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## **Advances in Spectral Nodal Methods applied to $S_N$ Nuclear Reactor Global Calculations in Cartesian Geometry**

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### ***Abstract***

Presented here are the advances in spectral nodal methods for discrete ordinates ( $S_N$ ) eigenvalue problems in Cartesian geometry. These coarse-mesh methods are based on three ingredients: (i) the use of the standard discretized spatial balance  $S_N$  equations; (ii) the use of the non-standard spectral diamond (SD) auxiliary equations in the multiplying regions of the domain, e.g. fuel assemblies; and (iii) the use of the non-standard spectral Green's function (SGF) auxiliary equations in the non-multiplying regions of the domain, e.g., the reflector. In slab-geometry the hybrid SD-SGF method generates numerical results that are completely free of spatial truncation errors. In X,Y-geometry, we obtain a system of two "slab-geometry"  $S_N$  equations for the node-edge average angular fluxes by transverse-integrating the X,Y-geometry  $S_N$  equations separately in the y- and then in the x-directions within an arbitrary node of the spatial grid set up on the domain. In this paper, we approximate the transverse leakage terms by constants. These are the only approximations considered in the SD-SGF-constant nodal method, as the source terms, that include scattering and eventually fission events, are treated exactly. Moreover, we describe in this paper the progress of the approximate  $S_N$  albedo boundary conditions for substituting the non-multiplying regions around the nuclear reactor core. We show numerical results to typical model problems to illustrate the accuracy of spectral nodal methods for coarse-mesh  $S_N$  criticality calculations.

### **1. INTRODUCTION**

Nuclear reactor criticality analysis is often best modeled by eigenvalue problems. In nuclear reactor physics, the effective multiplication factor ( $k_{\text{eff}}$  – the dominant eigenvalue) is thought of as the ratio between the numbers of neutrons generated in successive fission reactions. The eigenfunction corresponding to the dominant eigenvalue is assumed to be proportional to the neutron flux within the nuclear reactor core. Moreover, in most realistic reactor global

calculations, it is convenient to consider an approximation of the energy-dependent eigenvalue problem in which the energy variable is discretized into contiguous energy groups, giving rise to the conventional multigroup approximation [1].

We have divided this paper into two major parts. In the first part (Section 2) we describe a hybrid spectral nodal method for multigroup slab-geometry eigenvalue problems in neutron transport theory using the discrete ordinates ( $S_N$ ) formulation. We divide the slab into spatial nodes that have constant group macroscopic cross sections, and then we perform a spectral analysis of the multigroup  $S_N$  equations to obtain the general solution in each spatial node [2], for a given estimate of the dominant eigenvalue in the power iterations [3]. This coarse-mesh method is based on the use of the standard multigroup spatially discretized  $S_N$  balance equations [1] and two types of non-standard auxiliary equations that preserve the nodal general solutions. In the non-multiplying regions, e.g., the reflector, we use the multigroup spectral Green's function (SGF) auxiliary equations [4]. In the multiplying regions, e.g., the fuel assemblies, we use the multigroup spectral diamond (SD) auxiliary equations [2]. This hybrid characteristic of the multigroup SD-SGF method improves both the numerical stability and the convergence rate of the inner iterations in coarse-mesh calculations. Another positive feature of the SD-SGF method is the implementation of the multigroup albedo boundary conditions, that substitute the reflector region in nuclear reactor global calculations [5,6].

While the present multigroup SD-SGF hybrid method and the albedo boundary conditions do not directly apply to multidimensional  $S_N$  eigenvalue problems, they can be applied to improve the accuracy of conventional  $S_N$  nodal methods [7]. Therefore, in the second part of this paper (Section 3), we describe an extension of the SD-SGF method and albedo boundary conditions to criticality calculations in X,Y-geometry  $S_N$  neutron transport models. In this extension, we approximate the transverse leakage through the edges of each spatial node by constants, so we call the resulting method the SD-constant nodal (SD-CN) method, that we use in the multiplying regions of the domain. In the non-multiplying regions, we use the SGF-CN method [8]; hence the hybrid characteristic of the resulting SD-SGF-CN method. Furthermore, we extend the  $S_N$  albedo boundary conditions to X,Y-geometry  $S_N$  eigenvalue problems to illustrate the accuracy in substituting approximately non-multiplying media, e.g., the baffle-reflector system around the active domain, in criticality calculations. To conclude, in Section 4, we offer a number of concluding remarks.

