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PLUTONIUM AND URANIUM ANALYSIS BY GAMMA RAY SPECTROMETRY

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ABSTRACT

Non destructive gamma ray techniques have been developed for analysis of isotopic abundances and concentrations of plutonium and uranium in the respective product solutions of a reprocessing plant. The method involves analysis of gamma rays emitted from the sample and uses a multichannel analyser system. Data reduction and interpretation of these techniques are tedious and time consuming. In order to make it possible to use them in routine analysis, computer programs have been developed in HP-BASIC language which can be used in HP-9845B desktop computer. A set of programs, for plutonium estimation by high resolution gamma ray spectrometry and for on-line measurement of uranium by gamma ray spectrometry are described in this report.

1. INTRODUCTION

Determination of plutonium and uranium in the product solutions of a reprocessing plant are normally carried out by controlled potential coulometry(1) and Redox potentiometry(2) for the purpose of nuclear material accounting. Though these methods are accurate, they are time consuming. The nondestructive analysis (NDA) techniques are increasingly in use for the timely characterization, accounting and hence safeguarding of special nuclear materials. The advantages of NDA methods are; i) simplicity and speed of analysis(3), ii) comparable accuracy and precision, iii) no sampling is required, if used as on-line, and iv) additional information of isotopic composition and Am241 content (in the case of Pu analysis) is available. In PREFRE laboratory NDA methods are standardised for the measurement of plutonium and uranium using passive gamma ray spectrometry. These methods use a multichannel analyser with suitable detectors. Because of tedious and time consuming steps of data reduction and data interpretation of these methods, computers are commonly employed for carrying out this work. A computer program in FORTRAN language has already been developed by Gunnink(4) for the data reduction in plutonium analysis.

In our laboratory, two different programs in HP-BASIC language have been developed for the computation of data in plutonium and uranium analysis. These programs are written to use on a HP-9845B desktop computer interfaced

to a disk mass storage device. The present paper describes in detail the methods and the software involved in the data reduction of these techniques.

2. MEASUREMENT OF PLUTONIUM IN PRODUCT SOLUTION BY

 HIGH RESOLUTION GAMMA RAY SPECTROMETRY.

2.1 Method:

Plutonium isotopes and their daughter products emit more than 400 characteristic gamma rays. Isotope ratios of plutonium can be determined by measuring selected close lying gamma ray pairs in different energy regions. Seven of them in low energy region from 26 keV to 148 keV are used in the present work. The isotopes and gamma energies chosen are shown in Table 1. In general the isotope ratio of two plutonium isotopes i and j is determined by measuring intensities of selected gamma rays a and b using the following equation:

$$\frac{N_i}{N_j} = \frac{I_a}{I_b} * \frac{BI_b}{BI_a} * \frac{T(1/2)_i}{T(1/2)_j} * \frac{RE_b}{RE_a} \text{ -----} 1.$$

where, I = intensity of gamma ray(count rate).

BI = branching intensity.

T(1/2)= half life of the isotope.

RE = relative efficiency.

2.2 Instrumental

The experimental set up used is shown in fig.1. A high purity germanium (HPGe) detector having a sensitive volume one c.c. and resolution of 485 ev at 122 kev with vertical cryostat configuration and connected to a SILENA 8K multi-channel analyser (MCA) is used in this work.

The program for data reduction is run on a HP-9845B desk top computer. It has a 640K memory and mass storage devices of two cassette drives and two 8 inch flexible disc drives of 100K and 500K memory respectively. It is also equipped with an internal thermal printer and an external EPSON dot matrix printer.

2.3 Procedure

Plutonium product solutions from the intermediate product tanks(PUP & PUS) and plutonium oxide product dissolved solutions can be analysed by this technique. Solutions ranging in plutonium concentration from 1 g/l to 20 g/l are analysed. 2ml of plutonium nitrate solution is taken in a small sample bottle, sealed and pushed into another plastic bottle of nearly 5ml capacity. This sample is placed in a fixed position above the detector. Counting of the sample is carried out on the HPGe-MCA system for 1800 seconds. The analyser gives only gross and net counts under different regions of interest (Peaks). Further data reduction and data interpretations are carried out using the program titled PU/GS.

2.4 Software description.

Program is prepared in the operator interactive method. It is convenient method as the operator has only to answer the questions prompted by the program. Software involved is shown in appendix-1 .

2.4.1 Data inputs

Out put of the MCA system form the data inputs. These include sample identification, date of analysis, counting time and area counts of different regions of interest.

2.4.2 Calculations of relative efficiencies.

It is evident from equation 1 that to calculate the ratio of two isotopes from the count rate of two close lying energy peaks of these isotopes, it is necessary to know the efficiencies/ relative efficiencies of these energy peaks. Relative efficiency depends upon the detector efficiency, energy of the peak, sample matrix and sample to detector geometry. Hence first step of the program is to determine the relative efficiencies of different energy peaks. Option is provided in the program to use either an internal calibration method or a standard calibration method for obtaining the relative efficiencies.

