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PLASMOR: A LASER-PLASMA SIMULATION CODE, II

D. Salzmann, A.D. Krümbeln and H. Szichman



**Israel Atomic Energy Commission**  
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PLASMOR: A LASER-PLASMA SIMULATION CODE, II

D. Salzmann, A.D. Krumbeln and H. Sziehman

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D. Salzmann, A.D. Krumbein and H. Szichman

## ABSTRACT

This report supplements a previous one<sup>(1)</sup> which describes the PLASMOR hydrodynamics code. The present report documents, the recent changes and additions made in the code. In particular described are two new subroutines, for radiative preheat, a system of preprocessors which prepares the code before run, a list of postprocessors which simulate experimental setups, and the basic data sets required to run PLASMOR. In the Appendix a new computer-based manual which lists the main features of PLASMOR is reproduced.

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## 1. INTRODUCTION

Two years have passed from the time that the first report describing the PLASMOR laser-plasma simulation code<sup>1</sup> was published. During this period the PLASMOR has grown from a relatively straightforward hydrodynamics code into a system of programs. It was felt, therefore, that it is the time to supplement the first report by a new one and to document the recent changes and additions made in the code.

The new features of PLASMOR can be divided into three groups: First, some new physics was introduced into the code. This includes the computation of the radiative preheat (which is partially reported also in I) and black-body radiation diffusion. Second, postprocessors were written to carry out additional calculations based on the main PLASMOR output. These postprocessors control the graphics output and simulate some of the experimental diagnostics measurements. These processors run mainly, but not only, on the IBM-PC computer. Finally, major changes of a more technical character were introduced into the code to simplify the handling, debugging and running of the PLASMOR code. The most important of these is the build-up of a manual of PLASMOR on the computer disc, which is supposed to be updated periodically (see below).

The recent changes in PLASMOR helped in reducing the program size and run time, by deleting, or moving to postprocessors, portions of the

program which are seldom used and are not essential for the solution of the hydrodynamic equations. In fact, the source program is reduced to 55% of its original size and the running time on a selected problem was reduced by 12%. The program work area was changed to be dimensionally variable according to the problem requirements (compared to the constant number of cells used heretofore).

## 2. GENERAL

The present version of the PLASMOR system can be divided into three main parts, see Fig. 1. These are, (a) Preprocessors, (b) the main hydrodynamics code, PLASMOR, and (c) Postprocessors. Each of these groups operates through its own data-bases, which are prepared by a series of auxiliary programs.

The separation of the preprocessors and the postprocessors from the main program greatly facilitates the running of the code. In fact, the use of the preprocessor provides an easy way to change the array dimensions in the common blocks and to reduce the source program, to about 55% of its original size. An immediate consequence is the reduction of the program working area, and a subsequent reduction of CPU-time.

The use of postprocessors, which simulate the experimental diagnostics, also helps in reducing the run time. The transfer of these routines from the main program to the postprocessors has two main effects on the program. First, they are used only when necessary, and secondly, "bugs" in these programs do not stop the execution of the main program.

In section 3 the new additions to PLASMOR are described as well as the structure of the PLASMOR data sets. Section 4 is devoted to the description of the preprocessors and in particular, the new PLASMOR manual. In section 5 the postprocessors are listed and described.

## 3. NEW FEATURES OF PLASMOR

This discussion concerning the new features of PLASMOR is divided into two parts viz. new routines in PLASMOR and a description of the data bases, which is not included in I.

### 3.1 New Routines in PLASMOR

#### 3.1.1 Radiation Preheat

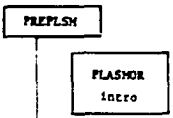
This routine has already been partially described in I. Here

CODES

DATA BASES

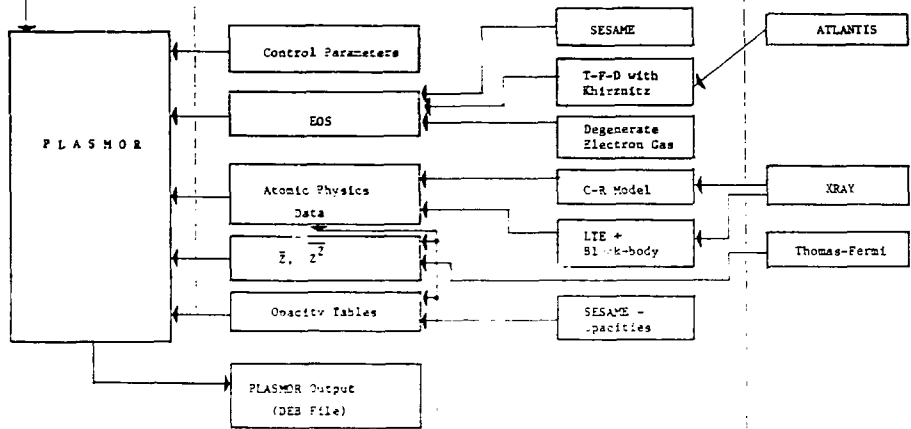
AUXILIARY

Preprocessor



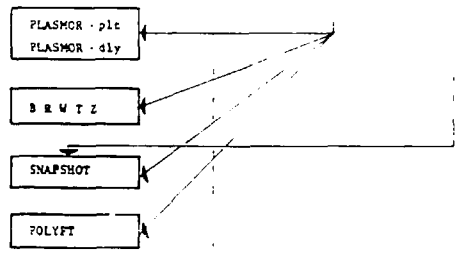
Main Code

→ data banks



Post - processors:

- (1) Graphics (PC)
- (2) Backsurface luminosity
- (3) X-ray emission spectrum
- (4) Shock wave velocity to the target



however, we give more detailed explanation.

Radiant energy arising in the corona can be absorbed in the target core resulting in the preheat of the colder portion of the target. This preheat may be especially important at low laser intensities where fast electron phenomena have not as yet come into play.

It is assumed that the plasma can be divided into two portions (see figure 2); a hot region which emits intense X-ray radiation, but is practically transparent to its own radiation, and a cold compressed region which strongly absorbs the incident radiation but has only faint black body radiation. A rather sharp boundary separates these regions.

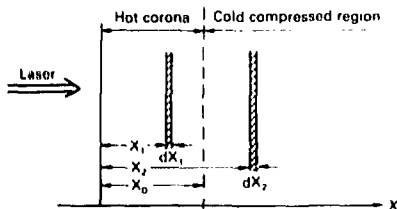


FIGURE 2. Schematic division of the plasma into hot and cold portions and visual aid for the parameter in formulas 1 to 3

Assuming planar symmetry, it can be shown that the total radiative energy absorbed in cell number k per unit time is given by

$$\bar{r}_k = 2\pi \int_0^{\alpha} d\omega \bar{I}(\omega) [E_2(\tau_k) - E_2(\tau_{k+1})] \quad (1)$$

where

$$\tau_k \equiv \tau(x_0; x_k; \omega) = \int_{x_0}^{x_k} n(x) n(x; \omega) dx \quad (2)$$

is the optical depth of cell k from the interface,

$$\bar{I}(\omega) = \int_0^{x_0} I(x; \omega) n(x) dx \quad (3)$$



is the total radiation flux from the hot region in the photon energy bin  $[\omega, \omega + d\omega]$  and  $E_2(y)$  is an exponential integral function of order 2. In (1) to (3),  $n(x)$  is the ion density,  $\sigma(x; \omega)$  is the photoabsorption cross section of photons having energy  $\omega$  at depth  $x$  in the target,  $x_0$  is the location of the interface between the hot and cold regions and  $I(x; \omega) dx$  is the emission rate from the infinite slab between  $x$  and  $x + dx$ . Equation (1) is the basic expression for the calculation of the radiation reabsorption.