## 2. THE HYBRID MULTIGROUP SD-SGF NODAL METHOD FOR SLAB-GEOMETRY

Let us consider an arbitrary spatial grid defined on a slab of height H. Now we consider the multigroup  $S_N$  equations, defined in an arbitrary node  $\Omega_j$

$$\mu_m \frac{d}{dx} \Psi_{m,g}(x) + \sigma_{Tg,j} \Psi_{m,g}(x) = \frac{1}{2} \sum_{g'=1}^G (\sigma_{Sg',g,j} + \frac{\chi_{g'}}{k_{eff}} \nu \sigma_{Fg',j}) \sum_{n=1}^N \Psi_{n,g'}(x) w_n, \quad (1)$$

$$g = 1 : G, m = 1 : N, x \in \Omega_j.$$

Here the notation is standard [1], the material parameters are constant in node  $\Omega_j$ , and  $k_{eff}$  is the dominant eigenvalue defined as the effective multiplication factor. To perform a spectral

analysis of the  $S_N$  equations (1) and determine the nodal general solution, we seek elementary solutions of the form

$$\Psi_{m,g,v}(x) = a_{m,g}(v) \exp(x/v) , \quad (2)$$

$$m = 1 : N , x \in \Omega_j , g = 1 : G .$$

By substituting ansatz (2) into Eq. (1), we follow the steps described in the work by de Abreu *et al.* [2] to obtain an expression for the nodal general solution of Eq. (1) for each estimate of the dominant eigenvalue  $k_{\text{eff}}$  in the outer iterations. This expression appears as

$$\Psi_{m,g}(x) = \sum_{\ell=1}^{G \times N} \alpha_{\ell} \Psi_{m,g,v_{\ell}}(x) = \sum_{\ell=1}^{G \times N} \alpha_{\ell} a_{m,g}(v_{\ell}) \exp(x/v_{\ell}) , \quad (3)$$

$$m = 1 : N , x \in \Omega_j , g = 1 : G ,$$

where  $\alpha_{\ell}$  are arbitrary constants.

Now we integrate the multigroup  $S_N$  equations (1) inside node  $\Omega_j$  to obtain the standard multigroup spatial balance  $S_N$  equations

$$\frac{\mu_m}{h_j} (\Psi_{m,g,j+1/2} - \Psi_{m,g,j-1/2}) + \sigma_{Tg,j} \bar{\Psi}_{m,g,j} = \frac{1}{2} \sum_{g'=1}^G \bar{\sigma}_{g',g,j}(k_{\text{eff}}) \sum_{n=1}^N \bar{\Psi}_{n,g',j} w_n , \quad (4)$$

where  $h_j$  is the width of node  $\Omega_j$ ,

$$\bar{\sigma}_{g',g,j}(k_{\text{eff}}) \equiv \sigma_{Sg',g,j} + \frac{\chi_g}{k_{\text{eff}}} v \sigma_{Fg',j} , \quad (5)$$

and

$$\bar{\Psi}_{m,g,j} \equiv \frac{1}{h_j} \int_{x_{j-1/2}}^{x_{j+1/2}} \Psi_{m,g}(x) dx . \quad (6)$$

Furthermore, we write the multigroup SGF auxiliary equations, that we use in the nodes located in the non-multiplying regions

$$\bar{\Psi}_{m,g,j} = \sum_{\mu_n > 0} \sum_{g'=1}^G \chi_{n,g' \rightarrow m,g} \Psi_{n,g',j-1/2} + \sum_{\mu_n < 0} \sum_{g'=1}^G \chi_{n,g' \rightarrow m,g} \Psi_{n,g',j+1/2} , \quad (7)$$

$$m = 1 : N , g = 1 : G .$$

In addition, we write the multigroup SD auxiliary equation, that we use in the nodes located in the multiplying regions

$$\bar{\Psi}_{m,g,j} = \frac{1}{2} \sum_{n=1}^N \sum_{g'=1}^G \xi_{n,g' \rightarrow m,g} (\Psi_{n,g',j-1/2} + \Psi_{n,g',j+1/2}), \quad (8)$$

$m = 1:N, \quad g = 1:G.$

The auxiliary equations (7) and (8) have parameters that are determined so that the nodal general solution, given by Eq. (3), is automatically preserved in the numerical algorithm. The multigroup spatial balance equations (4), the multigroup SGF auxiliary equations (7) used in the non-multiplying regions of the slab, the multigroup SD auxiliary equations (8) used in the fuel regions, all together with the appropriate boundary conditions and the continuity conditions at the node edges form the multigroup SD-SGF equations. For each estimate of the dominant eigenvalue  $k_{eff}$  in the outer iterations, we solve the multigroup SD-SGF equations iteratively (inner iterations), i.e., we employ the one-node block inversion (NBI) iterative scheme that uses the most recent estimates for the incoming node-edge angular fluxes in each energy group to calculate the multigroup exiting node-edge angular fluxes in the upwind directions. Moreover, in order to accelerate convergence of the power method used in the outer iterations, we implemented an acceleration scheme based on Tchebycheff extrapolation of the fission source [9].

