

Design of a High-Resolution High-Stability Positioning Mechanism for Crystal Optics

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Abstract. We present a novel miniature multi-axis driving structure that will allow positioning of two crystals with better than 50-nrad angular resolution and nanometer linear driving sensitivity. The precision and stability of this structure allow the user to align or adjust an assembly of crystals to achieve the same performance as does a single channel-cut crystal, so we call it an “artificial channel-cut crystal.” In this paper, the particular designs and specifications, as well as the test results, for a two-axis driving structure for a high-energy-resolution artificial channel-cut crystal monochromator are presented.

INTRODUCTION

With the availability of third-generation of hard x-ray synchrotron radiation sources, such as the Advanced Photon Source (APS) Argonne National Laboratory (ANL), x-ray inelastic scattering and x-ray nuclear resonant scattering provide powerful means for investigating vibrational dynamics of variety of materials and condensed matter systems.

The APS SRI-CAT 3-ID beamline is dedicated to high-energy-resolution x-ray scattering studies in the energy range of 6-30 keV [1]. A special 2.7-cm-period undulator, optimized for peak brilliance is installed. The beamline basic components include filters, white-beam slits, integral shutters, and the Kohzu double-crystal monochromator with water-cooled diamond crystals as a pre-monochromator. The beamline special components, such as custom-built high-energy-resolution monochromators and a dual-function (collimating or focusing) x-ray mirror system, provide a high flexibility for the optical system, so that users can optimize the beamline configuration for various applications. For instance, a 4-bounce high-resolution monochromator using a nested channel-cut crystal approach was used to deliver a x-ray beam with meV bandpass for x-ray inelastic scattering experiments [2].

There are design restrictions to the nested channel-cut geometry. Because these two channel-cut crystals are nested within each other, the size of the channel-cut crystals becomes an important design factor. The availability of large crystals with good long-range crystallinity restricts the size of the outer channel-cut crystal. On the other hand, the input beam power absorbed by the first optical surface on the outer channel-cut

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crystal can reach a fraction of a Joule and can cause crystal local temperature and strain variations. In certain high-energy-resolution applications, it becomes a major restriction to the optical design. To overcome these obstacles, we have developed a novel miniature multi-axis driving structure [3]. The precision and stability of this structure allow us to align or adjust an assembly of crystals to achieve the same performance as does a single channel-cut crystal, so we call it an “artificial channel-cut crystal.” Using this structure, we can make an outer channel-cut crystal large enough to optimize the nested monochromator’s performance and compensate the crystal local temperature and strain variations for the two optical surfaces on the crystals.

DESIGN SPECIFICATIONS

The artificial channel-cut crystal was designed for a novel nested high-energy-resolution monochromator, which is optimized for an ^{151}Eu nuclear resonance experiment at the energy of 21.542 keV. The high-energy-resolution monochromator uses a symmetric silicon (15 11 3) channel-cut crystal nested within an asymmetrically cut silicon (4 4 0) artificial channel-cut crystal. This optical design can produce a 1-meV resolution beam with a high throughput. However, if we use a natural channel-cut crystal to make the outer channel-cut crystal, the diffraction faces can be separated by 200 mm, which makes it difficult to avoid problems associated with strain and temperature variations.

We use two asymmetrically cut silicon (4 4 0) crystals, which are each sized 25 mm x 25 mm x 50 mm, to act as an artificial outer channel-cut crystal. The major specification for the artificial channel-cut crystal structure is the angular alignment capability between the two crystals. According to the 300-nrad Darwin width of the silicon (4 4 0) in this asymmetrically cut geometry, a 50-nrad pitch alignment resolution is needed. Long-term positioning stability is also very important to the artificial channel-cut crystal. In a temperature-controlled environment ($\pm 0.2^\circ\text{C}$), an angular drifting rate less than 25-nrad per hour is required. Table 1 lists the design specifications for this (4 4 0) artificial channel-cut crystal. Fig. 1 shows the artificial channel-cut crystal mounted on the Kohzu monochromator stage in the APS 3-ID-B experimental station.

Maximum Overall Dimension	216 mm x 212 mm x 92 mm
Main Shaft Diameter	10 mm
Maximum Thickness in Nested Area	30 mm
Single Crystal Size	25 mm x 25 mm x 50 mm
Number of Angular Alignment Axis	2
Angular Alignment Resolution (Pitch)	50 nrad
Angular Alignment Resolution (Roll)	600 nrad
Angular Alignment Stability (Pitch)	Drift less than 25 nrad per hour
Angular Alignment Stability (Roll)	Drift less than 100 nrad per hour
Angular Alignment Range (Pitch)	0.6 degree
Angular Alignment Range (Roll)	2 degree

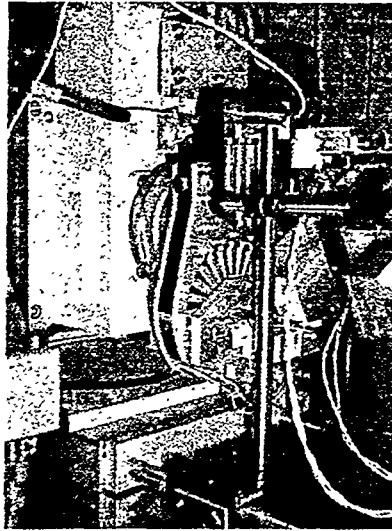


Figure 1. An artificial channel-cut crystal mounted on the Kohzu monochromator stage in the APS 3-ID-B experiment station.