It should be noted that (1) incorporates an integration over the isotropic photon emission, i.e., it does not assume a unidirectional photon propagation as other similar computer codes do. This integration is, in fact, the origin on the exponential integral in (1). See I for further explanations about the radiation preheat routines.

### 3.1.2 Black-body Radiation Diffusion

Incorporated in the program is the black body radiation diffusion in the cold substrate using the well-known expression for this process,

$$S = -\kappa(T) \nabla T \quad (4)$$

where the radiative conductivity is given by,

$$\kappa(T) = \frac{16}{3} l_R \sigma_{SB} T^3 \quad (5)$$

Here  $l_R$  is the Rosseland mean free path and  $\sigma_{SB}$  is the Stefan-Boltzmann factor. Equation 4 is incorporated into the energy equation in subroutine TEMPS in a manner similar to the electron heat conduction. The Rossland m.f.p. is read from the opacity tables (see below).

## 3.2 Data Bases

PLASMOR uses five sets of data bases, see Fig. 1. These are the control cards to run a problem, Equation-of-State (EOS) tables, Atomic Physics tables (DKR tables), average-Z and average  $Z^2$  tables and finally, when available, opacity tables (Rosseland m.f.p.).

### 3.2.1 Control Cards

The control cards are the main input cards to run the program. For a full description see Appendix A below.

### 3.2.2 EOS Tables

Three sources are available for the EOS used in PLASMOR.

(i) The earliest is a degenerate-electron-gas (Fermi-Dirac statistics) type EOS. This EOS turned out to be inadequate, except, perhaps, for a pure hydrogen high-temperature plasma. For other types of plasmas this EOS overestimates the plasma pressure and predicts compressions which are too high.

(ii) The SESAME-type EOS tables<sup>4</sup> developed in Los-Alamos, are available for a set of 32 materials, from Hydrogen to Uranium, including compounds and mixtures such as polyethylene, air, water and others. These tables list the pressure  $P$  and internal energy  $E$  as functions of the temperature and density of the plasma for  $0 \leq T \leq 10^8$  K and densities up to  $10^4$  times solid state density.

In spite of some inaccuracies that were found in some parameter regions, the SESAME tables are assumed to be very reliable and are frequently used world-wide. These tables are periodically updated by the Los-Alamos group and the new versions (which include new materials) are available on a commercial basis.

(iii) A set of high accuracy tables are available for aluminum<sup>5</sup>. This set was prepared by us using an auxiliary program ATLANTIS, and is explained in full in I. We hope to develop this method for other materials as well.

### 3.2.3 Atomic Physics Tables (DXR tables)

The content and the formulas for the preparations of these tables are explained in full in I. To date, tables are available for beryllium, carbon, oxygen, neon and aluminum.

In contrast to the EOS tables, PLASMOR can run without the DXR tables. In that case, the main inaccuracy in the result arises from neglecting the radiative cooling of the plasma. For high-Z plasmas this

omission may be important, but then a black-body emission mechanism can yield sufficient accuracy. Such an option however, is still not included in PLASMOR.

The DXR tables include, apart from the radiative cooling, also the emission rates of the various continuous-spectrum energy groups, the line emission rates,  $\bar{Z}$ ,  $\bar{Z}^2$ , total ionization energy and total photoabsorption cross-sections.

### 3.2.4 $\bar{Z}$ and $\bar{Z}^2$

The values of  $\bar{Z}$  and  $\bar{Z}^2$  are extensively used in PLASMOR for the calculation of the electron density and the local electron pressure in the plasma. Values of  $\bar{Z}$  and  $\bar{Z}^2$  are available from two sources:

(i) The DXR tables tabulate explicitly  $\bar{Z}$  and  $\bar{Z}^2$  on a mesh of temperatures and densities. The advantage of using these tables is the fact that the values of  $\bar{Z}$  and  $\bar{Z}^2$  are obtained from a Collisional-Radiative (CR) model, and are, therefore, more accurate for laser-plasmas than those obtained from other models.

(ii) For high-Z plasmas, where the Thomas-Fermi model is valid, a simple algorithm, developed by More<sup>6</sup>, can be used to yield reasonably accurate results.

### 3.2.5 Opacity Tables

Opacity tables are used only if radiation transport is calculated. These tables list the values of the Rosseland mean free path, which are required by Eq. (5).

Opacity tables are likewise available from the Los Alamos group on a commercial basis though not always for the same materials for which there are SESAME EOS tables. We have available for use in PLASMOR at present, opacities for Aluminum, titanium, iron, copper, CH<sub>2</sub> and SiO<sub>2</sub>.

## 4. PREPROCESSORS

### 4.1 The set PREPLSM

The common blocks of PLASMOR took up a significant portion of the source program. This resulted in an unnecessarily long program which was very difficult to handle. To illustrate this difficulty, it is enough to mention that to change a parameter in one of the common blocks which is

used throughout the program, becomes a "dangerous" task, nearly always accompanied by unavoidable bugs. It was therefore felt that a decoupling between the common blocks and the subroutines was necessary in order to make the program more flexible.

In the present version, the common blocks are located at the beginning of the MAIN program. The beginning of each block is tagged by \*CD NAME by where NAME is the name of the common block. The end of all the blocks is tagged by \*END. Each subroutine which uses a block includes a line \*CALL NAME. The program PREPLSM FORTRAN is used to substitute the relevant blocks into the calling subroutines. PREPLSM is applied to the source program, before compilation. The run time of PREPLSM is about 7 seconds.

The first block is \*CD PAR, which includes the PARAMETER statement through which one can assign variable values to the array dimensions. The two parameters: NCL (number of cells) and MIX-(number of DXR tables) define all the common block lengths. These variables should be set before the PLASMOR run.

The routine PREPLSM EXEC is a control file which carries out the following tasks:

- (i) runs PREPLSM
- (ii) compiles PLASMOR
- (iii) links PLASMOR
- (iv) erases extra unused files
- (v) runs PLASMOR

To run PLASMOR one has only type "PREPLSM" and the program carries out all the above commands in sequence. Care should be taken to update PREPLSM FILEDEF when necessary.

#### 4.2 PLASMOR MANUAL

The PLASMOR MANUAL is intended to provide an updated manual to facilitate running PLASMOR.

The PLASMOR MANUAL data set is stored on the computer disc and includes a list of the central properties of PLASMOR.

The following data are included in PLASMOR MANUAL:

- (i) Subroutines - a list of the subroutines, divided into categories of their function and numbered according to their use and calling sequence. The subroutines in the code are arranged according to the same order.
- (ii) I/O units - list of the I/O units and the data sets linked to them
- (iii) Common block- list and short definition of the variables in the various common blocks. This portion of the manual should be of the greatest help to the user.
- (iv) Input cards - list, definition and format of the input cards required to run PLASMOR. Significant changes were entered into the input cards since the publication of I.

We intend to update PLASMOR MANUAL whenever new features are introduced into the code. In this way we end up with a manual which can be easily changed and is always updated.

An updated printout of the PLASMOR MANUAL is given in Appendix A.

#### 4.3 The set ZIHUI

The programs ZIHUI are short auxiliary programs which help in handling PLASMOR:

- (i) ZIHUI1 FORTRAN - identifies and lists the variables and arrays in the various common blocks, and writes them on the disc as ZIHUI1 OUT.
- (ii) ZIHUI2 FORTRAN - lists the names of the variables and arrays that are used in the various subroutines and writes them on the disc as ZIHUI2 OUT. The program cannot distinguish the FORTRAN statements from the variable names so it lists the statements together with the variables. Run time of ZIHUI2 is about 40 sec.
- (iii) ZIHUI3 FORTRAN - compares the outputs of ZIHUI1 and ZIHUI2 and lists (on ZIHUI3 OUT) the variables which are never used in PLASMOR as well as the blocks used in each subroutine. This program helps greatly in

cleaning up PLASMOR and in deleting unused variables. Run time is about 20 sec.