As with the albedo boundary conditions, since vacuum boundary conditions usually apply on the outer boundaries of the reflector regions around the active core, the multigroup SGF auxiliary equations (7) for a single node in the reflector region of thickness  $a$  become

$$\bar{\Psi}_{m,g,R_r} = \sum_{\mu_n > 0} \sum_{g'=1}^G \chi_{n,g' \rightarrow m,g} \Psi_{n,g',R_r}^-, \quad (9)$$

$m = 1:N, \quad g = 1:G.$

Here  $R_r$  is the reflector region located on the right-hand side of the slab and  $\Psi_{n,g',R_r}^-$  is the group angular flux entering the reflector region  $R_r$  through the left edge. Substituting Eq. (9) into the spatial balance equation (4) with  $\mu_m < 0$ , we can reformulate the result as

$$\Psi_{m,g,R_r}^- = \sum_{\mu_n > 0} \sum_{g'=1}^G \Lambda_{n,g' \rightarrow m,g}^r \Psi_{n,g',R_r}^-, \quad \mu_m < 0, \quad (10)$$

where the right-hand side albedo substitutes exactly the reflector region of thickness  $a$  and is defined as

$$\Lambda_{n,g' \rightarrow m,g}^r = \frac{a}{|\mu_m|} \left[ \sum_{g''=1}^G \sigma_{Sg'',g} T_{n,g' \rightarrow g''} - \sigma_{Tg} \chi_{n,g' \rightarrow m,g} \right], \quad (11a)$$

where

$$T_{n,g' \rightarrow g''} = \frac{1}{2} \sum_{\ell=1}^N \chi_{n,g' \rightarrow \ell, g''} w_\ell. \quad (11b)$$

We proceed similarly for the reflector region  $R_\ell$  located on the left-hand side of the slab. The extension of this procedure to determine the multigroup  $S_N$  albedo for multilayer non-multiplying regions, e.g., baffle and reflector, is straightforward and is carefully described in Ref. [6].

Now we consider the two-group model problem No. 1 described in Ref. [2]. The numerical results listed in Table I show that the SD-SGF method is completely free from spatial truncation errors. That is, the dominant numerical results generated by the hybrid SD-SGF method do not change as the spatial grid coarsens. This is in contrast to the DD method that generates meaningless results for some coarse-mesh calculations. Moreover, to converge this problem, the number of transport sweeps required by the SD-SGF method with the power iterative scheme in the outer iterations was more than three times greater than the number of transport sweeps required by the SD-SGF method with the Tchebycheff acceleration scheme.

**Table I. Numerical results for model problem No. 1**

Number of nodes per region	Numerical method	Energy group	Group scalar fluxes ( $\text{cm}^{-2} \cdot \text{s}^{-1}$ )		
			x = 4.0 cm	x = 186.87 cm	x = 369.75 cm
128	DD	1	0.71098E+15 <sup>a</sup>	0.28703E+17	0.17349E+17
		2	0.32711E+15	0.53773E+16	0.10756E+17
	SD - SGF	1	0.71098E+15	0.28703E+17	0.17349E+17
		2	0.32711E+15	0.53773E+16	0.10756E+17
2	DD	1	0.69653E+15	0.28149E+17	0.17516E+17
		2	0.47886E+15	0.66757E+16	0.10268E+17
	SD - SGF	1	0.71098E+15	0.28703E+17	0.17349E+17
		2	0.32711E+15	0.53772E+16	0.10756E+17
1	DD	1	-0.23662E+15	0.29278E+17	0.18480E+17
		2	0.18379E+16	0.87456E+16	0.13296E+17
	SD - SGF	1	0.71098E+15	0.28703E+17	0.17349E+17
		2	0.32711E+15	0.53772E+16	0.10756E+17

<sup>a</sup> Should be read as  $0.71098 \times 10^{15}$

The effective multiplication factor generated by the SD-SGF method for this model problem was  $k_{\text{eff}} = 1.049697$  regardless of the spatial grid. However, the effective multiplication factor generated by the DD method was sensitive to the spatial grid, even though the maximum relative deviation was only equal to -0.11% for the coarsest grid. One reason for this small relative deviation is that the effective multiplication factor is a volume-integrated quantity; therefore, the effect of the spatial truncation error may be alleviated by cancellation of errors. On the other

hand, since the group scalar fluxes, listed in Table I, are local quantities, the numerical values generated by the DD method are extremely sensitive to the spatial grid, to the point that the DD method generates meaningless negative results for the coarsest grid.

