

9-20-77
27
ASB/TIS

MASTER

UCID. 17564

Lawrence Livermore Laboratory

MULTIGROUP CONSTANTS FOR CHARGED PARTICLE ELASTIC NUCLEAR (PLUS INTERFERENCE)
SCATTERING OF LIGHT ISOTOPES

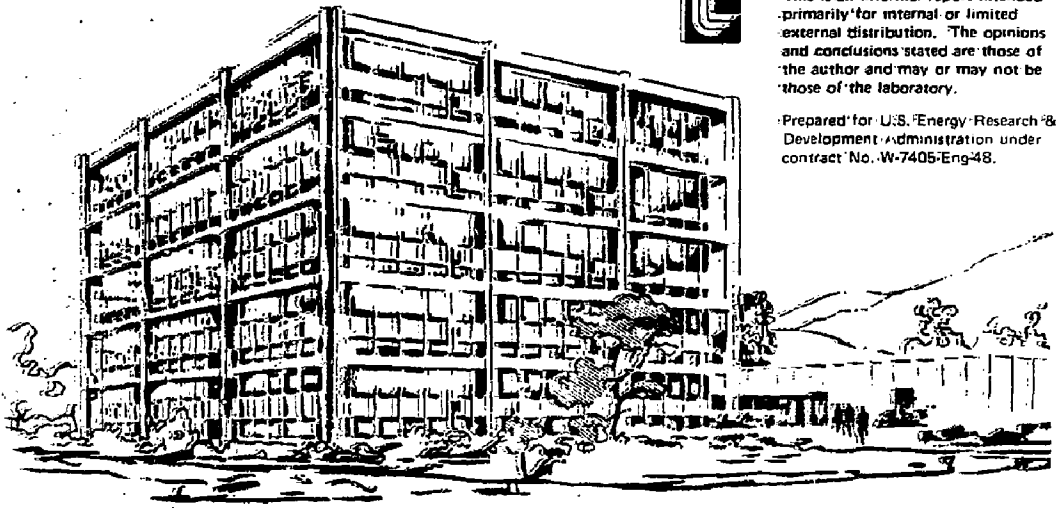
D. E. Cullen and S. T. Perkins

August 26, 1977



This is an informal report intended primarily for internal or limited external distribution. The opinions and conclusions stated are those of the author and may or may not be those of the laboratory.

Prepared for U.S. Energy Research & Development Administration under contract No. W-7405-Eng-48.



DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

MULTIGROUP CONSTANTS FOR CHARGED PARTICLE ELASTIC NUCLEAR
(PLUS INTERFERENCE) SCATTERING OF LIGHT ISOTOPES

TABLE OF CONTENTS

	<u>Page</u>
Abstract	3
Introduction	3
Multi-Group Definitions	4
Corrections for Finite Material Temperature	9
Group Structure	10
Weighting Spectrum	10
Data Base	13
Calculational Capabilities	15
Results	16
References	22

NOTICE
This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Energy Research and Development Administration, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or timeliness of any information, opinions, products or processes disclosed, or represents that its use would not infringe privately owned rights.

MULTIGROUP CONSTANTS FOR CHARGED PARTICLE ELASTIC NUCLEAR
(PLUS INTERFERENCE) SCATTERING OF LIGHT ISOTOPES

Abstract

Multi-group averaged reaction rates and transfer matrices have been calculated for charged particle induced elastic nuclear (plus interference) scattering. Results are presented using a ten group structure for all twenty-five permutations of projectile and target for the following charged particles: p, d, t, ^3He and α . Transfer matrices are presented in a simplified form for both incident projectile and the knock-ons; these matrices explicitly conserve energy.

Introduction

The objective of this study was to produce multi-group averaged reactions rates $\langle \sigma(E)W \rangle$ and simplified transfer matrices to describe both the slowing down of the projectiles and the energy gain of the knock-ons. The charged particle induced nuclear (plus interference) scattering from the ENDL¹ library was used for this purpose. Group averaged reaction rates were defined in the normal manner. The transfer matrix for the incident particle includes only up to two final groups (the source group and one other). The final groups and their transition probabilities are selected to give the scattered projectiles the correct secondary energy distribution. Similarly, the transfer matrix for the knock-ons includes only up to two final groups (the thermal sea and one other). Again, the final groups and their transition probabilities are selected to give the knock-on particle

exactly the energy lost by the projectile slowing down. With this simplified scheme, the correct average secondary energy and an energy balance is guaranteed.