- (iv) ZIHUI4 FORTRAN - given a variable name, this auxiliary program returns the names of the subroutines that use this variable. This program uses ZIHUI2 OUT. It works interactively i.e. type in the variable - the computer prints out the subroutines and waits for the next variable. Typing in a blank stops execution.

## 5. POST PROCESSORS

### 5.1 AUTOEXEC

This internal routine of the IBM-PC links the PC to the mainframe and, using a user-friendly system, enables the transfer of the PLASMOR DEB main output file from the mainframe to the PC hard disc.

The linkage is carried out by answering properly the computer's questions. When the linkage is finished one can use the regular CMS operating system commands (copy file) to copy data files from the mainframe to the PC hard disc.

The transfer of the files may take several hours, depending on the file length, and is preferably carried out at night.

### 5.2 Graphics

Two systems of packages for graphics are available on the IBM-PC, one for display on the monitor screen for a visual check of the PLASMOR results, and the second for plotting the results. Both programs are written in BASIC.

#### 5.2.1 PLASMOR.DLY

This program displays the output of PLASMOR on the monitor. The spatial behavior of three variables, namely, the temperature, the pressure and the compression, are shown for a predetermined list of timesteps. This program enables the user to choose the proper ranges of the axes which will be used later, in the final plots.

PLASMOR.DLG performs the same task as PLASMOR.DLY but on a logarithmic scale. For the control parameters see 5.2.2 below.

### 5.2.2 PLASMOR.PLG

After choosing the proper axes, one can use PLASMOR.PLG to plot the above parameters temperature, pressure and compression from PLASMOR.DEB. PLASMOR.PLG provides logarithmic axes, whereas PLASMOR.PLY provides linear scales (which are usually less useful).

The possibility of plotting the PLASMOR results was a very great advance in the use of PLASMOR. It enabled us to detect small phenomena inside the plasma<sup>2,3</sup>, which were otherwise very difficult to read off of a numerical printout and practically impossible to plot by hand. It also provided an easy way of choosing a set of representative graphs for publication.

The input parameters are entered into the program in lines 1110 - 1140 and they include the following:

- 1110: width of plot, scale of  $\rho/\rho_0$ , scale of P, scale of T, lower limit of T
- 1120: width of plotter in pixels
- 1130: first timestep to be plotted, frequency of plot, speed of plot, dummy, dummy
- 1140: name of file to be plotted

### 5.3 BRWTZ.FOR

The program BRWTZ.FOR simulates the streak camera recording after the arrival of the shock front on the backsurface of the target. The program can simulate only a one-dimensional emission. The light emission, reabsorption by the outer layers of the plasma and the streak camera response functions are included. The recorded light intensity is given by,

$$I = C \int_0^{\infty} dx F(x) S(x) \frac{x^3}{\exp(x/kT) - 1} \quad (6)$$

where C is a numerical constant proportional to the Stefan-Boltzmann factor,  $x = h\nu$  is the photon energy, S(x) is the streak camera spectral response function, and

$$F(x) = \exp[- \int \sigma(x,y) \sigma(y) dy] \quad (7)$$

Here  $\sigma(x,y)$  is the photoabsorption cross-section of photons with energy  $x$  at a depth  $y$  from the backsurface. In Eq. (6) black-body radiation from the shocked region is assumed. The density  $\rho(y)$  of the material ejected from the back surface is allowed to expand laterally at a constant opening angle (SLOPE) which is fixed arbitrarily, so that the computational results will fit the experimental ones.

Comparisons between the computational and experimental results showed good agreement, but the results have not as yet been published.

#### 5.4 SNAPSHOT FORTRAN

This program uses the results of PLASMOR FORTRAN to calculate the instantaneous and time-integrated continuous and line X-ray spectra emitted by a plasma. The X-ray emission rates are taken from the appropriate DXR table. Reabsorption is neglected, but it is intended to add it in the near future.

The program reads from the PLASMOR DEB output the local temperature and density in each cell at every time step. Spatial integration is carried out to find the instantaneous spectral emission rate, and finally, the spectra are added up to obtain the time-integrated emission spectrum.

An option is available which simulates the spectrum recorded by a spectrograph whose entrance window is covered by a thin beryllium or aluminum foil. The absorption factor of these foils is taken into account in the recorded spectrum.

This program was used to simulate experimental values of the temperature of KrF - laser produced aluminum plasma<sup>7</sup>, and agreement to high accuracy was obtained between the simulations and the experiments<sup>7</sup>. A graph of Ref. (3) was also computed by this program.

#### 5.5 POLYFT FORTRAN

This program reads the PLASMOR DEB output, finds the location of the shock front at each timestep and fits a linear or quadratic polynomial to these locations as a function of time. From the fitted values the instantaneous shock velocity and/or acceleration can be derived.



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APPENDIX: Printout of PLASOR MANUAL

FILE: PLASOR MANUAL A

PLASOR CONVERSATIONAL RUNTIME SYSTEM

CONTENTS  
\*\*\*\*\*

- I UPDATE
- II INTRODUCTION
- III EQUATIONS
- IV APPLICATIONS
- V COMMON BLOCKS
- VI INPUT CARDS

UPDATE  
\*\*\*\*\*

17.3.1937 PREPARATION OF THIS DOCUMENT 17.5.66

INTRODUCTION  
\*\*\*\*\*

- 111 THE ORIGINAL PURPOSE OF THE JOB DESCRIBED ABOVE WAS TO OBTAIN AND STORE ON DISK THE DATA OF PLASOR INPUT
- 121 EQUATIONS AND COMMENTS ACCORDING TO THE REPORT IN WHICH THEY APPEAR. THIS APPLIES TO ALL 1937 REVISIONS EXCEPT 72 IN ORDER TO BE PLASOR

SUBROUTINES  
\*\*\*\*\*

| 1. DATA INPUT AND INITIALIZATION |       |                                     |
|----------------------------------|-------|-------------------------------------|
| 1.1                              | CONSI | MATHEMATICAL AND PHYSICAL CONSTANTS |
| 1.2                              | PROFI | READ SCHEM DATA TABLES              |
| 1.3                              | PROFI | READ CONTROL DATA FROM INPUT CARDS  |
| 1.4                              | PROFI | INITIALIZE TEMPERATURE PROFILE      |
| 1.5                              | CONSI | PREPARE INPUT DATA                  |

2. GRAND LOOP OF COMPUTATION

|      |       |   |
|------|-------|---|
| 2.1  | TRC   | TRC LOOP CONTROL ROUTINE                          |
| 2.2  | TRC   | PRINTOUT EVERY ITERATION                          |
| 2.3  | READ  | FLOW FIELD CALCULATION, DELTA-TIME STEP           |
| 2.4  | APSOR | LASER ENERGY ABSORPTION                           |
| 2.5  | LASOR | LASER PULSE SHAPE                                 |
| 2.6  | STOR  | STORAGE OF ELECTRONIC ENERGY DEPOSITION           |
| 2.7  | TEMP  | SOLUTION OF THE ENERGY EQUATION, NEW TEMP PROFILE |
| 2.8  | SC    | SCHEM AND SCHEM DATA                              |
| 2.9  | TRC   | SOLUTION OF THE TRICHOGRAPHIC SET OF EQUATIONS    |
| 2.10 | TRVIS | ARTIFICIAL VISCOSITY                              |
| 2.11 | TRC   | TEMPERATURE REGULATION AND COOLING LOCATION       |
| 2.12 | TRC   | TEMP COMMON BLOCKS                                |
| 2.13 | TRC   | CONVERSION OF INPUT DATA TO COMMON AND LOCAL      |
| 2.14 | TRC   | LOCATION OF STATE                                 |
| 2.15 | TRC   | TRC   |
| 2.16 | TRC   | TRC   |
| 2.17 | TRC   | TRC   |
| 2.18 | TRC   | TRC   |
| 2.19 | TRC   | TRC   |
| 2.20 | TRC   | TRC   |

```

2.11 LAST ENERGY BALANCE AND VARIABLE RECYCLING
2.12 ION SET IONIZATION DATA
2.13 ENERB RADIATION ENERGY DEPOSITION
2.14 KEEM KE ELEM. EXPONENTIAL INTEGRAL FUNCTION