### 3. THE HYBRID SD-SGF-CN METHOD FOR X,Y-GEOMETRY

Let us consider an arbitrary rectangular spatial grid defined on a two-dimensional rectangular domain of width X and height Y. Now we consider the one-speed S<sub>N</sub> equations defined in a arbitrary node Ω<sub>i,j</sub>

$$\mu_m \frac{\partial}{\partial x} \Psi_m(x, y) + \eta_m \frac{\partial}{\partial y} \Psi_m(x, y) + \sigma_{Ti,j} \Psi_m(x, y) = \left( \sigma_{Si,j} + \frac{v}{k_{eff}} \sigma_{Fi,j} \right) \sum_{n=1}^N \Psi_n(x, y) w_n, \quad (12)$$

$m = 1 : M, \quad M = N(N+2)/2, \quad (x, y) \in \Omega_{i,j}.$

Here the notation is standard [1] and the material parameters are constant in node Ω<sub>i,j</sub>. By transverse-integrating Eq. (12) in the y-direction inside node Ω<sub>i,j</sub>, we obtain the one-dimensional transverse-integrated S<sub>N</sub> nodal equation for the x-direction

$$\mu_m \frac{d}{dx} \tilde{\Psi}_{m,j}(x) + \sigma_{Ti,j} \tilde{\Psi}_{m,j}(x) = \left( \sigma_{Si,j} + \frac{v}{k_{eff}} \sigma_{Fi,j} \right) \sum_{n=1}^N \tilde{\Psi}_{n,j}(x) w_n - \frac{\eta_m}{k_j} [\Psi_m(x, y_{j+1/2}) - \Psi_m(x, y_{j-1/2})], \quad (13)$$

where k<sub>j</sub> is the height of node Ω<sub>i,j</sub> and

$$\tilde{\Psi}_{m,j}(x) \equiv \frac{1}{k_j} \int_{y_{j-1/2}}^{y_{j+1/2}} \Psi_m(x, y) dy. \quad (14)$$

By transverse-integrating Eq. (12) in the x-direction inside node Ω<sub>i,j</sub> we obtain the one-dimensional transverse-integrated S<sub>N</sub> nodal equation for the y-direction, similar to Eq. (13). Furthermore, we consider constant approximation for the transverse leakage term in Eq. (13); that is,

$$\frac{\eta_m}{k_j} [\Psi_m(x, y_{j+1/2}) - \Psi_m(x, y_{j-1/2})] \cong \frac{\eta_m}{k_j} (\hat{\Psi}_{m,i,j+1/2} - \hat{\Psi}_{m,i,j-1/2}), \quad (15)$$

where we have defined

$$\hat{\Psi}_{m,i,j\pm 1/2} \equiv \frac{1}{h_i} \int_{x_{i-1/2}}^{x_{i+1/2}} \Psi_m(x, y_{j\pm 1/2}) dx, \quad (16)$$

with  $h_i$  being the width of node  $\Omega_{i,j}$ . By substituting the constant approximation (15) into Eq. (13), we obtain the transverse-integrated  $S_N$  constant nodal equations for the x-direction. Similar procedure leads to the transverse-integrated  $S_N$  constant nodal equations for the y direction. The general solutions of the transverse-integrated  $S_N$  constant nodal equations are given by

$$\tilde{\Psi}_{m,j}(x) = \tilde{\Psi}_{m,j}^p + \tilde{\Psi}_{m,j}^h(x) \quad \text{and} \quad \hat{\Psi}_{m,i}(y) = \hat{\Psi}_{m,i}^p + \hat{\Psi}_{m,i}^h(y) \quad , \quad (x, y) \in \Omega_{i,j} \quad , \quad (17)$$