Internal calibration method is normally employed for the analysis of plutonium solutions of higher concentration and for the plutonium isotopic assay in oxide samples. In this method the information of relative efficiencies is

generated from the measured sample spectrum itself. 26.34, 33.19 and 59.54 Kev lines of Am241 are chosen in lower energy region and 129.29, 144 and 203 Kev lines of Pu239 isotope are chosen in the higher energy region. Calculations carried out by the program are shown below.

$$Re1(26.34) = I1(26.34)/BI(26.34) \quad \text{-----}2.$$

$$Re2(33.19) = I2(33.19)/BI(33.19) \quad \text{-----}3.$$

$$Re3(59.54) = I3(59.54)/BI(59.54) \quad \text{-----}4.$$

where, $Re_i(E)$ is the relative efficiency of peak i of energy E and $I_i(E)$ & $Bi(E)$ are the area counts and branching intensities of respective energy peaks. Relative efficiencies thus determined are fitted into quadratic equation of the type shown, to extend the method of calculation of relative efficiencies for the other energy peaks.

$$Re1(26.34) = a_0 + a_1 E_1 + a_2 E_1^2 \text{-- (E}_1=26.34\text{keV)} \text{----}5$$

$$Re2(33.19) = a_0 + a_1 E_2 + a_2 E_2^2 \text{-- (E}_2=33.19\text{keV)} \text{----}6$$

$$Re3(59.54) = a_0 + a_1 E_3 + a_2 E_3^2 \text{-- (E}_3=59.54\text{keV)} \text{----}7$$

where, a_0 , a_1 and a_2 are constants, found by following equations;

$$a_2 = \frac{[(E_2-E_3)*(Re_1-Re_2)] - [(E_1-E_2)*(Re_2-Re_3)]}{[(E_1-E_2) * (E_2-E_3) * (E_1-E_3)]} \quad \text{-----}8.$$

$$a_1 = \frac{(Re_1-Re_2) - a_2(E_1^2 - E_2^2)}{(E_1-E_2)} \quad \text{-----}9.$$

$$a_0 = Re_1 - a_1 E_1 - a_2 E_1^2 \quad \text{-----}10.$$

Having calculated the constants, relative efficiencies of other energy peaks in the low energy region (Pu isotopes) are calculated using the same quadratic equation. For

higher energy region (129 to 203 kev), Pu239 lines are used and relative efficiencies are calculated by the same procedure.

Standard calibration method for obtaining relative efficiencies is followed for plutonium nitrate solutions in a low range of concentration (1 to 15 g/l) where change in the relative efficiency due to sample attenuation is minimum. In this method relative efficiencies of different energy peaks are experimentally determined using a set of standards and their values are available in the program for further calculations.

2.4.3 Isotope ratio calculation.

The isotope ratio of two plutonium isotopes is determined by measuring intensities of selected close lying gamma rays and using equation 1. Pu(240/239) ratio is calculated using the pairs of gamma lines 43.48 kev and 38.66 kev as well as 43.48 kev and 51.63 kev lines as follows.

$$N091 = \frac{I(43.48)}{I(51.63)} * \frac{Re(51.63)}{Re(43.48)} * 1.6134E-1 \quad \text{-----11.}$$

$$N092 = \frac{I(43.48)}{I(38.66)} * \frac{Re(38.66)}{Re(43.48)} * \frac{6537*1.05E-4}{24150*4.5E-4} \quad \text{----12.}$$

Average of these two isotope ratios is taken as the (240/239)ratio of the sample.

$$N09 = (N091 + N092)/2 \quad \text{-----13.}$$

Same way (241/239) ratio is calculated by using 148.57 kev & 129.29 kev lines and is given by

$$N_{191} = \frac{I(148.57)}{I(129.29)} * \frac{Re(129.29)}{Re(148.57)} * 2.0099E-2 \quad \text{-----14.}$$

For Am241/Pu239 ratio 59.05 kev and 51.63 kev lines are used. Since Pu241 also contributes to 59.05 peak, a correction is incorporated in the calculation.

$$Na_9 = \left[\frac{I(59.05)}{I(51.63)} * \frac{Re(51.63)}{Re(59.05)} - N_{191} * 5.2352E1 \right] * 1.3485E-5 \quad \text{-----15.}$$

In the case of (238/239) ratio 43.48 kev and 38.66 kev as well as 43.48 kev and 51.63 kev lines are chosen. Here again correction has been incorporated for the contribution of Am241 and Pu241 at 43.48 kev gamma line of Pu238.

$$N_{891} = \left[\frac{I(43.48)}{I(38.66)} * \frac{Re(38.66)}{Re(43.48)} - Na_9 * 3.6917E2 - N_{191} * 9.3586E-2 \right] * 9.7023E-4 \quad \text{-----16.}$$

$$N_{892} = \left[\frac{I(43.48)}{I(51.66)} * \frac{Re(51.68)}{Re(43.48)} - Na_9 * 1.4357E2 - N_{191} * 3.6395E-2 \right] * 2.4949E-3 \quad \text{-----17.}$$

(238/239) ratio is calculated from the average of two ratios obtained.

$$N_{89} = (N_{891} + N_{892})/2 \quad \text{-----18.}$$

Since Pu242 does not emit any characteristic gamma (242/239) ratio is computed by the relation,

$$N_{29} = K * (240/239) * (241/239) \quad \text{-----19.}$$

where K is a constant which depends upon the type of reactor. For power reactor fuels of CANDU type K is equal to 0.73 and this factor is obtained from mass spectrometric data of earlier processing campaign.

2.4.4 Isotopic composition/specific activity calculation.

Atom and weight percent of plutonium are calculated from the isotope ratios obtained and atomic mass of different plutonium isotopes. Using the nuclear data, the program also calculates the specific activity of plutonium which is required for use in radiometric analysis. Isotope ratios of 238/239, 239/239, 240/239, 241/239 and 242/239 are represented by R1 to R5 respectively.

$$T = \sum R_i \quad \text{-----20.}$$

$$\text{Atom percent of isotope } i (A_{pi}) = \frac{R_i}{T} * 100 \quad \text{--21.}$$

where, i = 1 to 5 for isotopes 238 to 242.

Weight percent is calculated using the atomic mass of different isotopes (Mi) and isotopic ratios (Ri)

$$\text{Average atomic weight} = \frac{\sum (R_i * M_i)}{T} \quad \text{-----22.}$$

$$\text{Weight percent of isotope } i \quad (W_{pi}) = \frac{R_i * M_i}{\sum (R_i * M_i)} * 100 \quad \text{----23.}$$

Informations regarding the specific activity of different

isotopes in dpm/microgram (S_{pi}) are available from the nuclear data i.e., atomic mass, half life of the respective isotopes and Avogadro number.