```

3. AUXILIARY ROUTINES

```

3.1 FINL NUMERICAL INTERPOLATION
3.2 ZINT LINEAR INTERPOLATION
3.3 INPL INITIALIZES A FLOATING POINT VECTOR
3.4 INT INITIALIZES A FIXED POINT VECTOR

```

INPUT/OUTPUT UNITS

\*\*\*\*\*

```

FILE 1 IRR1 DATA STORAGE OF COMMON BLOCKS FOR RESTART
PURPOSES
FILE 2 IRR2 DATA STORAGE OF COMMON BLOCKS FOR RESTART
PURPOSES
FILE 3 RESTR DATA CONTROL CARDS FOR RESTART
FILE 5 (IN) PLASM INPUT CONTROL CARDS FOR RUNNING PLASMA
FILE 6 (OUT) PLASMA OUT OUTPUT FILE FOR MISCELLANEOUS PRINTOUT
FILE 7 RSDAL DATA LIST OF RUSSELAND L. F. PATHS
FILE 10 OXRAL DATA ATOMIC DATA IONIZATION TABLES
FILE 21 AL INEOS HENRIK'S EQUATION-OF-STATE TABLES
FILE 31 AL SSM311L SESAME EQUATION-OF-STATE TABLES
FILE 50 TERMINAL PROMPT OUTPUT FOR DEBUGGING PURPOSES
FILE 70 NUCLEA OUT NUCLEAR DATA FOR EOS TABLES
FILE 80 PLASMA OUT PLASMA OUTPUT FILE

```

COMMON BLOCKS

\*\*\*\*\*

1. COMMON/CONST

HOSE OF THE MATHEMATICAL AND PHYSICAL CONSTANTS IN ZONSET ARE SELF-EXPLANATORY. FULL DESCRIPTION OF THE VARIABLES IS GIVEN IN SUB-ROUTINE CONST. THE FOLLOWING ARE NOTICABLY:

```

IENCL = 10000, IEND = 0, IAL = 0
ICL = 1, IEND = 12