where the superscript p indicates the particular solution that in either case is independent of space, because of the constant approximation considered. The superscript h indicates the homogeneous components of the solutions, which satisfy the homogeneous equations associated with the transverse-integrated  $S_N$  constant nodal equations. We determine the homogeneous solutions by performing spectral analyses that are carefully described in Ref. [10]. For the x-direction we obtain

$$\tilde{\Psi}_{m,j}^h(x) = \sum_{\ell=1}^M \alpha_{\ell} a_m(v_{\ell}) \exp(x/v_{\ell}) \quad , \quad (18)$$

$$m = 1 : M \quad , \quad x \in \Omega_{i,j} \quad ,$$

where  $\alpha_{\ell}$  are arbitrary constants. We obtain a similar expression for the y-direction. Furthermore, we integrate the  $S_N$  equations (12) inside node  $\Omega_{i,j}$  to obtain the conventional discretized spatial balance  $S_N$  equations

$$\frac{\mu_m}{h_i} (\tilde{\Psi}_{m,i+1/2,j} - \tilde{\Psi}_{m,i-1/2,j}) + \frac{\eta_m}{k_j} (\hat{\Psi}_{m,i,j+1/2} - \hat{\Psi}_{m,i,j-1/2}) + \sigma_{Ti,j} \bar{\Psi}_{m,i,j} = \sigma_{i,j}(k_{\text{eff}}) \sum_{n=1}^M \bar{\Psi}_{n,i,j} w_n \quad , \quad (19)$$

$$m = 1 : M \quad ,$$

where we have defined

$$\sigma_{i,j}(k_{\text{eff}}) \equiv \sigma_{Si,j} + \frac{v}{k_{\text{eff}}} \sigma_{Fi,j} \quad (20)$$

and the node-average angular flux

$$\bar{\Psi}_{m,i,j} \equiv \frac{1}{h_i k_j} \int_{x_{i-1/2}}^{x_{i+1/2}} \int_{y_{j-1/2}}^{y_{j+1/2}} \Psi_m(x, y) dx dy \quad . \quad (21)$$

Now, we consider the SGF auxiliary equations, that we use in the nodes located in the non-multiplying regions

$$\bar{\Psi}_{m,i,j} = \sum_{\mu_n > 0} \theta_{m,n} \tilde{\Psi}_{n,i-1/2,j} + \sum_{\mu_n < 0} \theta_{m,n} \tilde{\Psi}_{n,i+1/2,j} + \hat{G}_{m,i,j} \quad (22a)$$

$$m = 1 : M \quad ,$$

and

$$\bar{\Psi}_{m,i,j} = \sum_{\eta_n > 0} \gamma_{m,n} \hat{\Psi}_{n,i,j-1/2} + \sum_{\eta_n < 0} \gamma_{m,n} \hat{\Psi}_{n,i,j+1/2} + \tilde{G}_{m,i,j} \quad (22b)$$

$m = 1 : M .$

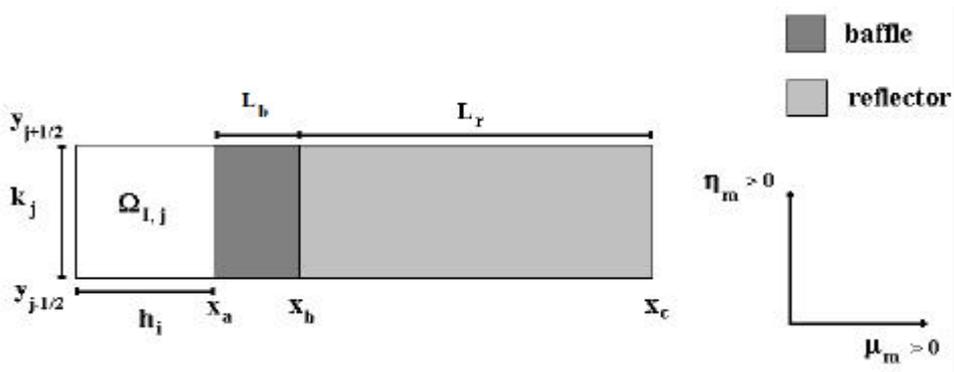
In addition, we write the SD auxiliary equations, that we use in the nodes located in the fuel regions

$$\bar{\Psi}_{m,i,j} = \frac{1}{2} \sum_{n=1}^M \theta_{m,n} (\tilde{\Psi}_{n,i-1/2,j} + \tilde{\Psi}_{n,i+1/2,j}) + \hat{G}_{m,i,j} \quad (23a)$$

and

$$\bar{\Psi}_{m,i,j} = \frac{1}{2} \sum_{n=1}^M \gamma_{m,n} (\hat{\Psi}_{n,i,j-1/2} + \hat{\Psi}_{n,i,j+1/2}) + \tilde{G}_{m,i,j} , m = 1 : M. \quad (23b)$$

