINUE
87      IND(M) = NT
88      GO TO 51
89      I IND(M) = N - 1
90      51 CONTINUE
91      61 CONTINUE
92      10 FORMAT (E15.5,110)
93 C      COMPUTE COEFFICIENTS
94      B(1) = (FT(2) - FT(1)) / (T(2) - T(1)) - FT(1) / (T(1) - TZERO)
95      B(NT) = (FT(NTP) - FT(NT)) / (T(NT) - T(NTP))
96      DO 11 N = 2,NTP
97      NP = N + 1
98      NL = N - 1
99      B(N) = (FT(NP) - FT(N)) / (T(NP) - T(N)) - (FT(N) - FT(NL)) / (T(N)
100      I ) - T(NL))
101      11 CONTINUE
102 C      COMPUTE TRANSFORM
103      FFZERO = FT(1) * (T(2) - TZERO)
104      DO 81 N = 2,NTP
105      NP = N + 1
106      NL = N - 1
107      81 FFZERO = FFZERO + FT(N) * (T(NP) - T(NL))
108      FFZERO = FFZERO + FT(NT) * (T(NT) - T(NTP))
109      FFZERO = FFZERO / 2.
110      DO 21 M = 1,NF
111      W = TOP1 * F(M)
112 C      COMPUTE TRAPAZOIDAL PORTION
113      INDM = IND(M)
114      INDMM = INDM - 1
115      INDMP = INDM + 1
116      FSTORE = CMPLX(0.,0.)
117      IF (INDMM 5,2,6
118      5 FF(M) = FT(1) * CEXP(-1 * W * T(1)) * (T(2) - TZERO)
119      IF (INDM .EQ. 2) GO TO 3
120      DO 71 N = 2,INDMM
121      NP = N + 1
122      NL = N - 1
123      FF(M) = FF(M) + FT(N) * CEXP(-1 * W * T(N)) * (T(NP) - T(NL))
124      71 CONTINUE
125      FF(M) = FF(M) + FT(INDM) * CEXP(-1 * W * T(INDM)) * (T(INDM) -
126      I T(INDMM))
127      GO TO 4
128      3 FF(M) = FF(M) + FT(2) * CEXP(-1 * W * T(2)) * (T(2) - T(1))

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129 GO TO 4
130 2 FF(M) = FT(1) * CEXP(-1 * W * T(1)) * (T(1) - TZERO)
131 4 FF(M) = FF(M) / 2.
132 C COMPUTE FILON PORTION
133 IF (IND(M) .EQ. NT) GO TO 21
134 FSTORE = FF(M)
135 FF(M) = FT(INDM) * CEXP(-1 * W * (T(INDM) - TZERO)) * 1 *
136 1 W - FT(NT) * CEXP(-1 * W * (T(NT) - TZERO)) * 1 * W + ((FT(INDMP)
137 2 - F(T(INDM))) / (T(INDMP) - T(INDM))) * CEXP(-1 * W * (T(INDM) -
138 3 TZERO))
139 GO TO 7
140 5 FF(M) = FT(1) / (T(1) - TZERO) - FT(NT) * CEXP(-1 * W * (T(NT) -
141 1 TZERO)) * 1 * W
142 7 CONTINUE
143 DO 21 N = INDMP,NT
144 31 FF(M) = FF(M) + B(N) * CEXP(-1 * W * (T(N) - TZERO))
145 FF(M) = -FF(M) * CEXP(-1 * W * TZERO) / (W * W) + FSTORE
146 21 CONTINUE
147 RETURN
148 C FREQUENCY TO TIME TRANSFORM
149 303 CONTINUE
150 C DO LINEAR SEARCH FOR NUMBER TO DIVIDE TRAPAZOIDAL FROM FILON
151 DO 151 N = 1,NT
152 TAU = .1 / T(N)
153 M = 1
154 IF (TAU .LT. 0.) GO TO 101
155 DO 141 M = 1,NF
156 IF (TAU .LT. F(M)) GO TO 101
157 141 CONTINUE
158 IND(N) = NF
159 GO TO 151
160 101 IND(N) = M - 1
161 151 CONTINUE
162 C COMPUTE COEFFICIENTS
163 NTP = NF - 1
164 B(1) = (FF(2) - FF(1)) / (F(2) - F(1)) - (FF(1) - FF(ZERO)) / F(1)
165 B(NF) = (FF(NTP) - FF(NF)) / (F(NF) - F(NTP))
166 DO 111 M = 2,NTP
167 NP = M + 1
168 NL = M - 1
169 B(M) = (FF(NP) - FF(M)) / (F(NP) - F(M)) - (FF(M) - FF(NL)) / (F(M)
170 1) - F(NL))