```

2. COMMON/VAR1

COMPUTED CELL VARIABLES

```

IA LOCATION OF THE INTERFACE BETWEEN CELLS J AND J+1, TIMESTEP I
IB LOCATION OF THE INTERFACE BETWEEN CELLS J AND J+1, TIMESTEP I+1
IWH IWH??
IV VELICITY OF INTERFACE BETWEEN THE CELLS, TIMESTEP I+1
TNA ELECTRON TEMPERATURE IN CELL J, TIMESTEP I
VOLUME VOLUME OF CELL J AT TIMESTEP I
VOLUME VOLUME OF CELL J AT TIMESTEP I+1
TNR ELECTRON TEMPERATURE IN CELL J, TIMESTEP I+1
TNA ION TEMPERATURE IN CELL J, TIMESTEP I
TNA ION TEMPERATURE IN CELL J, TIMESTEP I+1
IWH VELICITY OF INTERFACE BETWEEN CELLS J AND J+1, TIMESTEP I+1
PRESS PRESSURE
ALGAM LOSIE-LAMDA T FOR ELECTRONS
C VECTOR TO STORE DATA FOR TETRAHEDRAL EQUATIONS
D VECTOR TO STORE DATA FOR TRIANGULAR EQUATIONS
TPM SEE PROFILE (DOESN'T SEEM TO BE USED)
PACI FRACTIONAL INCREASE OF CELL SIZE
UP ARTIFICIAL VISCOSITY FACTOR
QN RATIO OF NET ENERGY TRANSPORT BY ELECTRONS THROUGH CONDUCTIVITY INTO CELL J TO CALC'D IN TERMS USED IN IONIZ. SEE EQ. 1033
II AVERAGE I
IISO AVERAGE I??
NENSA NUMBER OF ELECTRONS IN CELL J
NENSA ELECTRON NUMBER DENSITY IN CELL J, TIMESTEP I
NENSA ELECTRON NUMBER DENSITY IN CELL J, TIMESTEP I+1
U ENERGY ASSIGNED BY THE SYSTEM (SEE 305C05)

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A VECTOR TO STORE DATA FOR TRIDIAGONAL EQUATIONS  
 SUMI TOTAL IMPACT OF IONS IN CELL J ( = N(IJ) IN IONSET )  
 AVERAGE MASS OF IONS IN CELL J  
 REEION LOGIC FLAG 1 FOR IONS  
 NNA55 AVERAGE MASS OF NEUTRAL PARTICLES  
 NP TOTAL NUMBER OF NEUTRAL PARTICLES IN CELL J ( SET TO 0 IN IONSET )  
 NP TOTAL NUMBER OF HEAVY PARTICLES ( IONS + NEUTRALS )  
 CVB SPECIFIC HEAT AT CONSTANT VOLUME  
 PDEFF SPECIFIC HEAT AT CONSTANT PRESSURE  
 ESAVE IONIZATION ENERGY IN CELL J

ISAVE SEG. LOGICAL 1 IN IONSET 1  
 EPR TOTAL RADIATED ENERGY FROM CELL J ( CALC'D IN DRENCA )  
 FOR I TOTAL RADIATED ENERGY IN CONTINUOUS SPECTRUM, INTEGRATED OVER ALL CELLS ( ALSO IN DRENCA )  
 SMPA DE WAVELENGTH ( SEG. LOGICAL )  
 EARL IONIZ. RADIATED ENERGY IN LINE SPECTRUM, INTEGRATED OVER ALL CELLS ( ALSO IN DRENCA )  
 ILL LOWER LIMIT OF TEMPERATURE IN THE DIR TABLES  
 IYL UPPER LIMIT OF TEMPERATURE IN THE DIR TABLES  
 DEX LOWER LIMIT OF DENSITY IN THE DIR TABLES  
 DUY UPPER LIMIT OF DENSITY IN THE DIR TABLES  
 ILL IONIZ. ENERGY OVER ALL CELLS  
 ZL1 ZENITH ANGLE OF MATERIAL 1  
 IT QUANTITY OF HEAVY PARTICLES IN REGION 1  
 ZL2 ZENITH ANGLE OF MATERIAL 2  
 IGE IONIZATION ENERGY  
 CIO COLLISION ZONING FLAG IN IONSET

DI INITIAL IONIZ. FOR DIR ELECTRON TEMPERATURE  
 TABL AVERAGE IONIZ. PARAMETERS  
 TAVE AVERAGE IONIZ. TEMPERATURE  
 MWAVELENGTH, I, J, K, LENGTH, IONIZ. RATIO, POINTS

|   |                               |
|---|-------------------------------|
| A | ALL DIR IONSET                |
| A | ALL DIR 22.0-INITIAL * 0.0010 |
| A | ALL DIR 22.0-INITIAL * 0.0010 |
| A | ALL DIR 22.0-INITIAL * 0.0010 |
| A | ALL DIR 22.0-INITIAL * 0.0010 |

I, J, K TEMPERATURE INITIAL IONIZ. RATIO, POINTS  
 I, J, K INITIAL IONIZ. RATIO FOR THIS M  
 I, J, K INITIAL IONIZ. RATIO  
 I, J, K INITIAL IONIZ. RATIO

CAVA 0.001  
 TIC INITIAL IONIZ. TEMPERATURE IN KEV/CM  
 TIP INITIAL IONIZ. TEMPERATURE IN KEV/CM  
 CHASS AVERAGE IONIZ. OF MATERIAL 1  
 PP INITIAL IONIZ. OF MATERIAL 1 IN REGION 1  
 APT AVERAGE IONIZ. OF MATERIAL 1  
 PRHII INITIAL IONIZ. OF MATERIAL 1  
 IP IONIZ. CALCULATION OF MATERIALS IS NOT USED IN CASE 1

|   |                          |
|---|--------------------------|
| <p>1. CODE VARSZY</p> <p>TIME CASER RESCUE</p> <p>POWER CASER PUMP CONDUCTIVITY ( CASER) *****</p> <p>ROUR TORQUER OF REGION 1</p> <p>CUT DURATION OF CASER PULSE, IN UNITS OF RESCUE</p> <p>IPUT TIME AFTER TIME FOR SIMULATION</p> <p>OTU INITIAL TEMPERATURE</p> <p>OLN IONIZ. FOR MATERIAL</p> <p>ODEF COLLISION ZONING SWITCH (CONDUCTION TIME TO THE COLLISION ZONING CONDUCTIVITY)</p> | <p>GENERAL VARIABLES</p> |
|---|--------------------------|

RADI RADIUS OF GREATEST GAIN ( ONLY FOR SPHERICAL GEOMETRY )  
 FFLA3 FRACTION OF TOTAL LASER ENERGY WHICH CAN BE INJECTED IN ONE  
 TIMESTEP ( USUALLY SET TO 0.05 )  
 FCLF1 COUPLANT-LEAK FRICTION FACTOR ( USUALLY = 0.1 )  
 FMCN LARGEST FRACTIONAL DECREASE IN ELECTRON ENERGY ALLOWED IN ANY  
 CELL IN A GIVEN TIMESTEP ( USUALLY = 0.25 )  
 FMC2 LARGEST FRACTIONAL DECREASE IN ELECTRON ENERGY ALLOWED IN ANY  
 CELL IN A GIVEN TIMESTEP ( USUALLY = 0.20 )  
 FVOL LARGEST FRACTIONAL CHANGE IN CELL VOLUME ALLOWED IN ANY  
 CELL IN A GIVEN TIMESTEP ( USUALLY = 0.10 )  
 FMAX MAXIMUM ALLOWABLE COMPRESSION OF CENTER CELL ( USUALLY = 20.0 )  
 FRES FRACTION OF REMAINING LASER BEAM ENERGY ABSORBED AT CRITICAL SURFACE  
 FRESN MAXIMUM ALLOWABLE RADIATION LOSS DURING TIMESTEP ( USUALLY = 0.001 )  
 FRA3D CRITERION USED IN ABSORB FOR COLLISION DENSITY ARRANGEM ( USUALLY 50.000 )  
 REEM NUMERICAL COEFFICIENT FOR ELECTRON-ION RELAXATION TIME CONSTANT,  
 EQ. 1.22  
 COBAR SEE CONST  
 CRFOP LASER FREQUENCY IN SEC<sup>-1</sup> )  
 FEG 6.00E1  
 SORTEM SOURCE P.E. )  
 RDETC DIETZMANN CONSTANT  
 CHRG ELECTRON CHARGE ( ESU )  
 AC "H 1.5 \* BOLTZ  
 C CEL 1.0 \* BOLTZ  
 NCUT CRITICAL DENSITY  
 NCUT1 1.0 \* NCUT  
 CCF SEE CONST  
 CANS SEE MAXN  
 CLM SEE CONST  
 CARON SEE CONST  
 FRADPA DIVISOR OF RCHL IN MAIN  