The auxiliary equations (22a-b) and (23a-b) have parameters that are determined so that the nodal general solutions of the transverse-integrated  $S_N$  constant nodal equations, given by Eq. (17), are automatically preserved in the numerical algorithm. The spatial balance equations (19), the SGF auxiliary equations (22a-b, used in the non-multiplying regions), the SD auxiliary equations (23a-b, used in the fuel regions), all together with the appropriate boundary conditions and the continuity conditions at the node edges form the SD-SGF-constant nodal (CN) equations. For each estimate of the dominant eigenvalue  $k_{eff}$  in the outer iterations, we solve the SD-SGF-CN equations iteratively (inner iterations) with the NBI iterative scheme [10].



**Figure 1. Albedo for two non-multiplying regions.**

As with the approximate  $S_N$  two-region albedo boundary conditions, we neglect the transverse leakage terms in the non-multiplying regions around the core, i.e., baffle and reflector. In other words, in deriving the two-region  $S_N$  albedo matrix, we transverse-integrate the one-speed  $S_N$  equations in X,Y geometry inside the baffle-reflector system contiguous to the active boundary

cell of the spatial grid set up on the domain. That is, for the  $x$  direction, we integrate the  $S_N$  equations inside the baffle-reflector system in the  $y$  direction, neglect the transverse leakage terms and solve the resulting homogeneous “one-dimensional” transverse-integrated  $S_N$  nodal equations in the  $x$  direction analytically by performing a spectral analysis [10]. The procedure follows two major steps: (i) the use of the familiar discretized spatial balance  $S_N$  equations [1], with neglect of the leakage terms in the  $y$  direction, and (ii) the use of the spectral Green’s function (SGF) auxiliary equations, that have parameters to preserve the analytical general solution of the homogeneous “one-dimensional” transverse integrated  $S_N$  nodal equations in the  $x$  direction, i.e.,  $\hat{G}_{m,i,j} \equiv 0$  in Eq. (22a). The procedure for the  $y$  direction follows similar steps. Therefore, by substituting the SGF auxiliary equations into the discretized spatial balance  $S_N$  equations, we can relate the neutron angular fluxes backscattered into the active cell to the neutron angular fluxes entering the baffle from the active cell, since vacuum boundary conditions apply on the outer boundaries of the reflector regions, viz Figure 1 for the  $x$  direction.

We remark that the only approximation that we consider in the derivation of the  $S_N$  albedo matrices for  $S_N$  eigenvalue problems in  $X,Y$  geometry is the neglect of the transverse leakage terms. Therefore, should this approximation introduce no significant errors, we expect the use of the present two-region albedo boundary conditions to improve the efficiency of  $S_N$  codes for criticality calculations, by analyzing the accuracy of the numerical results versus the CPU time of each run.

At this point we show numerical results to test problem No. 2 that we model using the level symmetric  $S_4$  angular quadrature set [1]. This model problem consists of a heterogeneous critical system, composed of four different material zones, viz Figure 2, whose material data are listed in Table II [11].

Table III displays the numerical results generated for the effective multiplication factor ( $k_{eff}$ ) by the hybrid SD-SGF-CN method [12] on various spatial grids with (i) explicit baffle-reflector system; (ii) explicit baffle and albedo for the reflector (SD-SGF-CN<sub>alb1R</sub>); and (iii) two-region albedo boundary conditions (SD-SGF-CN<sub>alb2R</sub>). As we see, the use of albedo boundary conditions does not increase significantly the relative deviations with respect to the fine-grid results generated by the conventional DD method with explicit baffle-reflector system. In addition, the CPU execution time for the albedo calculations also decreased with respect to the explicit baffle-reflector system calculations. Based on the results that we show in Table III for this critical model problem, we conclude that without increasing too much the relative deviations of the numerical results generated by the SD-SGF-CN method for the eigenvalue  $k_{eff}$  with respect to the reference DD result, the one-region albedo calculations reduced the execution time by 27 % for the  $\Gamma_3$  run up to 47 % for the  $\Gamma_7$  run. On the other hand, the two region albedo calculations reduced the execution time by 31 % for the  $\Gamma_3$  run up to 74 % for the  $\Gamma_7$  run. This means a gain in efficiency in the sense we have described in section 1. Moreover, Table III also lists the results generated for the eigenvalue  $k_{eff}$  by the fine-mesh DD method ( $\Gamma_8$  run) with one- and two-region albedo boundary conditions. We note that the use of one-region albedo boundary conditions reduced the execution time by 64 %, whereas the use of two-region albedo boundary conditions reduced the execution time by 83 % for the  $\Gamma_8$  DD run. We remark that the albedo DD runs generated relative deviations, which are comparable to the ones generated by