Multi-Group Definitions

The group-averaged quantities calculated are:

1.) The group-averaged reaction rate

$$\langle \sigma(E) \nu \rangle_g = \frac{\int_{E_g}^{E_{g+1}} \nu \sigma(E) n(E) dE}{\int_{E_g}^{E_{g+1}} n(E) dE} \quad (1)$$

2.) The group-averaged secondary energy

$$\begin{aligned} \langle E' \rangle_g &= \frac{\int_{E_g}^{E_{g+1}} E' \nu \sigma(E) n(E) dE}{\int_{E_g}^{E_{g+1}} \nu \sigma(E) n(E) dE} \\ &= \frac{\int_{E_g}^{E_{g+1}} [E - D(E)] \nu \sigma(E) n(E) dE}{\int_{E_g}^{E_{g+1}} \nu \sigma(E) n(E) dE} \\ &= \langle E \rangle_g - \langle D(E) \rangle_g \end{aligned} \quad (2)$$

where

$\nu \sigma(E)$ - reaction rate

$D(E)$ - average energy loss per collision

$n(E)$ - number density weighting spectrum.

The group averaged reaction rate was calculated for each group. The secondary energy was used to define the average secondary group and transition probability. Relative to the center of each energy group the effective energy loss is given by

$$\langle D'(E) \rangle_g = \frac{1}{2} (E_{g+1} + E_g) - \langle E' \rangle_g \quad (3)$$

Note that the effective energy loss $\langle D'(E) \rangle_g$ is only equal to the energy loss $\langle D(E) \rangle_g$ if the average energy of a collision $\langle E \rangle_g$ is equal to the average energy of the group $[\frac{1}{2} (E_{g+1} + E_g)]$. Usually $\langle D'(E) \rangle_g$ is close to $\langle D(E) \rangle_g$ except near the threshold of a reaction. Near the threshold, in order to reproduce the correct probability of scattering out of the group, it is important to use the correct averaged secondary energy $\langle E' \rangle_g$ and effective energy loss $\langle D'(E) \rangle_g$, as opposed to defining the secondary energy by subtracting the energy loss $\langle D(E) \rangle_g$ from the group averaged energy $[\frac{1}{2} (E_{g+1} + E_g)]$.

The selection of the average secondary group was simply based upon which group the averaged secondary energy $\langle E' \rangle_g$ fell into. The transition probability was introduced in order to exactly conserve the effective energy loss $\langle D'(E) \rangle_g$.

Allowing for two final groups for either the projectile or knock-on and explicitly conserving the effective energy loss we have the two equations

$$\langle D'(E) \rangle_g = \Delta_{g \rightarrow g'} f_{g \rightarrow g'} + \Delta_{g \rightarrow g''} f_{g \rightarrow g''} \quad (4)$$

$$1 = f_{g \rightarrow g'} + f_{g \rightarrow g''}$$

where

$\langle D'(E) \rangle_g$ - effective energy loss

$f_{g \rightarrow g'}$ - transition probability from group g to g'

$\Delta_{g \rightarrow g'}$ - absolute value of energy change due to transition from group g to g'

$$= |1/2(E_{g+1} + E_g) - 1/2(E_{g'+1} + E_{g'})|$$

Once the two final groups g' and g'' have been selected, $\Delta_{g \rightarrow g'}$ and $\Delta_{g \rightarrow g''}$ are known and it is possible to uniquely solve for the transition probabilities,

$$f_{g \rightarrow g''} = \frac{\Delta_{g \rightarrow g'} - \langle D'(E) \rangle_g}{\Delta_{g \rightarrow g'} - \Delta_{g \rightarrow g''}} \quad (5)$$

$$f_{g \rightarrow g'} = \frac{\langle D'(E) \rangle_g - \Delta_{g \rightarrow g''}}{\Delta_{g \rightarrow g'} - \Delta_{g \rightarrow g''}} \quad (6)$$

These transition probabilities will be physically acceptable (i.e., both in the range 0 to 1) if g' and g'' are selected such that,

$$\Delta_{g \rightarrow g'} \geq \langle D'(E) \rangle_g > \Delta_{g \rightarrow g''} \quad (7)$$

The most accurate treatment is obtained by selecting g'' and g' such that they are adjacent groups (i.e., $g' = g'' \pm 1$) and energy loss or gain terms straddle the effective energy loss,

$$\Delta_{g \rightarrow g'' \pm 1} \geq \langle D'(E) \rangle_g > \Delta_{g \rightarrow g''} \quad (8)$$

However, in the present calculations one of the two final groups was defined to be the initial group (i.e., $g'' \equiv g$) for both the projectile and knock-on.

