High-Temperature Compatibility Study
of Iridium (DOP-26 Alloy)
with Graphite and Plutonia

K. M. Axler
D. T. Eash

Los Alamos National Laboratory
Los Alamos, New Mexico 87545

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ABSTRACT

This report outlines the materials compatibility tests conducted on DOP-26 iridium alloy and carbon. The carbon used was in the form of woven graphite as present in the impact shell used to encase plutonia in nuclear heat sources. In addition, compatibility tests of the DOP-26 alloy with plutonia are described. The reactivity observed in both systems is discussed.

I. INTRODUCTION

This work was conducted as part of a test program to investigate materials compatibility in nuclear heat sources. The units under investigation are those composing the General Purpose Heat Source (GPHS). The self-heating effect of the $^{238}\text{PuO}_2$ fuel in the GPHS provides thermal energy, which is converted to electrical power via Radioisotope Thermoelectric Generators (RTGs). RTGs can supply electric power for more than 20 years and are used in various space applications.

The $^{238}\text{PuO}_2$ heat sources are designed to operate at temperatures on the order of 1200°C-1300°C. However, higher temperature phase studies are conducted to characterize materials compatibility in the event of an accidental temperature excursion. These temperature excursions might be induced by an explosion or fire or by aerodynamic heating during accidental reentry into the earth's atmosphere.

In the GPHS, PuO$_2$ is contained within a cladding of iridium-based DOP-26 alloy. This alloy contains 0.3-0.5 wt.% tungsten and trace amounts of aluminum and thorium. In service, a protective graphite impact shell (GIS) of fineweave-pierced fabric (FWPF) graphite (AVCO Systems Division) surrounds the GPHS cladding.

II. DOP-26/GRAPHITE

A. Experimental Procedure

A series of induction heatings was conducted to determine the minimum reaction temperature for carbon (as woven graphite) and DOP-26. Specifically, we wanted to determine if contact with the GIS would induce a low-melting eutectic-like reaction with the heat source cladding.

Shards of DOP-26 were placed within crucibles fabricated from the same FWPF used in the GIS. The graphite cells were separated from the yttria stage of the induction heater by tungsten foil. The material was heated for 15 minutes at progressively higher temperatures. Temperatures were read with an optical
pyrometer sighting on the sample surface through a black-body hole in the cell lid. The reported temperatures reflect a correction factor for window attenuation. Between each consecutive heating, the sample was visually examined for signs of reaction and was also checked for weight loss. After consecutive heatings to 2283°C, there was no evidence of reaction or liquificalion, and no weight loss had occurred. Upon the next heating, to 2360°C, the sample showed signs of melting. No weight loss was observed. A cross section was cut from the product and prepared for electron microprobe examination.

B. Observations

The mounted specimen was found to contain two phases distributed throughout its depth. Figure 1 shows a secondary electron image of a typical region with a corresponding x-ray dot map for carbon. The

Fig. 1a. Secondary electron image of carbon platelets (400X).

Fig. 1b. X-ray dot map for carbon (400X).
major component of the specimen was an iridium matrix of the nominal DOP-26 composition. The secondary phase consisted of large platelets of carbon dispersed throughout the specimen and a distribution of extremely fine carbon striations within the matrix. The carbon-rich platelets contained \(~0.2\text{ at.\%}\) iridium. No carbon was detected in the matrix. Figure 2 shows a typical boundary between a platelet and the matrix. The superimposed x-ray intensity lines illustrate the absence of a compositional gradient at the interface region.

C. Discussion and Conclusions

According to Moissan,\(^1\) carbon dissolves in pure iridium liquid, but it is precipitated out as graphite upon cooling. Our observations are in agreement with this previously published work. In our study, the absence of dissolved carbon within the DOP-26 matrix indicates that the solid solubility for carbon in iridium is negligible at room temperature. However, the finely distributed striations appear to have grown out of the melt and indicate a larger solubility at elevated temperatures. (The large carbon inclusions may be artifacts of loosely woven graphite picked up by the melt.)

These observations are consistent with the Ir-C phase diagram\(^2\) shown in Fig. 3. According to the Ir-C phase diagram, the melting point for iridium with 3.12\% dissolved carbon is 2296\(\pm\)16°C. The specimen showed signs of melting within this temperature range, which indicates a melting point depression associated with dissolved carbon. The melting point for the DOP-26 alloy is approximately 2447°C (based on the melting point of iridium\(^3\)).