SD-SGF-CN method with albedo boundary conditions on a spatial grid composed of 16 nodes per region in each spatial direction ( $\Gamma_6$  run, 141.7 seconds and 72.55 seconds) [13].

Supposing that the power density generated by the entire domain is 1 Watt/cm<sup>3</sup>, Figure 3 shows the power density distribution as generated by six independent runs with explicit two non-multiplying region calculations, one-region albedo and two-region albedo calculations, using both the coarse-mesh SD-SGF-CN method on the  $\Gamma_4$  spatial grid, and the fine-mesh DD method on the  $\Gamma_8$  spatial grid. At this point we remark the following *corrigendum* to the statement: “As we see in Figure 4, although the relative deviations for this numerical experiment are still acceptable for practical applications, we remark that the two-region albedo calculations, generate less accurate results for the boundary regions, mainly for the corner regions, that have two sides interfacing the baffle-moderator system”, appearing in section 3 of Ref. [13]. This statement, as we see now in Figure 4, is not correct, and this unjustified conclusion was due to an error in our computational code.

**Table II. Material Data for Model Problem No. 2.**

Zone Number	$s_T$ (cm <sup>-1</sup> )	$s_S$ (cm <sup>-1</sup> )	$n_S F$ (cm <sup>-1</sup> )
<b>1 (Pu – 239)</b>	3.26400E-1 <sup>a</sup>	2.25216E-1	0.11491E+0
<b>2 (Pu - 239)</b>	3.26400E-1	2.25216E-1	0.10072E+0
<b>3 (baffle)</b>	3.30600E-2	7.39000E-3	0.0
<b>4 (reflector)</b>	3.26400E-1	2.93760E-1	0.0

<sup>a</sup>Read as 2.22589 x 10<sup>-1</sup>.



**Table III. Numerical Results for Model Problem No. 2.**

Spatial Grid $G_n^a$	Numerical Method	Dominant Eigenvalue ( $k_{eff}$ )	Relative Deviation (%) <sup>h</sup>	CPU time <sup>i</sup> (seconds)	CPU time reduction (%)
$G_3$	SD-SGF-CN <sup>b</sup>	0.99698	0.15	14.870	27
	SD-SGF-CN <sub>alb1R</sub> <sup>c</sup>	0.99719	0.17	10.810	
	SD-SGF-CN <sub>alb2R</sub> <sup>d</sup>	0.99802	0.25	10.230	
$G_4$	SD-SGF-CN	0.99598	0.05	24.640	28
	SD-SGF-CN <sub>alb1R</sub>	0.99631	0.08	17.800	
	SD-SGF-CN <sub>alb2R</sub>	0.99714	0.17	14.230	
$G_5$	SD-SGF-CN	0.99564	0.01	69.660	38
	SD-SGF-CN <sub>alb1R</sub>	0.99606	0.06	42.990	
	SD-SGF-CN <sub>alb2R</sub>	0.99689	0.14	25.820	
$G_6$	SD-SGF-CN	0.99554	0.0	249.020	43
	SD-SGF-CN <sub>alb1R</sub>	0.99600	0.05	141.700	
	SD-SGF-CN <sub>alb2R</sub>	0.99683	0.13	72.550	
$G_7$	SD-SGF-CN	0.99551	0.0	988.740	47
	SD-SGF-CN <sub>alb1R</sub>	0.99598	0.05	536.210	
	SD-SGF-CN <sub>alb2R</sub>	0.99681	0.13	257.790	
$G_8$	DD-CBI <sup>e</sup>	0.99550		5654.720	64
	DD <sub>alb1R</sub> <sup>f</sup>	0.99560	0.05	2062.860	
	DD <sub>alb2R</sub> <sup>g</sup>	0.99680	0.13	946.870	

a  $2^n / 4$  spatial nodes per region in each spatial direction.

b *Spectral diamond-spectral Green's function-constant nodal* method with explicit reflector and baffle.

c *Spectral diamond-spectral Green's function-constant nodal* method with albedo boundary conditions for one non-multiplying region.

d *Spectral diamond-spectral Green's function-constant nodal* method with albedo boundary conditions for two non-multiplying regions.

e *Diamond difference* method with explicit reflector and baffle (reference result).

f *Diamond difference* method with albedo boundary conditions for one non-multiplying region.

g *Diamond difference* method with albedo boundary conditions for two non-multiplying regions.

h Relative deviation with respect to the DD fine-mesh solution.

i On a Pentium III 850 MHz PC.