In this case, for the projectile a fraction of the particles are transferred to a final group and the remainder stay in the source group. The average energy loss is then given by

$$\langle D''(E) \rangle_g = 0f_{g \rightarrow g} + \Delta_{g \rightarrow g'} f_{g \rightarrow g'}$$

where

$f_{g \rightarrow g}$ - fraction remaining in group g

$f_{g \rightarrow g'}$ - fraction transferring to group g'

$\Delta_{g \rightarrow g'}$ - energy loss due to transfer from group g to g'
 $= \left| \frac{1}{2}(E_{g+1} + E_g) - \frac{1}{2}(E_{g'+1} + E_{g'}) \right|$

$\langle D''(E) \rangle_g$ - effective energy loss .

In the multi-group approximation there is no energy loss due to a scattering that remains in group g . The group g' is selected as the nearest group to g in which

$$\Delta_{g \rightarrow g'} \geq \langle D''(E) \rangle_g \quad (10)$$

The transition probabilities are then defined as

$$f_{g \rightarrow g'} = \langle D''(E) \rangle_g / \Delta_{g \rightarrow g'} \leq 1 \quad (11)$$

$$f_{g \rightarrow g} = 1 - f_{g \rightarrow g'} \quad (12)$$

For the target a fraction of the particles are transferred to a final group and the remainder stay in the thermal sea. The average energy gain is then

$$\langle D'(E) \rangle_g = 0f_{0 \rightarrow 0} + \Delta_{0 \rightarrow g''} f_{0 \rightarrow g''} \quad (13)$$

where

$f_{0 \rightarrow 0}$ - fraction remaining in the thermal sea

$f_{0 \rightarrow g''}$ - fraction transferring to group g''

$\Delta_{0 \rightarrow g''}$ - energy gain due to transfer from thermal sea to group g''

$$= \frac{1}{2} (E_{g''+1} + E_{g''})$$

$\langle D'(E) \rangle_g$ - effective energy loss .

The group g'' is selected as the lowest energy group in which

$$\Delta_{0 \rightarrow g''} \geq \langle D'(E) \rangle_g \quad (14)$$

The transition probabilities are then defined as

$$f_{0 \rightarrow g''} = \langle D'(E) \rangle_g / \Delta_{0 \rightarrow g''} \leq 1 \quad (15)$$

$$f_{0 \rightarrow 0} = 1 - f_{0 \rightarrow g''} \quad (16)$$

The above conventions guarantee energy conservation since the projectile average energy loss and the target average energy gain are both exactly equal to the effective energy loss $\langle D'(E) \rangle_g$.

Only one special convention had to be adopted to use the above scheme. In the group containing the reaction threshold it is possible to have the average secondary energy $\langle E' \rangle_g$ be greater than the group averaged energy $[\frac{1}{2} (E_{g+1} + E_g)]$. In this case the effective energy loss $\langle D'(E) \rangle_g$ is negative. This indicates there is little or no probability of scattering out of the group. In this case by convention the final

group is defined to be equal to the initial group ($g' = g; g'' = 0$) and the transition probabilities are defined as unity ($f_{g \rightarrow g} = 1, f_{0 \rightarrow 0} = 1$). Again, energy is conserved.

Corrections for Finite Material Temperature

In the case where the projectiles are interacting with a hot media, the energy loss is decreased, which should affect the transfer matrices. A simple approximate method of accounting for this effect is available.² The average energy loss should be modified as follows,

$$\langle \widetilde{D(E)}_g \rangle = \langle D(E) \rangle_g - \frac{1-\alpha}{2} E_A \tag{17}$$

where

$\langle \widetilde{D(E)}_g \rangle$ - Hot group averaged energy loss

$\langle D(E) \rangle_g$ - Cold group averaged energy loss

$$\alpha = [(A_p - A_T) / (A_p + A_T)]^2$$

A_p - Atomic weight of projectile

A_T - Atomic weight of target

E_A - $\frac{3}{2} kT$ - Average ion temperature of the media

Then re-define the hot average secondary energy, E'_g (2), as

$$\langle \widetilde{E}' \rangle_g = \langle E \rangle_g - \langle \widetilde{D(E)} \rangle_g = \langle E' \rangle_g + \frac{1-\alpha}{2} E_A \tag{18}$$

which in turn defines the hot effective energy loss, E''_g (3),

$$\langle \widetilde{D''(E)} \rangle_g = \frac{1}{2} (E_{g+1} + E_g) - \langle \widetilde{E}' \rangle_g = \langle D'(E) \rangle_g - \frac{1-\alpha}{2} E_A \tag{19}$$

This may then be used with the simple algorithm presented (see the previous section) directly in any application code to simply and inexpensively define the final group and transition probabilities for both the projectile and the knock-ons.