Specific activity of plutonium in sample (dpm/ug) is calculated from the weight percent of different isotopes and their specific activity and is given by

$$\text{Specific activity of plutonium} = \frac{\sum (W_{pi} * S_{pi})}{100} \quad \text{----24.}$$

(dpm/ug)

2.5 Plutonium concentration determination.

Plutonium concentration is determined in solution from the intensities of 51 keV and 129 keV gamma lines of Pu239. Intensities(count rates) of these gamma lines with change in concentration are shown in figures 2 and 3. It can be seen that at 129 keV for a concentration range of 1 to 15g/l, the data fits with a linear curve of the type $Y = mX + C$, where as at 51 keV the curve is found to deviate slightly from the linear equation above 10 g/l due to sample attenuation. The program gives option to the user to find the concentration of plutonium using the exponential relation of the type $Y = a * e^{-bx}$ or using linear equation in short intervals.

2.6 Data out.

Isotopic composition and plutonium concentration are printed out on a dot matrix printer or on an internal thermal printer. A typical out put is shown in Appendix-2.

3. MEASUREMENT OF URANIUM CONCENTRATION BY GAMMA RAY SPECTROMETRY.

3.1 Method

Uranium isotopes emit several gamma rays. The gamma rays associated with the daughter products of U235 and U238 185.7 kev, and 1001 kev respectively are used in this work. Isotope ratio is calculated from the ratio of measured intensities of these gamma rays.

3.2 Procedure.

A coaxial high purity germanium detector with a resolution of 1.8 kev at 1.33 Mev and volume of 50cc, coupled to a 8K multichannel analyser is used. A sketch of the set up is shown in figure 4. The sample cell of 50cc capacity is situated above the detector and uranium solution is pumped into the cell and circulated continuously through the sample cell during the counting time of 1800 seconds. A Set of uranium standards in the concentration range of 50 g/l to 300 g/l are used for the calibration of the system.

3.3 Software description.

This program titled UONLINE is 'user friendly program'. Operator with minimum knowledge of computer can calculate the results using this program. Appendix-3 shows the listing of the program to perform this analysis.

3.3.1 Inputs

Data out put of multichannel analyser are entered along with other inputs namely, sample identification, date of analysis, and counting time.

3.3.2 Calculation of efficiency factor.

Efficiency factor of an energy peak includes both branching intensity and detection efficiency. They are predetermined using a set of standards. At 1001 keV (U236) there is little change in the sample attenuation over the entire concentration range and hence a constant efficiency factor (EF) is used. Sample attenuation of 185.7 keV energy peak (U235) increases with the concentration and hence the program includes a self calibration to compute the efficiency factor of 185.7 keV from the count rate obtained for the sample using a linear relation (fig.5)

3.3.3 Isotope ratio calculation.

Uranium isotope ratio of 235/238 is calculated from the intensities of gamma rays by,

$$R(235/238) = \frac{I(185.7)}{I(1001)} \times \frac{EF(1001)}{EF(185.7)} \times \frac{T_{1/2}(235)}{T_{1/2}(238)} \quad \text{----25}$$

Where $T_{1/2}$ is the half life of the isotope. From this ratio weight fraction of U238 is calculated.

3.3.4 Uranium concentration measurement.

Concentration of U238 is calculated from the linear relationship of the type $Y = MX + C$, where Y is the intensity (I) of the 1001 kev and X is the U238 concentration (fig 6). M and C which are predetermined using a set of standards are available as data in the program.

Uranium concentration is further calculated by dividing U238 concentration with weight fraction of U238.

3.4 Data out

U235 content and uranium concentration are printed out. Options are provided for directing the data out to an internal thermal printer or an external dot matrix printer.

4. DISCUSSIONS

The programs have been successfully used for the routine analysis of plutonium product solutions and aged uranium product solutions. The programs make the otherwise tedious data reduction of these techniques simpler and faster for routine analysis of plant samples. Tables 2 and 3 give the results obtained using these techniques.

The programs can be adopted on a personal computer with changes in the print out statements. Microsoft Basic version is also prepared to use with IBM-PC.

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Appendix - 1
 Listing of program for plutonium concentration
 and isotopic calculation by HRGS.

```

10  OPTION BASE 1
20  REM TITLE ---PU/GS
30  REM PROGRAM FOR NDA MEASUREMENT OF Pu ISOTOPIC CONC. BY HRGS
40  REM PREPARED BY A.D.MOORTHY ON 7/07/88
50  PRINTER IS 16
60  DIM E(12),Re(12),I(12),K(5),Sample$(30)
70  MAT READ E(12)
80  DATA 26.34,33.19,38.66,43.48,45.23,51.63,59.054,129.29,144.23,148.57,203.5
      2,208
90  DATA 238.0495,239.0522,240.0540,241.056,242.0587
100 MAT READ K
110 PRINTER IS 16
120 INPUT "DATE ?",Date$
130 INPUT "SAMPLE ?",Sample$
140 INPUT "COUNTING TIME seconds ?",Q
150 C=0
160 REM PROGRAM FOR CALCULATION BY STD. CALIBRATION METHOD
170 INPUT "Enter the area of 38, 43, 45, 51, 59, 129, 148 ",I(1),I(2),I(3),I(4
),I(5),I(6),I(7)
180 Re(7)=I
190 Re(8)=.78342*EXP(.02222*(I(2)/Q))
200 Re(9)=.96171*EXP(.0041657*(I(3)/Q))
210 Re(10)=1.02188*EXP(.007223*(I(4)/Q))
220 Re(3)=1.5104+1.8530E-4*(I(5)/Q)
230 Re(4)=.42945*EXP(.041439*(I(6)/Q))
240 Re(11)=.34454*EXP(.041439*(I(7)/Q))
250 N191=I(7)/I(6)+2.0099E-2*(Re(4)/Re(11))
260 Na9=I(5)/I(4)+(Re(10)/Re(3))-N191*5.2352E11*1.3485E-5
270 N891=I(2)/I(1)*(Re(7)/Re(8))-Na9*3.6917E2-N191*9.3586E-2)*9.7023E-4
280 N892=I(2)/I(4)*(Re(10)/Re(8))-Na9*1.4357E2-N191*3.6395E-2)*2.4949E-3
290 N89=(N891+N892)/2
300 N091=I(3)/I(4)*(Re(10)/Re(9))+1.6134E-1
310 N092=I(3)/I(1)*(Re(7)/Re(9))+6537*1.05E-4/(24150*4.5E-4)
320 N09=(N091+N092)/2
330 N29=.73*N09*N191
340 T=N89+N09*N191+N29+1
350 Ap(1)=100*N89/T
360 Ap(2)=100/T
370 Ap(3)=100*N09/T
380 Ap(4)=100*N191/T
390 Ap(5)=100*N29/T
400 Ap(6)=Na9*Ap(2)
410 W=0
420 FOR X=1 TO 5
430 D(X)=Ap(X)*K(X)
440 W=W+D(X)
450 NEXT X
460 Av_at_wt=W/100
470 FOR X=1 TO 5
480 Mp(X)=D(X)*100/W
490 NEXT X
500 Mp(6)=Ap(6)*241/Av_at_wt