The study has indicated that the liquification of DOP-26 is affected by contact with the GIS material in agreement with the Ir-C phase diagram.

II. DOP-26/PuO\(_2\)

A. Experimental Procedure

The initial test involved reacting DOP-26 with PuO\(_2\) powder by arc melting. The starting composition was \(~50\text{ vol}\%\) PuO\(_2\). The reactants were combined and pressed into a pellet at \(~100,000\text{ psi}\). The
pellet was then reacted in the arc melter, producing a metallic button that appeared homogeneous when examined visually. Slight sputtering occurred during the reaction, which accounted for a small amount of unrecovered material. Because of the nature of this technique, no temperature could be associated with the reaction; however, it is certain that the temperature was considerably higher than the melting points of the components. A specimen cut from the pellet was mounted with a cross sectional view exposed. After polishing, the mounted specimen was electroetched at 15 V with HCl in saturated salts. Metallographic examination was performed on the etched specimen. After the metallographic examination, the sample was ground and polished again, then examined by electron microprobe.

In an effort to determine the threshold of reaction for the system, the tests were continued by reacting PuO$_2$ powder with shards of DOP-26 by induction heating. Preparations were made by packing PuO$_2$ into a tungsten cell, then placing the DOP-26 into the PuO$_2$. Care was taken to ensure that the DOP-26 shard did not contact the tungsten cell during heating. As before, temperatures were read using an optical pyrometer sighting on the sample surface through a black-body hole in the cell lid. Reported temperatures reflect a correction for window attenuation. The sample was heated to 1800°C in the induction heater under vacuum for 15 minutes. The iridium shard was mounted, polished, and examined by electron microprobe. An identical preparation was then heated to 2210°C for 15 minutes. The reacted DOP-26 shard from this heating was also mounted and examined by microprobe.
B. Observations

The metallographic examination of the arc-melted product revealed the presence of two phases. Electron microprobe showed that the major phase was iridium with the nominal tungsten content. The second phase, localized within the grain boundaries, consisted of Ir with 19-26 at.% Pu. Two reflected-light photomicrographs (Fig. 4) show the distribution of the Pu-Ir intermetallic phase within the phase boundary regions. Figure 5 shows two backscatter electron images of a typical grain boundary region examined by microprobe. Also shown in Fig. 5 are x-ray dot maps for plutonium illustrating its distribution within the grain boundaries. Apparently, the PuO\(_2\) was reduced because no oxygen was detected in either phase (the detection limit for oxygen in this system was 0.2 at.%).

A visual examination of the reacted PuO\(_2\) packing from both induction-heated specimens revealed that it had darkened, indicating partial reduction that was due to vacuum heating. Figure 6 shows a secondary electron image of a typical region within the shard heated to 2210°C. Also included in Fig. 6 are corresponding x-ray dot maps for plutonium and iridium. Microprobe examination of the induction-heated DOP-26 shards revealed PuO\(_2\) within the grain boundaries throughout both specimens. No indications of an intermetallic reaction were found in either case.

C. Discussion and Conclusions

An intermetallic phase was formed in the arc-melted sample. The compound PuIr\(_2\) is the most iridium-rich intermetallic compound reported\(^1\) in the binary system. The interstitial phase in the arc-melted specimen is believed to be PuIr\(_2\) with dissolved iridium.

The induction-heating experiments have shown that no intermetallic reaction occurs at temperatures up to 2210°C when the plutonium is present as the oxide. The induction-heating tests do indicate, however, that at temperatures below the onset of reaction, the PuO\(_2\) had moved through the grain boundary regions of the DOP-26 matrix. This grain boundary migration indicates that at temperatures at least as low as 1800°C, plutonium containment may be compromised by the effects of a solid state diffusion mechanism.

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Fig. 4. Photomicrographs of DOP-26 shard reacted with PuO$_2$ by arc melting. The material within the grain boundary regions is the Pu-Ir intermetallic phase.
Fig. 5. Backscatter electron images and corresponding x-ray dot maps for plutonium showing a typical grain structure. The matrix is uranium with the nominal tungsten composition.
Secondary electron image of an area containing the reduced form of PuO$_2$ (4000X).

X-ray dot map for plutonium (4000X).

X-ray dot map for iridium (4000X).

Fig. 6. Secondary electron image and corresponding x-ray dot maps for plutonium and iridium.

REFERENCES