HIGH-STIFFNESS WEAK-LINK MECHANISM DESIGN

Designing such a miniature multi-axis driving structure with high stiffness and nanometer sensitivity is challenging. The novelty of this new structure is combining the closed-loop controlled piezoelectric transducer (PZT) technology with a novel high-stiffness weak-link design. Using stacked thin metal sheets configured and manufactured by chemical etching and lithography techniques, we were able to design a planar-shaped, high-stiffness, high-stability weak-link structure for artificial channel-cut crystal use (see Fig.2).

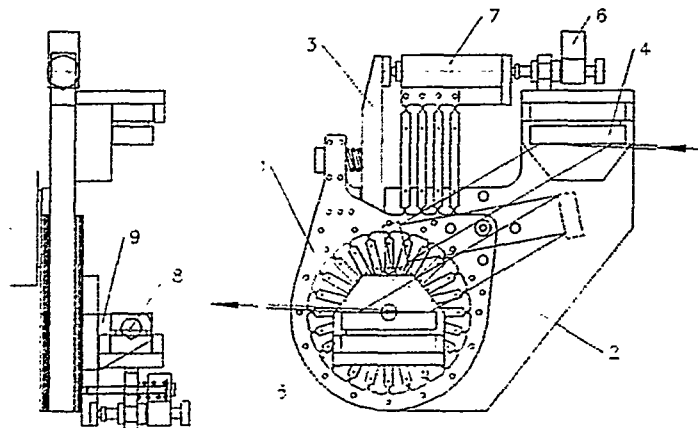


Figure 2. Design of the miniature multi-axis driving structure for an artificial channel-cut crystal.

The structure consists of three sub-assemblies: one base structure and two crystal holders. The base structure includes a compact sine-bar driving mechanism for the crystal pitch alignment, which is the key component of the whole structure. There are two groups of stacked thin metal weak-link structures (1) mounted on each side of the base plate (2). A sine-bar (3) is installed on the center of the planar rotary shaft for the pitch alignment between the two (4 4 0) single crystals (4, 5). Two linear drivers are mounted on the base plate serially to drive the sine-bar. The rough adjustment is performed by a Picomotor [5] (6) with a 20-nm to 30-nm step size. A Queensgate [6] closed-loop controlled PZT (7) with capacitance sensor provides 1-nm resolution for the pitch fine alignment. A pair of commercial flexure bearing (8) is mounted on one of the crystal holders (9), and a Picomotor driven structure (10) provides the roll alignment for the crystal.

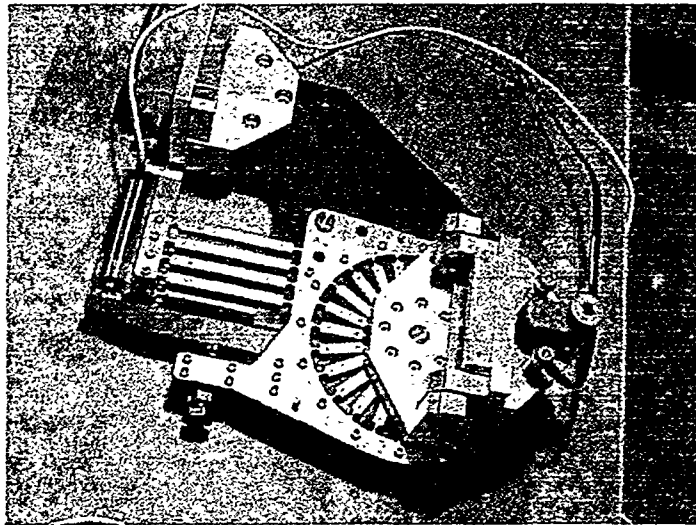


Figure 3. Photograph of the weak-link Structure mounted on the base plate.

Fig. 3 shows the shape of the metal weak-link sheet, which is produced by a photochemical machining process. Two motion structures are designed on the same metal sheet. A wheel-shaped weak-link group performs as a planar rotary shaft, and a parallelogram-shaped weak-link group acts as a linear slide. To optimize the system stiffness, we have chosen overconstrained mechanisms in this design. The precision of the modern photochemical machining process using lithography techniques make it possible to construct a strain-free (or strain limited) overconstrained mechanism on thin metal sheet. By stacking these thin metal weak-link sheets with align-pins, we can construct a solid complex weak-link structure with a reasonable cost. For our first prototype, 250- μm thick stainless steel sheet was used. Each group consists of twenty weak-link sheets. 0.6 degree adjustment range was reached, which was agreed with the finite element analysis result. Fig. 4 shows a finite element simulation for the wheel-shaped weak-link displacement under a 0.89-Nm torsion load. In this case, the maximum displacement on the weak-link is 94- μm , which is corresponding to a 0.25 degree angular motion on the planar shaft, and the maximum stress in the weak region is 175-Mpa. More analysis for this overconstrained mechanism will be discussed in a separate paper later.