```

```

510 PRINTER IS 16
520 PRINT "PUT ON THE EPSON PRINTER AND CONT. "
530 BEEP
540 PAUSE
550 PRINTER IS 6,2
560 PRINT TAB(10);"ISOTOPIC COMPOSITION BY HIGH RESOLUTION GAMMA SPECTROMETRY"
570 PRINT TAB(10);"*****"
580 PRINT
590 PRINT TAB(10);"SAMPLE:-";Sample$;TAB(52);"DATE:-";Date$
600 PRINT TAB(10);"METHOD:- Online measurement"
610 PRINT
620 PRINT TAB(15);"ISOTOPE";TAB(36);"ATOM PERCENT";TAB(58);"WEIGHT PERCENT"
T*
630 FIXED 5
640 PRINT TAB(15);"Pu-238";TAB(38);Ap(1);TAB(59);Wp(1)
650 PRINT TAB(15);"Pu-239";TAB(36);Ap(2);TAB(57);Wp(2)
660 PRINT TAB(15);"Pu-240";TAB(36);Ap(3);TAB(57);Wp(3)
670 PRINT TAB(15);"Pu-241";TAB(37);Ap(4);TAB(58);Wp(4)
680 PRINT TAB(15);"Pu-242";TAB(38);Ap(5);TAB(59);Wp(5)
690 PRINT TAB(15);"Am-241";TAB(38);Ap(6);TAB(59);Wp(6)
700 PRINT TAB(15);"AVERAGE AT.WT.";TAB(35);Av_at_wt
710 PRINT TAB(15);"-----"
-----"
720 PRINTER IS 16
730 PRINT
740 PRINT TAB(15);"RATIO OF ISOTOPE";TAB(40);"RATIO OBTAINED"
750 PRINT
760 PRINT TAB(20);"238/239(using 43/38)";TAB(44);NB91
770 PRINT TAB(20);"238/239(using 43/51)";TAB(44);NB92
780 PRINT TAB(20);"238/239( Average )";TAB(44);NB9;"*"
790 PRINT TAB(20);"240/239(using 45/51)";TAB(44);N091
800 PRINT TAB(27);"(using 45/38)";TAB(44);N092
810 PRINT TAB(27);"( average )";TAB(44);N09;"*"
820 PRINT TAB(20);"241/239(using 148/129)";TAB(44);N191;"*"
830 PRINT TAB(20);"242/239";TAB(44);N29;"*"
840 PRINT
850 PRINT TAB(20);"*-Ratios used for isotopic composition"
860 PRINT TAB(10);"*****"
*****"
870 PRINTER IS 6,2
880 ! Program for concentration measurement -ONLINE
890 Z=0
900 INPUT "CALIBRATION LINEAR or EXPONENTIAL or BOTH",M$
910 IF M$="L" THEN 1140
920 M=5.8677
930 C=7.67895
940 B1=13.14489
950 C1=.0807329
960 B2=1.494255
970 C2=.0883593
980 X=(1-(4)/Q-C)/M
990 PRINT X
1000 Con51=1-(4)/Q/B1*EXP(C1*X)

```

```

1010 PRINT Con51
1020 T_pu_con51=Con51*100/Wp(2)
1030 X=(1(4)/Q-C)/M
1040 Con129=I(6)/Q/B2*EXP(C2*X)
1050 PRINT Con129
1060 T_pu_con129=Con129*100/Wp(2)
1070 Av_con=(Con51+Con129)/2
1080 Av_t_pu_con=Av_con*100/Wp(2)
1090 Fu_con=Av_t_pu_con/W
1100 PRINTER IS 6,2
1110 PRINT "","EXPONENTIAL METHOD"
1120 PRINT "","-----"
1130 GOTO 1630
1140 Z=Z+1
1150 IF Z=2 THEN 1830
1160 Cr4=I(4)/Q
1170 IF Cr4<7.85 THEN 1270
1180 IF Cr4<23.82 THEN 1330
1190 IF Cr4<34.51 THEN 1390
1200 IF Cr4<50.12 THEN 1450
1210 PRINT 5
1220 M51=3.85047
1230 C51=24.6452
1240 M129=.473886
1250 C129=2.23867
1260 GOTO 1500
1270 PRINT 1
1280 M51=10.0639
1290 C51=0
1300 M129=1.02986
1310 C129=0
1320 GOTO 1500
1330 PRINT 2
1340 M51=8.8054
1350 C51=.98214
1360 M129=.93861
1370 C129=.07121
1380 GOTO 1500
1390 PRINT 3
1400 M51=7.69674
1410 C51=3.8572
1420 M129=.75897
1430 C129=.53707
1440 GOTO 1500
1450 PRINT 4
1460 M51=5.9280
1470 C51=10.9001
1480 M129=.68893
1490 C129=.81597
1500 U=I(4)/Q