171 111 CONTINUE
172 C COMPUTE TRANSFORM
173 DO 121 N = 1,NT
174 C COMPUTE TRAPAZOIDAL PORTION
175 INDM = IND(N)
176 INDMM = INDM - 1
177 INDMP = INDM + 1
178 TSTORE = CMPLX(0.,0.)
179 IF (INDMM) 105,102,106
180 106 FT(N) = REAL(FF(ZERO)) * F(1) + REAL(FF(1)) * COS(TOP) * F(1) * T(N)
181 1) * F(2)
182 FTA(N) = AIMAG(FF(1)) * SIN(TOP) * F(1) * T(N) * F(2)
183 IF (INDM .EQ. 2) GO TO 103
184 DO 171 M = 2,INDMM
185 NP = M + 1
186 NL = M - 1
187 FT(N) = FT(N) + REAL(FF(M)) * COS(TOP) * F(M) * T(N) * (F(NP) -
188 1 F(NL))
189 FTA(N) = FTA(N) + AIMAG(FF(M)) * SIN(TOP) * F(M) * T(N) * (F(NP)
190 1 - F(NL))
191 171 CONTINUE
192 FT(N) = FT(N) + REAL(FF(INDM)) * COS(TOP) * F(INDM) * T(N) *

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193      1 (F(IJNDM) - F(IJNDMM))
194      FTA(N) = FTA(N) + AIMAG(FF(IJNDM)) * SIN(TOP) * F(IJNDM) * T(N) *
195      1 (F(IJNDM) - F(IJNDMM))
196      GO TO 104
197 103 FT(N) = FT(N) + REAL(FF(2)) * COS(TOP) * F(2) * T(N) * (F(2) - F(
198      1 1))
199      FTA(N) = FTA(N) + AIMAG(FF(2)) * SIN(TOP) * F(2) * T(N) * (F(2) -
200      1 F(1))
201      GO TO 104
202 102 FT(N) = (REAL(FFZERO) + REAL(FF(1)) * COS(TOP) * F(1) * T(N)) *
203      1 F(1)
204      FTA(N) = AIMAG(FF(1)) * SIN(TOP) * F(1) * T(N) * F(1)
205 104 FT(N) = FT(N) * 2.
206      FTA(N) = -FTA(N) * 2.
207 C    COMPUTE FILON PORTION
208      IF (IIND(N) .EQ. NF) GO TO 121
209      TSTORE = CMPLX(FT(N),FTA(N))
210      FT(N) = (REAL(FF(IJNDMP) - FF(IJNDM)) / (F(IJNDMP) - F(IJNDM))) * COS
211      1 (TOP) * F(IJNDM) * T(N) - TOP * T(N) * (REAL(FF(NF)) * SIN(TOP)
212      2 * F(NF) * T(N) - REAL(FF(IJNDM)) * SIN(TOP) * F(IJNDM) * T(N))
213      FTA(N) = (AIMAG(FF(IJNDMP) - FF(IJNDM)) / (F(IJNDMP) - F(IJNDM))) *
214      1 SIN(TOP) * F(IJNDM) * T(N) + TOP * T(N) * (AIMAG(FF(NF)) * COS
215      2 (TOP) * F(NF) * T(N) - AIMAG(FF(IJNDM)) * COS(TOP) * F(IJNDM) *
216      3 T(N))
217      GO TO 107
218 105 FT(N) = REAL(FF(1) - FFZERO) / F(1) - TOP * T(N) * REAL(FF(NF)) *
219      1 SIN(TOP) * F(NF) * T(N)
220      FTA(N) = TOP * T(N) * (AIMAG(FF(NF)) * COS(TOP) * F(NF) * T(N)
221      1 - AIMAG(FFZERO))
222 107 CONTINUE
223      DO 131 M = IJNDP,NF
224      FT(N) = FT(N) + REAL(B(M)) * COS(TOP) * F(M) * T(N)
225 131 FTA(N) = FTA(N) + AIMAG(B(M)) * SIN(TOP) * F(M) * T(N)
226      FT(N) = -4. * FT(N) / (TOP * TOP * T(N) * T(N)) + REAL(TSTORE)
227      FTA(N) = 4. * FTA(N) / (TOP * TOP * T(N) * T(N)) + AIMAG(TSTORE)
228 121 CONTINUE
229      RETURN
230      END

```