Group Structure

A ten group structure was used.

<u>Number</u>	<u>Lower energy limit-MeV</u>	<u>Average Energy-MeV</u>
1	0.	0.0015
2	0.003	0.0165
3	0.03	0.09
4	0.15	0.375
5	0.50	1.35
6	2.00	3.50
7	4.80	6.02
8	7.24	8.62
9	10.00	12.00
10	14.0	14.05
	14.1	

In addition, by convention the group index 0 is used to denote the thermal sea, in which by assumption, the average energy is 0.0.

Weighting Spectrum

The flux weighting spectrum was based on continuous slowing down due to Coulomb scattering only,³

$$\phi(E) \approx \frac{1}{\frac{\partial E}{\partial S}} \approx \frac{1}{v \frac{\partial E}{\partial t}} \approx \frac{v}{\frac{Y}{E^{1/2}} + \frac{E}{t_e}} \quad (20)$$

where the energy loss terms are due to,

$$\frac{Y}{E^{1/2}} = \text{ions}$$

$$\frac{E}{t_e} = \text{electrons.}$$

Upon multiplying through and eliminating a constant factor, the flux is given by

$$\phi(E) = \frac{E}{\gamma t_e + E^{3/2}} \quad (21)$$

Since it is reaction rate averages that will be defined, it is the number density, not the flux, that should be used as the weighting spectrum.

The number density is simply given by

$$n(E) = \frac{1}{v} \phi(E) \approx \frac{E^{1/2}}{\gamma t_e + E^{3/2}}$$

where

$$\gamma t_e = 1.09514 Z^2 A^{1/2} \frac{\rho}{\langle A_i \rangle} \left\langle \frac{Z_i^2}{A_i} \right\rangle L_i \times 51.8155 (kT_e)^{3/2} \times \quad (22)$$

$$\frac{A \langle A_i \rangle}{Z^2 \langle Z_i \rangle \rho L_e} \quad (\text{Mev}^{3/2}).$$

In this expression Z and A refer to the projectile slowing down, $\rho, Z_i,$ and A_i refer to the plasma, L_i and L_e are the Coulomb logs and kT_e is the electron temperature.

A good approximation is

$$\frac{L_i}{L_e} \sim 1.5,$$

and for a DT plasma (i.e. plasma averages atom fraction weighted over all ion constituents).

$$\langle Z \rangle = 1$$

$$\langle A \rangle = 2.5$$

$$\left\langle \frac{Z^2}{A} \right\rangle = .417.$$

Therefore,

$$yt_e = 35.5 (kT_e A)^{3/2}. \quad (\text{eV}^{3/2}) \quad (23)$$

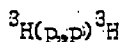
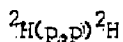
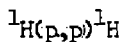
Use of a variety of electron temperatures between 10 and 100 Kev illustrated that the resulting group averages are fairly insensitive to the value of kT_e selected. Therefore, 10 Kev was used in all cases; thus, the number density weighting function used is given by

$$n(E) = \frac{E^{1/2}}{0.0355A^{3/2} + E^{3/2}}. \quad (24)$$

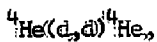
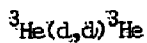
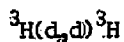
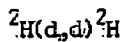
Data Base

The ENDL¹ library of evaluated nuclear data contains angular distributions and integrated parameters for charged particle induced nuclear (plus interference) scattering over the laboratory energy range 0-20 Mev. Only low atomic weight charged particles are included in the library; specifically, only reactions in which the projectile and target include p, d, t, ³He and α. By convention, the ENDL library only explicitly contains data for projectiles which are equal to or lighter than the target. Therefore, the data actually contained in the ENDL library includes.