```

```

1510 V=I(6)/Q
1520 PRINT U,V
1530 Con51=(U-C51)/M51
1540 Con129=(V-C129)/M129
1550 T_pu_con51=Con51*100/Wp(2)
1560 T_pu_con129=Con129*100/Wp(2)
1570 Av_con=(Con51+Con129)/2
1580 Av_t_pu_con=Av_con*100/Wp(2)
1590 PRINTER IS 6,2
1600 PRINT " ", "LINEAR METHOD"
1610 PRINT " ", "-----"
1620 Print=2
1630 PRINTER IS 6,2
1640 PRINT TAB(23); "ONLINE MEASUREMENT OF PLUTONIUM CONCENTRATION"
1650 PRINT TAB(23); "-----"
1660 STANDARD
1670 PRINT TAB(13); "SAMPLE: -"; Sample$; TAB(59); "DATE: -"; Date$
1680 PRINT TAB(15); "COUNT TIME: -"; Q; TAB(59); "COUNT NO.: -"; C
1690 PRINT
1700 FIXED 5
1710 PRINT TAB(32); "PLUTONIUM CONCENTRATION OF THE SAMPLE (G/L)"
1720 PRINT TAB(30); " (Using51)      (Using129)      ( Average )"
1730 PRINT
1740 PRINT TAB(15); "Pu-239"; TAB(30); Con51; TAB(43); Con129; TAB(59); Av_con
1750 PRINT TAB(15); "TOTAL Pu"; TAB(30); T_pu_con51; TAB(43); T_pu_con129; TAB(59); Av
_t_pu_con
1760 PRINT TAB(15); "-----"
.

1770 IF Print=2 THEN 1790
1780 IF W$="B" THEN 1140
1790 C=C+1
1800 IF C=2 THEN 1830
1810 GOTO 160
1820 PRINTER IS 16
1830 END

```

Appendix-2

A typical out put for isotopic composition and plutonium concentration.

ISOTOPIC COMPOSITION BY HIGH RESOLUTION GAMMA SPECTROMETRY.

SAMPLE :- 293 Pu Lab Date:- 8/9/88
 METHOD :- Online measurement

ISOTOPE	ATOM PERCENT	WEIGHT PERCENT
Pu-238	.09353	.09302
Pu-239	73.90958	73.81292
Pu-240	21.44993	21.51166
Pu-241	3.75205	3.77855
Pu-242	.79491	.80385
Am-241	.00303	.00305
AVERAGE AT. WT.	239.36523	

 LINEAR METHOD

ONLINE MEASUREMENT OF PLUTONIUM CONCENTRATION

SAMPLE :- 293 Pu Lab Date:- 8/9/88
 COUNT TIME:- 1800 COUNT NO.:-1
 PLUTONIUM CONCENTRATION OF THE SAMPLE(G/L)

	(Using 51)	(Using 129)	(Average)
Pu-239	9.01588	9.26920	9.14254
TOTAL Pu	12.21451	12.55769	12.38610

Appendix - 3

Listing of program for uranium concentration by on-line HRGS.

```

10  REM TITLE UOXLIME
20  REM PREPARED BY A.D.MODRTHY ON 22JANUARY 1987
30  INPUT "Enter the date of analysis & CONT.",Date$
40  INPUT "Enter the sample ident. & CONT. ",S$
50  INPUT "Enter the counting time in secods & CONT.",Q
60  INPUT "Enter the area of 63, 163, 185, 1001 Kev peaks & CONT. ",I(1),I(2
),I(3),I(4)
70  FOR X=1 TO 4
80  Cr(X)=I(X)*3600/Q
90  NEXT X
100 E(1)=2.08215E-3-2.5262E-8*Cr(1)
110 E(2)=4.46126E-3-1.66169E-7*Cr(2)
120 E(3)=4.58271E-2-1.1970E-7*Cr(3)
130 E(4)=1.0717E-4
140 US81=Cr(3)/Cr(1)+E(1)/E(3)+2.604/16.47
150 U48=.00005
160 T1=1+US81+U48
170 Af81=1/T1
180 US82=Cr(3)/Cr(4)+E(4)/E(3)+2.604/16.47
190 T2=1+US82+U48
200 Af82=1/T2
210 US83=Cr(2)/Cr(1)+E(1)/E(2)+2.604/16.47
220 T3=1+US83+U48
230 Af83=1/T3
240 US84=Cr(2)/Cr(4)+E(4)/E(2)+2.604/16.47
250 T4=1+US84+U48
260 Af84=1/T4
270 ! CONC. CALCULATION USING 63 KEV PEAK
280 A=19.73639
290 B=5.31138E-5
300 CB63=A*EXP(B*Cr(1))
310 A2=5.05753E-7
320 A1=.0393837
330 A0=3.68828
340 CB1001=A2+Cr(4)^2+A1*Cr(4)+A0
350 Cu1=CB63/Af81
360 Cu2=CB1001/Af82
370 Cu3=CB63/Af83
380 Cu4=CB1001/Af84
390 PRINTER IS 6,2
400 BEEP
410 DISP "PUT ON THE EPSON PRINTER & CONT. "
420 PAUSE