 FFLUX DIVISOR OF QO IN TEMP  
 DT DIFF TIMESTEP  
 JECV ELECTRON THERMAL ENERGY, TIME AND SPACE INTEGRATED  
 FROR RELATIVE FRACN IN TOTAL ENERGY  
 TEND TIME  
 E3BL TOTAL RADIATED ENERGY  
 C3BNS TERMINATION COUNTS ( SEE LAST )  
 T3BFF LASER ENERGY ABSORBED UP TO PRESENT TIMESTEP  
 T3BR TOTAL ENDRG  
 T3BEF THERMAL ENERGY, SPACE INTEGRATED  
 T3BEM ELECTRIC ENERGY, SPACE INTEGRATED  
 T3BTA TOTAL THERMAL+KINETIC E. ENERGY, SPACE INTEGRATED, TIMESTEP EAT  
 E3BP TOTAL ENERGY SUPPLIED BY THE LASER UP TO PRESENT TIMESTEP  
 T3BTF TOTAL THERMAL+KINETIC ENERGY, SPACE INTEGRATED, TIMESTEP EAT  
 T3BMJ SUM OVER J MOMENTUM, FOR EACH CELL  
 P3BMJ POS. MOMENTUM OUTWARD CALCULATED IN MOMENTUM LOOP  
 P3BMJ1 MOMENTUM E. IN THE DETERMINE PART WHICH IS POINTING  
 D3BMJ AS POSION OF IT CALCULATED IN SEPARATE LOOP, DIFF. PROGRAM  
 H3BT SEE CONST  
 T3FID SEE MAXN  
 C3IE CONV. FACTOR FROM DEGREES TO EV  
 C3EI CONV. FACTOR FROM EV TO DEGREES  
 F3AS TERMINATION PARAMETER ( SEE LAST )  
 D3SM SEE ARTIVS

SPA TIMESTEP, I SEE TEND )  
 DTB DT TIMESTEP, I SEE TEND )  
 E3BFR LATENT THERMAL ENERGY ORIGINALLY PRESENT IN THE SYSTEM  
 E3BFI INITIAL RADIATED ENERGY  
 P1A LASER PULSE SHAPE  
 #TOT TOTAL ENERGY GOING INTO HOT ELECTRONS  
 T1NCR TIME / RISETIME  
 JECV ELECTRON THERMAL ENERGY, SPACE INTEGRATED  
 FLAT DELTA-LATENT ENERGY, SPACE INTEGRATED  
 I3TL TOTAL LATENT ENERGY, SPACE INTEGRATED  
 F3MRE RADIATED ENERGY IN CONTINUOUS SPECTRUM, SPACE INTEGRATED  
 I3MRE TOTAL CONTINUOUS EMISSION, SPACE + TIME INTEGRATED  
 F3LNE RADIATED ENERGY IN LINE SPECTRUM, SPACE INTEGRATED  
 T3LNE TOTAL LINE EMISSION, SPACE + TIME INTEGRATED  
 I3PM INITIAL ELECT.-TEMP. FOR ADJUSTING PRESSURE AT  
 I3PM1 INCREASAGES OF RESONANCE FOR COLD SYSTEM ( 1-1000 )  
 I3PM2 ELECTEMP AT WHICH NO MORE ADJUSTMENT ( 1-1000 )  
 I3PM3 I3PM1 FOR I3CALC = 2

3. COMMON/VAR37

FIXED POINT VARIABLES

- NRXK NUMBER OF ISOTOPE
- NF ATOMIC NUMBER OF MATERIAL
- NFC EXCEPT FOR HYDROGEN WHERE #0
- NRXNM NUMBER OF DIFFERENT REGIONS IN CORE
- NRKX NUMBER OF CELLS IN REGION K
- NREGS SAME AS NRXK FOR THE ELECTRON EQUATION ( SEE BELOW )
- NRSTK NUMBER OF TIME STEPS
- NRFWD NUMBER OF TIME STEPS BETWEEN MAJOR OUTPUT PRINTINGS
- NRWTF NUMBER OF ITERATIONS OF IMPLICIT NEW EQUATION FOR THE IONS ( SEE TEMPS )
- ICAS EOS FORMULATION, USE #3. SEE INPUT LIST
- IRN PLASMA IONIZATION, ( SEC INPUT LIST )
- EDEFR EXCER FREQUENCY IN MULTIPLES OF WDM CLASS FREQUENCY
- IBR4E #1 FOR NEW CALCULATIONS, #2 FOR CONTINUATION
- FINC# TERMINATION OPTICS, SEE INPUT LIST
- IGROM GEOMETRY OPTION, SEE INPUT LIST
- IPOFF DENSITY PROFILE PARAMETER
- ILEFT INDEX OF INNERMOST CELL WHICH IS ACTIVE IN THE SIMULATION
- JPRC CURRENT CELL WHERE THE SHOCK HAS ARRIVED. EMPLOYED
- JPR1 JLEFT + 1
- JPR2 JLEFT + 1
- ITMP1 NUMBER OF TEMPERATURE MESH POINTS IN THE DATA TABLES ( JASAL )
- ITMP2 NUMBER OF DENSITY MESH POINTS IN THE DATA TABLES
- JN TOTAL NUMBER OF CELLS
- JNPK JNPK + 1
- JSTOP IF JSTOP GE 1 THEN STOP EXECUTION
- J1 JLEFT
- IT NUMBER OF CURRENT TIME STEP
- ITOL FIRST TIME STEP
- JPR3 NUMBER OF TIME STEPS BETWEEN MAJOR OUTPUT PRINTINGS

- ICELC I-INDEX OF CELL WHERE AN INTERNAL VARIABLE OF CORE
- ICELC I-INDEX AFTER COMBINATION NUMERICAL CELL - INDEX
- IPR3 IPR3 AFTER JNPK HAVE TO BE KEPT IN
- JNCKS CELL NUMBER IN WHICH HAVE MAXIMUM COMPRESSION
- JNMAK CELL NUMBER IN WHICH HAVE MAXIMUM ELECTRON TEMPERATURE
- JNMKS CELL NUMBER IN WHICH HAVE MAXIMUM ION TEMPERATURE
- ICEMR MAXIMUM ELECTRON TEMPERATURE PARAMETER ( SEE INPUT LIST )
- ICEMR MAXIMUM ION TEMPERATURE PARAMETER ( SEE INPUT LIST )
- JST NUMBER OF TIME STEPS BETWEEN GROUPS OF DATA ONLY TAKE ON DISK FOR PURPOSES OF RESART
- NIMAX NUMBER OF DATA TABLES

4. COMMON/VAR47 MISCELLANEOUS

- R00R INTEGRAL OF RHO\*CR
- EMAXX MAX. ION TEMPERATURE
- EMAXK MAX. ELECTRON TEMPERATURE
- NE1 NUMBER OF MATERIAL K
- NTEMP NUMBER OF TEMPERATURE MESH POINTS IN DATA TABLES
- ITEMP NUMBER OF DENSITY MESH POINTS IN DATA TABLES
- NRH INDEX OF MATERIAL P
- TOLES LIST OF TEMPERATURES ( LOG SCALE ) IN DATA TABLES
- TOLAS LIST OF TEMPERATURES ( LIN SCALE ) IN DATA TABLES
- TOLAE AVERAGE T ( LIN SCALE ) IN DATA TABLES
- TDENX AVERAGE Z\*P ( LOG SCALE ) IN DATA TABLES
- TDAS LIST OF DENSITY MESH POINTS ( LIN SCALE ) IN DATA TABLES
- TDOAS LIST OF DENSITY MESH POINTS ( LOG SCALE ) IN DATA TABLES
- NRBD PARTICLE RADIATION ENERGIES ( LIN SCALE ) IN DATA TABLES ONLY
- ERDAS IONIZATION ENERGY LIST ONLY IN DATA TABLES BELOW
- SPRCK CONTINUOUS EMISSION SPECTRUM ( SEE OPTI )
- SPR2D "N" DIMENSION OPTIC BELOW
- SP1J CONTINUOUS EMISSION SPECTRUM - TIME INTEGRATED
- SP1JUT CONTINUOUS EMISSION SPECTRUM - SPAC AND TIME INTEGRATED
- SP2JX LINE EMISSION SPECTRUM ( LOG SCALE ) IN DATA TABLES
- SP2JX LINE EMISSION SPECTRUM - TIME INTEGRATED
- SP1JUT LINE EMISSION SPECTRUM - SPAC AND TIME INTEGRATED
- SP2JYX LINE EMISSION SPECTRUM ENERGY GROUPS

CLND3 LIST EMISSION LINES  
 DTRR TIMESTEP INCREASE FROM RADIATION EMISSION CRITERIA  
 ENR1 EMISSION ION COLLECTION DECELERATION TIME  
 ENR2 LOCAL ENERGY SUPPLIED BY THE LASER (AFTER LOSS OF SCATTER)  
 ENR3 INDEX OF THE LASER PULSE SHAP  
 ENR4 INDEX SHOWING THAT THE SIMULATION YIELDED NEGATIVE TEMPERATURE  