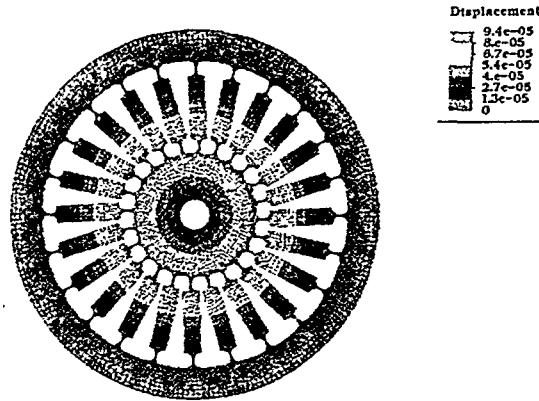


Figure 4. A finite element simulation for the wheel-shaped weak-link displacement under a 0.89-Nm torsion load. The maximum displacement on the weak-link is 94- μ m.

SENSITIVITY TEST WITH LASER ENCODER

We have tested the sensitivity of the weak-link sine-bar structure with a laser Doppler angular encoder. A 200-mm-long aluminum-arm is mounted on the center of the planar rotary shaft, perpendicular to the sine-bar. A set of prisms are mounted at the end of the arm as a multi-reflection displacement sensor [7]. During this test, a batch of 5-nm incremental steps are applied on the sine-bar by the Queensgate PZT. Fig. 5 shows a serial of angular steps recorded from the laser encoder with an averaging step size of 33-nrad.

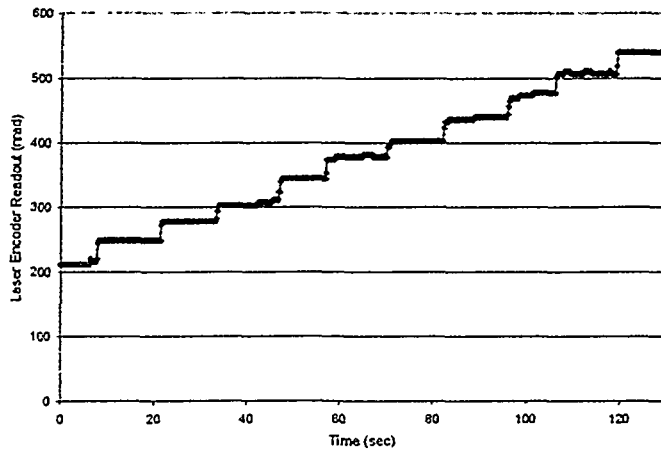


Figure 5. Sensitivity test of the weak-link sine-bar structure. The averaging step size is 33-nrad.

STABILITY RESULT FROM X-RAY EXPERIMENT

We have tested the first prototype artificial channel-cut crystal as an outer crystal for a 4-bounce high resolution monochromator with nested configuration at the APS

3-ID-B experimental station. As a typical case, Fig. 6 shows a two hours stability result with a 1-meV bandwidth monochromatic beam.

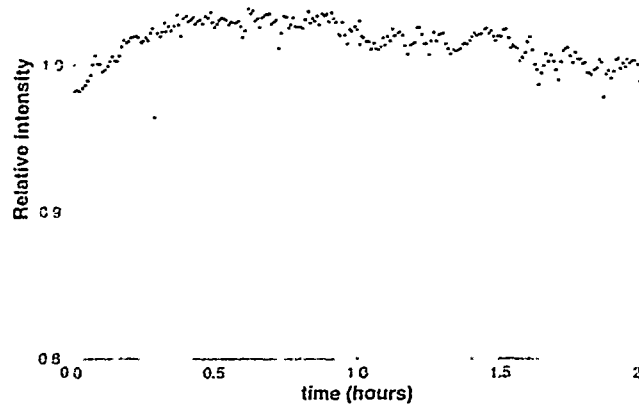


Figure 6. Srelative intensity measured by an ionization chamber after the high resolution monochromator as a function of time. The data is corrected for the decaying current in the storage ring.

SUMMARY

In the traditional channel-cut crystal design, the silicon is not only the material of choice for optics but also is the material for the base structure. The limitation of the silicon material mechanical properties and the difficulties of finishing the optical surfaces in certain geometries limited the design capability. An artificial channel-cut crystal will allow us to use the best materials for the base of the driving structures and use pre-finished crystals for optics to optimize the performance.

The benefit of an artificial channel-cut crystal lies in the reduction of the number of rotation axes of an optical setup, such as a monochromator. In certain cases, two or more crystals need to be rotated simultaneously, which is often difficult to achieve with high precision and good repeatability. By allowing independent motions of individual crystals, as described here, a great freedom in the design of the x-ray optical setup is offered.

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