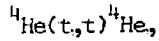
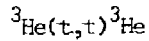
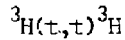
(1) proton induced



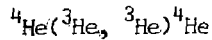
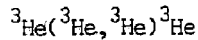
(2) deuteron induced



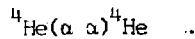
(3) triton induced



(4) ${}^3\text{He}$ induced



(5) alpha induced



The data for the remaining combinations obtained by interchanging projectile and target (e.g. ${}^4\text{He}(p,p){}^4\text{He} \rightarrow {}^1\text{H}(\alpha,\alpha){}^1\text{H}$) can be exactly derived from the data for the above reactions by simple energy transformations.

The data from EMDL that was used to obtain group averages was the charged particle induced nuclear (plus interference) scattering reaction rate ($V\sigma(E)$) and energy loss ($D(E)$). The data in EMDL corresponds to interaction with a cold (nominally 0°K) medium. In order to obtain finite reaction rates by integrating angular distributions, a cut-off of 20° (cosine of .94) was used.

Data for reactions obtained by interchanging projectile and target are obtained by realizing that the reactions will be identical for the same relative speed between particles; i.e.,

$$E_2 = \left(\frac{A_2}{A_1}\right) E_1 \quad ,$$

where A_1 and A_2 are the atomic weights of the projectile and target, respectively. Therefore, the required reaction rate is given by

$$V_2 \sigma(E_2) = V_1 \sigma(E_1) \quad (V_2 = V_1), \quad (25)$$

and the energy deposit by

$$D(E_2) = \left(\frac{A_2}{A_1}\right) D(E_1) \quad (26)$$

Calculational Capabilities

The results presented in this report were obtained using the CPGROUP⁴ code. This code is capable of calculating charged particle induced group averaged reaction rates and two element transfer matrices for both projectile and knock-ons. The calculation can be performed using any weighting function and up to 400 groups.

The CLYDE⁵ code is presently capable of calculating charged particle induced group averaged reaction rates and the complete transfer matrix for the slowing down of the projectile. Only minor modifications to CLYDE would be required to include calculation of the complete knock-on transfer matrix. Therefore, if a more complete treatment than that presented herein is required for any application, contact the authors.

Results

The following tables present the ten group results. Results are grouped by incident projectile in increasing Z, A order; p,d,t, ^3He and α . For each incident projectile, results are presented in increasing target Z, A order; ^1H , ^2H , ^3H , ^3He and ^4He . All energies are in MeV. The meaning of each column read left to right is:

- TARGET - Z, A of target in the form 1000x Z + A
(e.g., 2004 - ^4He)
- GR - Group index (group 1 is the lowest energy group and group 0 is the ion thermal sea).
- GROUP-Mev - Lower energy limit of the group. For completeness the upper energy limit of the last group is also presented.
- REACTIONS - Group averaged reaction rate in units⁶ of barn x cm/shake
- E - Average reaction energy in group.
- E' - Average secondary energy
- E - E' - Average energy loss
- EGROUP-E'' - Effective energy loss (relative to the middle of the group)
- PROJECTILE - Final group index and transition probability for the scattered projectile.
- TARGET - Final group index and transition probability for the knock-ons.