 (SEE TEMPS AND LEAM'S EXPLANATIONS)  
 ENR5 LOWER LIMIT OF CONTINUOUS RADIATION  
 ENR6 NUMBER OF ITER ITERATIONS (SEE ENR1)  
 ENR7 AVERAGE PRESSURE AROUND THE SHOCK FRONT  
 ENR8 INTERNAL ENERGY DENSITY

5. COMMON/PRSR/ RADIATION DATA

ENR9 CONTINUOUS SPECTRA FOR EACH CELL AND ENERGY RANGE (ENR9)  
 ENR10 LINE SPECTRA FOR EACH CELL AND LINE ENERGY (ENR10)  
 ENR11 PHOTOABSORPTION CROSS-SECTION IN CM\*\*2/G. SEE "OSIGMA"  
 IN " DIMENSION DTR BELOW "

6. COMMON/FI17/ GENERAL FIACC POINT DATA

IC1 INDEX OF THE FIRST CONTINUOUS ENERGY GROUP TO BE USED  
 IC2 INDEX OF THE LAST CONTINUOUS ENERGY GROUP TO BE USED  
 IL1 INDEX OF THE FIRST EMISSION LINE TO BE USED  
 IL2 INDEX OF THE LAST EMISSION LINE TO BE USED  
 IPROL THE UNIT NUMBER OF THE ION TABLES  
 IRE THE UNIT NUMBER OF THE TEMPORARY DATA STORAGE FOR RESISTANCE PURPOSES  
 IWS UNIT NUMBER OF IONIC DATA SET  
 IWS UNIT NUMBER OF PLASMA CUR

7. COMMON/TITLE/

DTIME FIRST TIMESTEP AFTER WHICH FIELDS OUTPUT WILL BE PRINTED OUT  
 RLEN TOTAL LENGTH OR RADIUS OF THE SYSTEM \* RALJMP2  
 WPATH ABSORPTION PATH BETWEEN TWO CELLS (CALC'D IN EOS 1)  
 WPATH SAVED VALUE OF WPATH (SEE ABSORB)  
 WPATH SAVED VALUE OF WPATH  
 SUPTR SURFACE THERMAL ELECTRICITY TREATED AS MAXWELLIAN  
 WPATH SPECIFIC HEAT CAPACITY AT CONSTANT PRESSURE  
 WPATH SPECIFIC HEAT CAPACITY AT CONSTANT TEMPERATURE  
 WPATH BACKSCATTERING FACTOR, INITIALLY SET = 1.0  
 (SEE I P. 11, WHERE IT IS CALLED ORG.)  
 WPATH AVERAGE Z, CALC'D FROM EOS TABLES  
 WPATH TIME BASE TO BE PRINTED IN OUTPUT E. G., IF IN NSEC'S  
 THEN WPATH = 1.E5  
 WPATH CALCULATE THERMAL HCT ELECTRON TAIL ENERGY SEPARATELY  
 WPATH UNIT NUMBER OF PLASMA DED3. THE MAJOR PRINTOUT DEVICE  
 WPATH WPATH MEANS DO NOT CALCULATE BACKSCATTERING ADJUSTMENT  
 WPATH = 1. DO CALCULATE IT  
 WPATH MATERIAL LAYER TO DETERMINE PROPER CG TO BE USED

8. COMMON/PRSR/ RADIATION DATA

WPATH LIST OF TEMPERATURE MESH POINTS  
 WPATH LIST OF DENSITY MESH POINTS

05500 MASSIVE AND SPATE FREE PAIR  
 05505 NUMBER OF TEMPERATURE MESH POINTS  
 05510 NUMBER OF DENSITY MESH POINTS

2. DIMENSION DATA ATOMIC AND RADIATION DATA

01EMP LIST OF LOG OF TEMPERATURES (MAX. 20 VALUES)  
 01ENS LIST OR LOG OF DENSITIES (MAX. 10 VALUES)  
 02EK LIST OF ENERGY INTERVALS (ELEM. CHARGE FOR CONTINUOUS SPECTRA)  
 02K0 LIST OF WAVELENGTHS IN LINE RADIATION  
 02AV Z-AVERAGED TEMPERATURE LINEAR SCALE  
 02E LOG OF ELECTRON DENSITY (TEMP, DENS)  
 02Z LOG OF IONIZATION STATE DENSITY (STATE, TEMP, DENS)/TOTAL JC45  
 02EY LOG OF CONTINUOUS SPECTRUM INTENSITY ENERGY INTERNAL TEMP.  
 02EY1 ONION STATE CROSS SECTION TO 16-ATOMS 100- EV  
 02EY2 LOG OF TOTAL INTENSITY TEMP, DENS. INCLUDES LINE AND CONTINUOUS  
 INTENS. CROSS SECTION TO 16 ATOMS  
 02ER LOG OF INTERNAL ENERGY (TEMP, JC61). UNITS: CAL/ION  
 02ENX LOG OF LINE INTENSITY (LINE, TEMP, DENS)  
 02ZV AVERAGE Z-AV. LINEAR SCALE  
 02ZV1 TEMPERATURE (LINEAR SCALE)  
 02ZV2 DENSITIES (LINEAR SCALE)  
 02ZV3 TABLE OF PHOTOABSORPTION CROSS-SECTIONS ENERGY GROUPS 2AV1  
 UNITS: CM<sup>2</sup>/ION

DATA EQUIVALENCE TABLE

|      |        |   |     |   |    |        |   |     |        |   |   |
|------|--------|---|-----|---|----|--------|---|-----|--------|---|---|
| 1    | 01EMP  | 1 | 20  | 1 | 20 | 02AS1  | 1 | 111 | 02GAP  | 1 | 1 |
| 21   | 02ENS  | 1 | 20  | 1 | 20 | 02AS2  | 1 | 111 | 02GNS  | 1 | 1 |
| 31   | 02EK   | 1 | 160 | 1 | 40 | 02AS3  | 1 | 111 | 02K0   | 1 | 1 |
| 41   | 02K0   | 1 | 20  | 1 | 20 | 02AS4  | 1 | 111 | 02ZV   | 1 | 1 |
| 51   | 02AV   | 1 | 20  | 1 | 20 | 02AS5  | 1 | 111 | 02E    | 1 | 1 |
| 61   | 02E    | 1 | 20  | 1 | 20 | 02AS6  | 1 | 111 | 02Z    | 1 | 1 |
| 701  | 02ZV   | 1 | 20  | 1 | 20 | 02AS7  | 1 | 111 | 02ZV1  | 1 | 1 |
| 801  | 02ZV1  | 1 | 20  | 1 | 20 | 02AS8  | 1 | 111 | 02ZV2  | 1 | 1 |
| 901  | 02ZV2  | 1 | 20  | 1 | 20 | 02AS9  | 1 | 111 | 02ZV3  | 1 | 1 |
| 1001 | 02ZV3  | 1 | 20  | 1 | 20 | 02AS10 | 1 | 111 | 02ZV4  | 1 | 1 |
| 1101 | 02ZV4  | 1 | 20  | 1 | 20 | 02AS11 | 1 | 111 | 02ZV5  | 1 | 1 |
| 1201 | 02ZV5  | 1 | 20  | 1 | 20 | 02AS12 | 1 | 111 | 02ZV6  | 1 | 1 |
| 1301 | 02ZV6  | 1 | 20  | 1 | 20 | 02AS13 | 1 | 111 | 02ZV7  | 1 | 1 |
| 1401 | 02ZV7  | 1 | 20  | 1 | 20 | 02AS14 | 1 | 111 | 02ZV8  | 1 | 1 |
| 1501 | 02ZV8  | 1 | 20  | 1 | 20 | 02AS15 | 1 | 111 | 02ZV9  | 1 | 1 |
| 1601 | 02ZV9  | 1 | 20  | 1 | 20 | 02AS16 | 1 | 111 | 02ZV10 | 1 | 1 |
| 1701 | 02ZV10 | 1 | 20  | 1 | 20 | 02AS17 | 1 | 111 | 02ZV11 | 1 | 1 |
| 1801 | 02ZV11 | 1 | 20  | 1 | 20 | 02AS18 | 1 | 111 | 02ZV12 | 1 | 1 |
| 1901 | 02ZV12 | 1 | 20  | 1 | 20 | 02AS19 | 1 | 111 | 02ZV13 | 1 | 1 |
| 2001 | 02ZV13 | 1 | 20  | 1 | 20 | 02AS20 | 1 | 111 | 02ZV14 | 1 | 1 |

INPUT CARDS  
 \*\*\*\*\*  
 TWO PACKAGES OF INPUT CARDS ARE NEEDED TO RUN PACKAGES ONE TO RUN  
 A NEW PROBLEM AND ONE TO CONTINUE A PREVIOUS RUN. IN THE FIRST  
 OF THESE, THE PARAMETERS OF THE PROBLEM ARE INITIALIZED INTO THE PROGRAM,  
 WHEREAS THE SECOND PACKAGE CONTAINS ONLY SOME CONTROL SWITCHES AND

THE MAIN PARAMETERS ARE READ IN FROM MICR DISC 1 THE IBC FILES 1.

4. INPUT CARDS FOR A NEW PROBLEM
- 
- CARD 1.            I CARD            FORMAT    103, 15 1  
 N111            NUMBER OF CARDS IN THE HEADER