```



```

430 PRINT "          URANIUM BY GAMMA SPECTROMETRY"
440 PRINT "          -----"
450 PRINT "DETECTOR: Coaxial                      DATE: ";Date$
460 PRINT "SAMPLE :";S$;"                      COUNT TIME(sec.):";Q
470 PRINT "....."
.
480 PRINT
490 PRINT "63Kev (area)    163Kev (area)    185.72Kev (area)    1001Kev (area)"
.
500 PRINT TAB(4);I(1);TAB(22);I(2);TAB(40);I(3);TAB(59);I(4)
510 PRINT "....."
.
511 FIXED 4
520 PRINT "CONC. OF URANIUM 238(Mg/ml) USING 63 Kev  :";CB63
530 PRINT "CONC. OF URANIUM 238(Mg/ml) USING 1001 Kev :";CB1001
531 STANDARD
540 IMAGE "235/238 RATIO          :";Z.DDDDDD
550 IMAGE "ATOM FRACTION ON 238    :";Z.DDDDD
560 IMAGE "TOTAL URANIM CONC. (Mg/ml) :";DDD.DDD
570 PRINT
580 PRINT "PEAKS USED 63 Kev & 187.5 Kev"
590 PRINT "-----"
600 PRINT USING 540;U581
610 PRINT USING 550;Af81
620 PRINT USING 560;Cu1
630 PRINT
640 PRINT "PEAKS USED 1001 Kev & 187.5 Kev"
650 PRINT "-----"
660 PRINT USING 540;U582
670 PRINT USING 550;Af82
680 PRINT USING 560;Cu2
690 PRINT
700 PRINT "PEAKS USED 63 Kev & 163 Kev"
710 PRINT "-----"
720 PRINT USING 540;U583
730 PRINT USING 550;Af83
740 PRINT USING 560;Cu3
750 PRINT
760 PRINT "PEAKS USED 1001 Kev & 163 Kev"
770 PRINT "-----"
780 PRINT USING 540;U584
790 PRINT USING 550;Af84
800 PRINT USING 560;Cu4
810 PRINT
820 PRINT "....."
.
830 DISP "CALCULATIONS DONE. IF YOU WANT TO REUSE JUST COMT "
840 END

```

Table 1.

Gamma ray used for high resolution gamma spectrometry

Isotope	Energy of the peak (Kev)	Branching intensity	Interference.
Pu 238	43	3.93E-04	Pu-241, Am-241
239	38	1.05E-04	
	51	2.7 E-04	
	129	6.26E-05	
240	45	4.53E-04	
241	145	1.87E-06	
Am-241	59	5.24E+01	

Table 2.

Plutonium concentration by HRGS-NDA method.

S. No.	Sample No.	Tank	Pu Concentration(mg/g)		B A
			Coulometry (A)	HRGS (B)	
1.	4	Audit	7.267	7.343 +/-0.068	1.0105
2.	606173	Pus	11.823	11.779 +/-0.037	0.9963
3.	606261	Pus	10.477	10.644 +/-0.259	1.0159
4.	606271	Pus	10.710	10.429 +/-0.036	0.9738
5.	606712	Pus	11.267	11.267 +/-0.211	1.0000
Average					0.9993
Std. dev. +/-					0.0163

Table 3.

Uranium concentration by Gamma ray spectrometry

 and Potentiometry.

S.No.	Sample No.	Concentration (mg/ml)		A --- B	U235/U238 ratio by HRGS
		HRGS (A)	Potentiometry (B)		
1.	STD-5 +/-	281.53 0.43	283.53	0.9929	0.00769 +/-0.00003
2.	S-1 +/-	206.69 0.36	208.44	0.9916	0.00483 +/-0.00003
3.	S-2 +/-	257.61 3.77	266.13	0.9680	0.00504 +/-0.00012

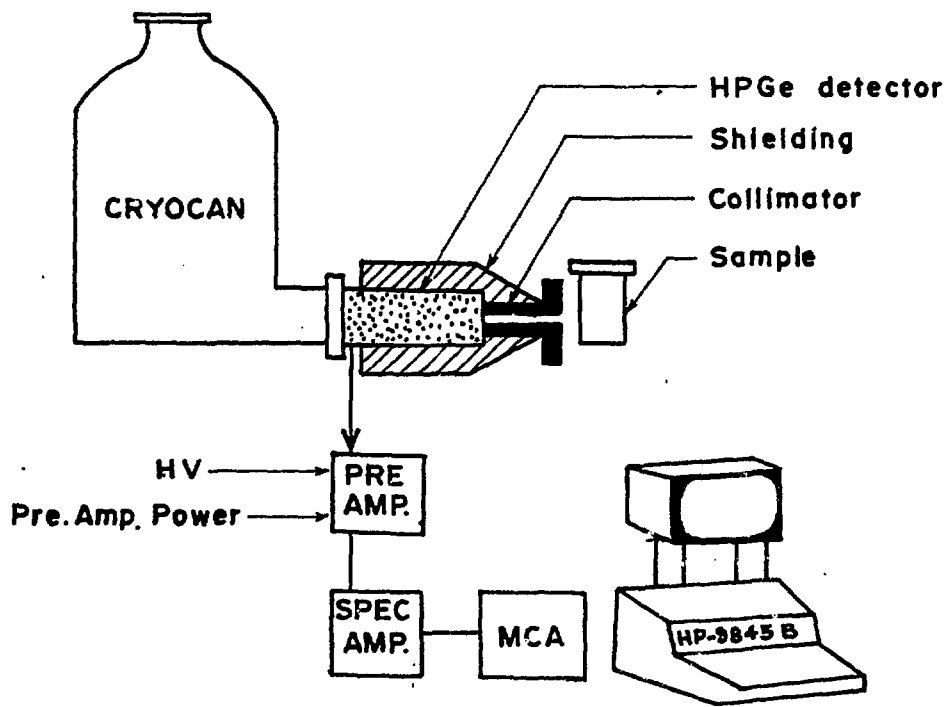


Fig.1. Set up used for Pu measurement.