ALPHA INDUCED REACTIONS

TARGET	OR GROUP-HEV	REACTIONS	E	E	E-E	EGROUP-E	PROJECTILE	TARGET
0001	OR-UNRESAN-1	0000	1506E-01	8264E-01	6416E-01	3236E-01	E-UNRESAN	0000
0002		0000	6171E-01	4267E-01	1889E-01	4266E-01		0000
0003		0000	4111E-01	1267E-01	3241E-01	6149E-01		0000
0004		0000	3000E-01	1000E-01	4267E-01	3178E-01		0000
0005		0000	2000E-01	1000E-01	4267E-01	3178E-01		0000
0006		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0007		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0008		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0009		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0010		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0011	OR-UNRESAN-2	0000	1506E-01	8264E-01	6416E-01	3236E-01	E-UNRESAN	0000
0012		0000	6171E-01	4267E-01	1889E-01	4266E-01		0000
0013		0000	4111E-01	1267E-01	3241E-01	6149E-01		0000
0014		0000	3000E-01	1000E-01	4267E-01	3178E-01		0000
0015		0000	2000E-01	1000E-01	4267E-01	3178E-01		0000
0016		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0017		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0018		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0019		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0020		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0021	OR-UNRESAN-3	0000	1506E-01	8264E-01	6416E-01	3236E-01	E-UNRESAN	0000
0022		0000	6171E-01	4267E-01	1889E-01	4266E-01		0000
0023		0000	4111E-01	1267E-01	3241E-01	6149E-01		0000
0024		0000	3000E-01	1000E-01	4267E-01	3178E-01		0000
0025		0000	2000E-01	1000E-01	4267E-01	3178E-01		0000
0026		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0027		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0028		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0029		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0030		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0031	OR-UNRESAN-4	0000	1506E-01	8264E-01	6416E-01	3236E-01	E-UNRESAN	0000
0032		0000	6171E-01	4267E-01	1889E-01	4266E-01		0000
0033		0000	4111E-01	1267E-01	3241E-01	6149E-01		0000
0034		0000	3000E-01	1000E-01	4267E-01	3178E-01		0000
0035		0000	2000E-01	1000E-01	4267E-01	3178E-01		0000
0036		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0037		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0038		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0039		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0040		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0041	OR-UNRESAN-5	0000	1506E-01	8264E-01	6416E-01	3236E-01	E-UNRESAN	0000
0042		0000	6171E-01	4267E-01	1889E-01	4266E-01		0000
0043		0000	4111E-01	1267E-01	3241E-01	6149E-01		0000
0044		0000	3000E-01	1000E-01	4267E-01	3178E-01		0000
0045		0000	2000E-01	1000E-01	4267E-01	3178E-01		0000
0046		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0047		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0048		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0049		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0050		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0051	OR-UNRESAN-6	0000	1506E-01	8264E-01	6416E-01	3236E-01	E-UNRESAN	0000
0052		0000	6171E-01	4267E-01	1889E-01	4266E-01		0000
0053		0000	4111E-01	1267E-01	3241E-01	6149E-01		0000
0054		0000	3000E-01	1000E-01	4267E-01	3178E-01		0000
0055		0000	2000E-01	1000E-01	4267E-01	3178E-01		0000
0056		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0057		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0058		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0059		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000
0060		0000	1000E-01	1000E-01	4267E-01	3178E-01		0000

References

1. S. T. Perkins, D. E. Cullen, and R. J. Howerton, ENDL Evaluated Charged Particle Cross Sections for Light Isotopes, UCRL-50400, Vol. 15, Part D, Lawrence Livermore Laboratory, (to be published).
2. S. T. Perkins, Approximate Material Temperature and Boundary Motion Corrections for Local Energy Deposition Due to Elastic Scattering, Lawrence Livermore Laboratory, Report No. UCID-17533 (1977).
3. E. G. Corman, W. E. Loewe, G. E. Cooper, and A. M. Winslow, Nucl. Fusion 15, 377 (1975).
4. D. E. Cullen, Program CPGROUP: Calculation of Charged Particle Induced Reaction Rates and Transfer Matrices, Lawrence Livermore Laboratory, (internal code).
5. R. J. Doyas, et al., CLYDE, A Code for the Production of Calculational Constants from Nuclear Data, Report No. UCRL-50400, Vol. 5, Rev. 1, (1975), Lawrence Livermore Laboratory.
6. 1 Shake = 10^{-8} Seconds.

NOTICE

This report was prepared as an account of work sponsored by the United States Government. Neither the United States nor the United States Energy Research & Development Administration, nor any of their employees, nor any of their contractors, subcontractors, or their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness or usefulness of any information, apparatus, product or process disclosed; or represents that its use would not infringe privately-owned rights.

NOTICE

Reference to a company or product name does not imply approval or recommendation of the product by the University of California or the U.S. Energy Research & Development Administration to the exclusion of others that may be suitable.

Printed in the United States of America
 Available from
 National Technical Information Service
 U.S. Department of Commerce
 5285 Port Royal Road
 Springfield, VA 22161
 Price: Printed Copy \$ Microfiche \$3.00

Page Range	Domestic Price	Page Range	Domestic Price
001-025	\$ 3.50	326-350	10.00
026-050	4.00	351-375	10.50
051-075	4.50	376-400	10.75
076-100	5.00	401-425	11.00
101-125	5.50	426-450	11.75
126-150	6.00	451-475	12.00
151-175	6.75	476-500	12.50
176-200	7.50	501-525	12.75
201-225	7.75	526-550	13.00
226-250	8.00	551-575	13.50
251-275	9.00	576-600	13.75
276-300	9.25	601-up	"
301-325	9.75		

*Add \$2.50 for each additional 100 page increment from 601 to 1,000 pages;
 add \$4.50 for each additional 100 page increment over 1,000 pages.