- CARD 2.            N111 CARDS            FORMAT    2044 1
- CARD 3.            HEADLINE, DESCRIPTION OF THE PROBLEM, OF THE PROBLEM'S  
 VOLTAGE, NUMBER OF LAYERS, IONIC COMPOSITION AND ENERGIES  
 OF THE PARTICLES, LAYER NUMBER AND TYPE OF ELECTRIC  
 FIELD, THE DESCRIPTION DETAILS ARE INITIALIZED TO THE  
 USER.



CARD 3. 1 CARD FORMAT (2I10X,15), 10X,20,4, (10X,15)F

IREAD = 1 FOR NEW CALCULATION; = 0 RESTART PREVIOUS PROBLEM  
ITEM MAX. NUMBER OF Timesteps = 1; IF TIME < 99999.1  
CUTL MAXIMUM SIMULATED TIME FOR PROBLEM  
NEMAX NUMBER OF OXR TABLES. A TABLE IS REQUIRED FOR EACH MATERIAL

CARD 4. 1 CARD FORMAT (2I10X,15) )

NRSS NUMBER OF TEMPERATURE MESH POINTS IN THE RUSSELLAND N.F.P. TABLES. IF = 0, THEN THE BLACKBODY RADIATION IS NOT CALCULATED  
NDRSS NUMBER OF DENSITY MESH POINTS IN THE RUSSELLAND N.F.P. TABLES

CARD 5. 1 CARD FORMAT (5E10X,15) )

DRJF MATERIAL INITIAL DENSITY PARAMETER  
= 1 SOLID DENSITY THROUGHOUT  
= 2 REDUCED DENSITY IN THE LAST 10 CELLS  
= 3 PARABOLIC INITIAL ELECTRON DE IFF  
= 4 OTHER  
ISA NUMBER OF Timesteps BETWEEN JUMPS OF DATA INTO TAPE OR DISC FOR PURPOSES OF RESTART  
DIFL NUMBER OF Timesteps BETWEEN MAJOR OUTPUT PRINTINGS  
LPL AFTER COMPUTATION REACHES FIRST REAL CELL LEFT = 2  
LPRF AFTER SHOCK WAVE IS REFLECTED 1 IN CASE OF TARGETS OF MORE THAN ONE LAYER 1

CARD 6. 1 CARD FORMAT (5I10X,15) )

KRPT SEE COLLIGN/VAR 1/

KRPT SEE COLLIGN/VAR 1/  
LGAC EG: FORMULATION  
= 1 PERFECT NON-DEGENERATE GAS = 2, FERMI-DIRAC EJS  
= 3, TFC MODEL 10M SOLID-GAS INTERPOLATION 1 USE THIS OPTION ONLY 1  
LEON PLASMA IONIZATION = 1 ACC COMP. SEE IONIZATION;  
= 2 IONIZATION FROM OXR TABLES 1 USE THIS OPTION 1  
LPRF SEE COLLIGN/VAR 1/

CARD 7. 1 CARD FORMAT (5I10X,15) )

IRPCH VERIFICATION OPTIONS  
= 1 IF TIME OR NUMBER OF Timesteps EXCEEDED  
= 2 SAME AS 1 WITH THE ADDITIONAL CONDITION THAT THE COMPRESSION IN CENTER CELL EXCEEDS 1444  
ICOM GEOMETRY OPTION: = 1 SPHERE; = 2 SLAB; = 3 SHELL  
LPRF RADIATION CALCULATION PARAMETERS:  
= 0 DO NOT CALCULATE OR CALCULATE FROM OXR TABLES  
LPRF NUMBER OF DIFFERENT REGIONS IN TARGET  
NINFF NUMBER OF CELLS IN REGION 1

CARD 8. 1 CARD FORMAT (5I10X,15) )

NINFF = 2 ..... MAXIMUM SIZE = 1 NUMBER OF CELLS IN REGION 1

CARD 9. 2 CARDS FORMAT (5I10X,15) )

ICRFL CONTROL SWITCH FOR THE EJS USED IN THE CALCULATION  
= 5 ICR PRESSURE CALCULATED FROM SOLID-GAS INTERPOLATION  
ICRFF = 0 NOT USED  
ICRFL = 17000: NOT USED  
ICRFL = 2: NOT USED  
ICRFF = 0 - PREPARE INPUT FOR SPECIFIC CALCULATE SPECIALLY  
= 1 PREPARE INPUT, DO NOT CALCULATE  
= 2 DO NOT PREPARE INPUT, DO NOT CALCULATE  
= 3 CALCULATE RADIATION PHOTON ABSORPTION ONLY

= 4 CALCULATE NET ELECTRON ABSORPTION ONLY  
= 5 CALCULATE BOTH NET ELECTRON AND RADIATION PRESENT

FORM 10-103 - NOT USED

CARD 10. 1 CARD FORMATE 415X.E15.4 1

IRISE SEE COMMON/VAR2/  
DIPER SEE COMMON/VAR2/  
DTEN SEE COMMON/VAR2/  
EUI SEE COMMON/VAR2/

CARD 11. 2000XNJM CARDS FORMATE 415X.E15.4 1

THIS CONTAINS TWO CARDS FOR EACH REGION & 1 FOR EACH MAXIMUM

NOTED IN THE SAME FORMAT

INUN SEE COMMON/VAR2/  
NCDR SEE COMMON/VAR2/  
TIM SEE COMMON/VAR1/  
REP SEE COMMON/VAR1/  
FACI SEE COMMON/VAR1/  
INPI NOT USED

CARD 12. 1 CARD FORMATE 5X.E15.4 1

MODE INNER RADIUS OF SHIELD: THIS CARD IS USED ONLY FOR 1000-1

CARD 13. 1 CARD FORMATE 5X.E15 1

MAA SEE COMMON/VAR3/

CARD 14. MANY CARD GROUPS

FOR EACH MATERIAL THREE (3) OF MOST 3 CARDS ARE READ IN

IF 1000-1 THEN ONLY 14A AND 14E

IF 1000-0 THEN 14A, 14B AND 14D

OTHERWISE: 14A, 14B, 14C

CARD 14A FORMATE 20X. 2110. E20.4 1

MZ ATOMIC NUMBER  
IND SEE COMMON/VAR3/  
WAT ATOMIC WEIGHT

CARD 14B FORMATE 20X. 3E20.4 1

FF FRACTURAL ADVANCEANCE OF MATERIAL IN EACH REGION 1

CARD 14C FORMATE 20X. 4E15.6 1

A\*14: 1,3,4,51 SEE COMMON/VAR1/

CARD 14D FORMATE 20X. 4E15.6 1

AL14: 1,2,3,150 SEE COMMON/VAR1/

CARD 15. 1 CARDS FORMATE 315X.E10.4 1

F1A SEE COMMON/VAR2/  
F1E SEE COMMON/VAR2/  
F1H SEE COMMON/VAR2/  
F1C SEE COMMON/VAR2/  
F1L SEE COMMON/VAR2/  
F1A SEE COMMON/VAR2/

FRIN SEE COMMON/VAR2/  
 FJOB1 SEE COMMON/VAR2/  
 FPAR1 SEE COMMON/VAR2/

FKAPPA SEE COMMON/VAR2/  
 FFLUX SEE COMMON/VAR2/  
 FPA1 SEE COMMON/VAR2/  
 FPRM SEE COMMON/VAR2/  
 FRTN SEE COMMON/VAR2/

COMPI SEE COMMON/VAR6/

CARD 10. 1 CARD FORMAT 1, 2, 3, 4, 5, 6, 7

CTIME SEE COMMON/TITLE/  
 \*\* 15 SPACES ARE LEFT BLANK  
 PRCN SEE COMMON/TITLE/  
 WPRM SEE COMMON/TITLE/  
 FABS SEE COMMON/TITLE/

4. THESE CARDS TO RESTART A PROBLEM

GENERALLY, TO RESTART A PREVIOUS-RUN ONE USES ONLY CARDS 10, 20, AND 30 OF THE CARDS USED FOR A NEW PROBLEM.

CARD 1. 1 CARD FORMAT 1, 2, 3, 4, 5

NYIT NUMBER OF CARDS IN THE ANSWER

CARD 2. 1111 CARDS FORMAT 2, 3, 4, 5

PARA HEADLINE DESCRIBES EACH OF THE FEATURES OF THE PROBLEM.  
 VEZ# NUMBER OF EXTENSIVE ERROR DESCRIPTIONS AND CHECKS.  
 THE PULSE RESISTANCE, GAIN, POWER AND TYPE OF COS TO BE  
 USED. THE DESCRIPTION DETAILS ARE ENTIRELY UP TO THE  
 USER.

CARD 3. 1 CARD FORMAT 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12

NRGRT \*1 FOR NEW CALCULATION; \*0 RESTART PREVIOUS PROBLEM  
 ITIME MAX. NUMBER OF Timesteps. ( IF LINE < 99999 )  
 CUTI MAXIMUM SIMULATED TIME FOR PROBLEM  
 NMEM NUMBER OF DATA PAGES. \*1 PAGE IS REQUIRED FOR EACH MATERIAL