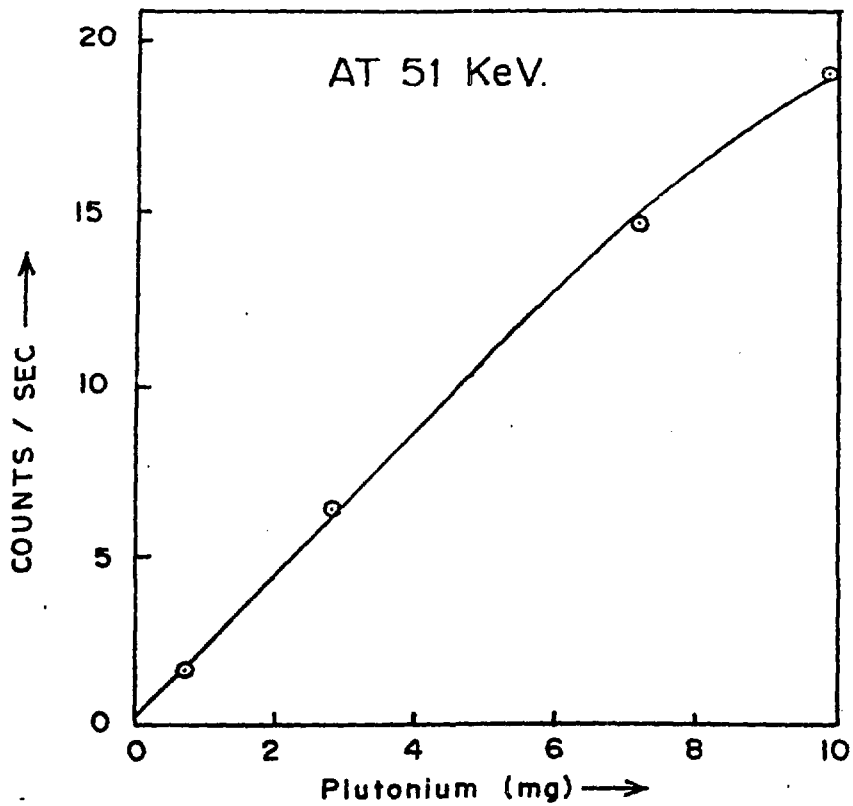
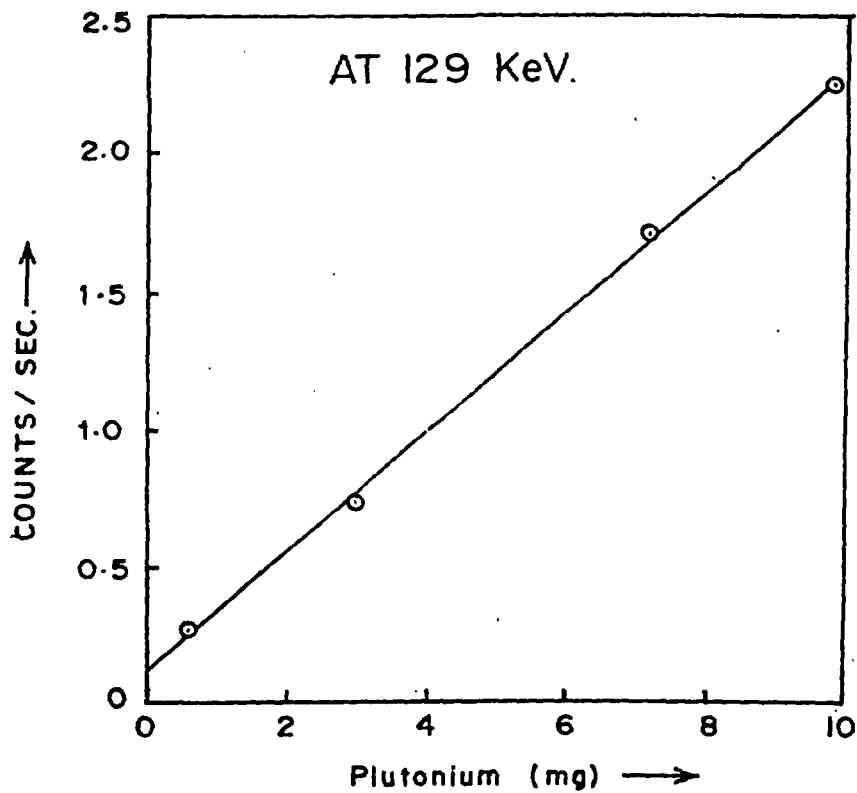


Fig. 2. Plutonium concentration vs. count rate.



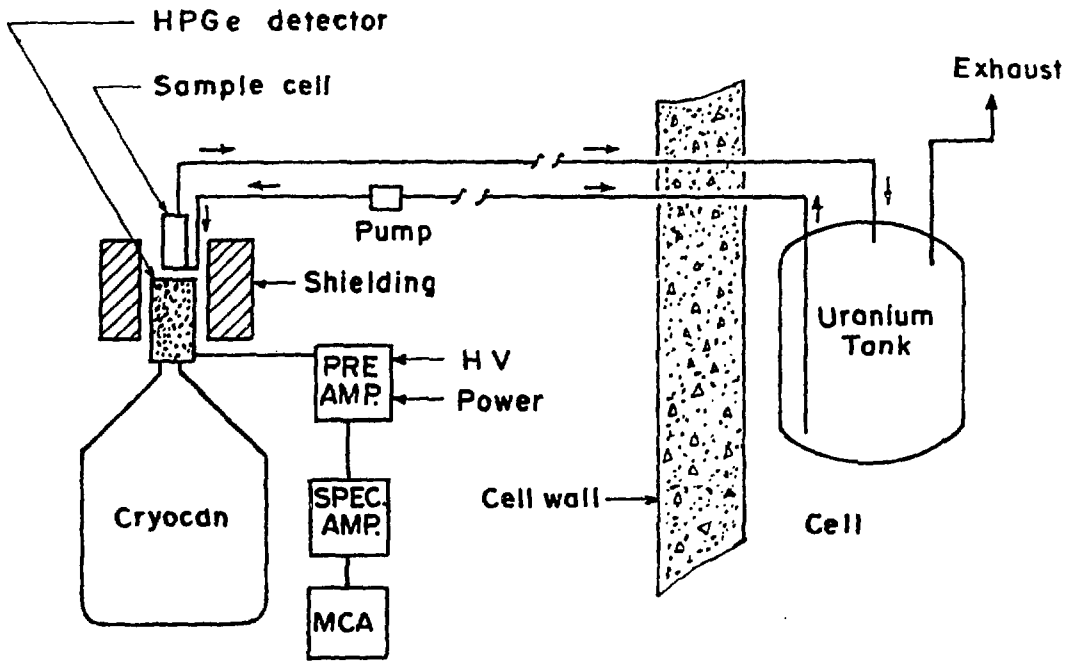


Fig.4. Setup for Uranium online measurement.

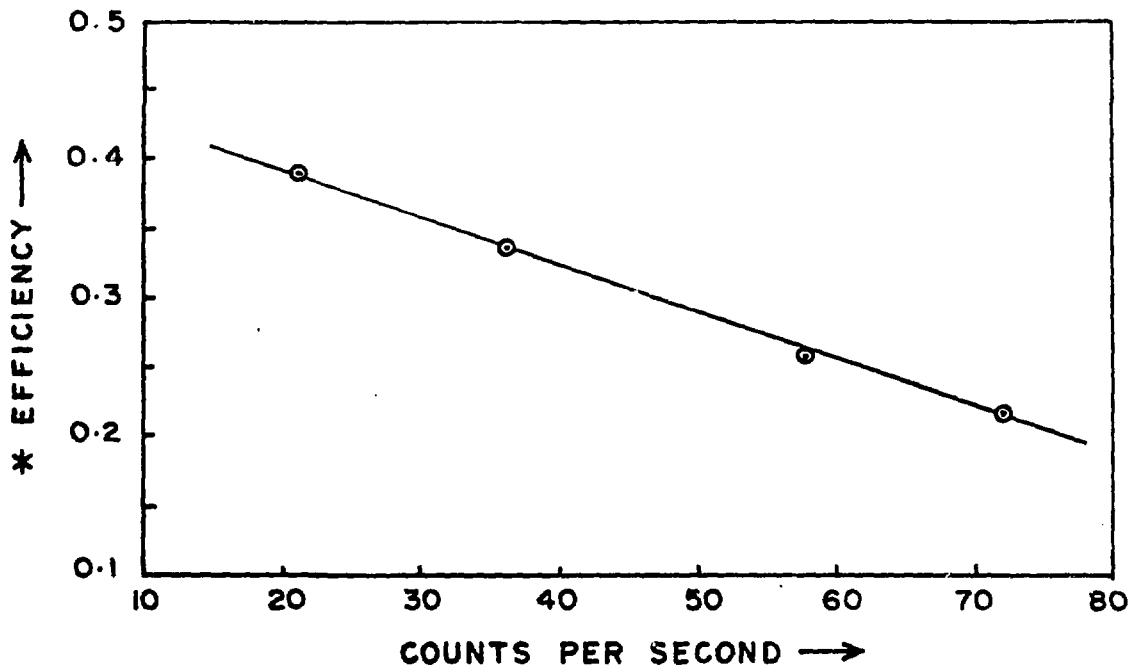


Fig.5. Efficiency vs. count rate at 185.7 KeV.

$$* \text{ Efficiency} = \frac{\text{Observed count rate}}{\text{Theoretical count rate}} \quad (\text{at } 185.7 \text{ KeV.})$$

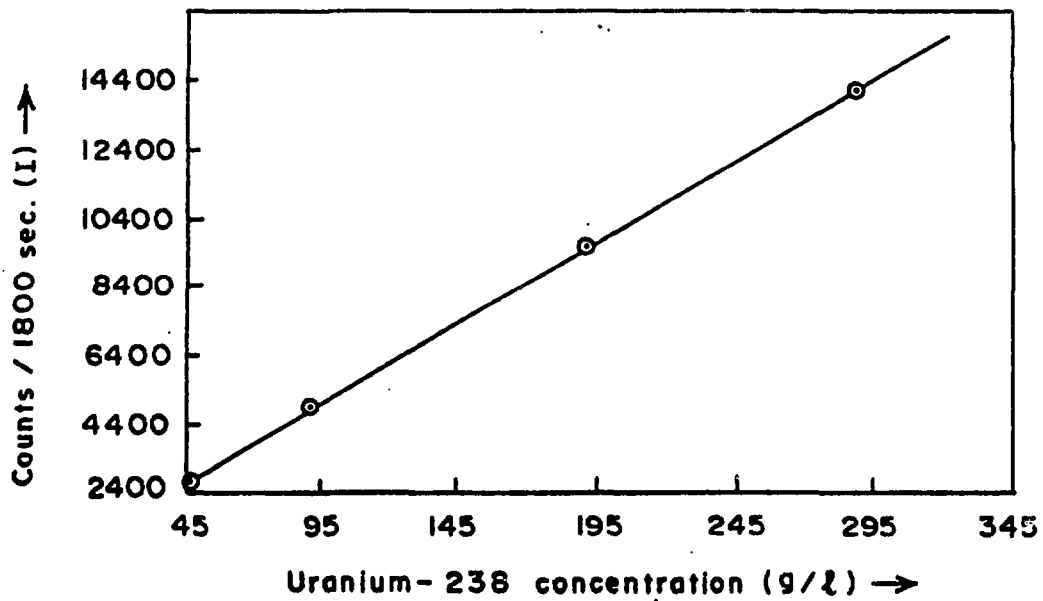


Fig. 6. Uranium concentration calibration curve using 1001 KeV peak.