***** 4.8917E-2 ***** 4.8550E-2 ***** 4.8423E-2 ***** 4.8494E-2 ***** 4.8675E-2 ***** 4.9040E-2	***** 2.5090E-2 ***** 2.5190E-2 ***** 2.5138E-2 ***** 2.5122E-2 ***** 2.5167E-2 ***** 2.5079 E-2		
***** 0.1271E+0 ***** 0.1277E+0 ***** 0.1280E+0 ***** 0.1279E+0 ***** 0.1275E+0 ***** 0.1268E+0	***** 4.8917E-2 ***** 4.8550E-2 ***** 4.8423E-2 ***** 4.8494E-2 ***** 4.8675E-2 ***** 4.9040E-2		

- \*\*\*\*\* SD-SGF-CN results with albedo boundary conditions for two non-multiplying regions and  $\Gamma_4$  spatial grid.
- \*\*\*\*\* SD-SGF-CN results with albedo boundary conditions for one non-multiplying region and  $\Gamma_4$  spatial grid.
- \*\*\*\*\* SD-SGF-CN results with explicit reflector and baffle and  $\Gamma_4$  spatial grid.
- \*\*\*\* *Diamond difference* results with explicit reflector and baffle and  $\Gamma_8$  spatial grid
- \*\*\* *Diamond difference* results with albedo boundary conditions for one non-multiplying regions and  $\Gamma_8$  spatial grid.
- \*\* *Diamond difference* results with albedo boundary conditions for two non-multiplying regions and  $\Gamma_8$  spatial grid.
- \* *Diamond difference* results with albedo boundary conditions for two non-multiplying regions and  $\Gamma_8$  spatial grid.

**Figure 3. Power Density Distribution for Model Problem No. 2.**

<p>***** 0.87            ***** 0.11            *** 0.15            ** 0.37            * 1.12</p>	<p>***** 0.01            ***** 0.26            *** 0.06            ** 0.18            * 0.17</p>		
<p>***** 0.64            ***** 0.13            *** 0.09            ** 0.0            * 0.82</p>	<p>***** 0.87            ***** 0.11            *** 0.15            ** 0.37            * 1.12</p>		

- \*\*\*\*\* SD-SGF-CN results with albedo boundary conditions for two non-multiplying regions and  $\Gamma_4$  spatial grid.
- \*\*\*\*\* SD-SGF-CN results with albedo boundary conditions for one non-multiplying region and  $\Gamma_4$  spatial grid.
- \*\*\* SD\_SGF-CN results with explicit reflector and baffle and  $\Gamma_4$  spatial grid
- \*\* *Diamond difference* results with albedo boundary conditions for one non-multiplying regions and  $\Gamma_8$  spatial grid.
- \* *Diamond difference* results with albedo boundary conditions for two non-multiplying regions and  $\Gamma_8$  spatial grid.

**Figure 4. Relative Deviation (%) for the Power Density Distribution**

#### 4. CONCLUDING REMARKS

We have described in this paper the advances on spectral nodal methods applied to  $S_N$  eigenvalue problems in Cartesian geometry.

In slab geometry, the multigroup hybrid SD-SGF method generated dominant numerical solutions to multigroup  $S_N$  eigenvalue problems that were absolutely free from spatial truncation errors. The multigroup  $S_N$  albedo boundary conditions are "exact" in the sense that no further approximations are introduced in deriving them. Moreover, the Tchebycheff acceleration scheme for the convergence of the dominant numerical solution was very efficient as the number of transport sweeps was reduced by a factor of three in model problem No. 1.

In X,Y-geometry the SD-SGF-CN method is very accurate for monoenergetic  $S_N$  eigenvalue problems. The approximate one- and two-region  $S_N$  albedo boundary conditions for criticality calculations substituted very accurately the non-multiplying regions around core. Moreover, without losing too much accuracy, the use of albedo boundary conditions reduced significantly the CPU execution time of each run. This is particularly noticeable for fine-grid calculations. We remark that the  $S_N$  albedo boundary conditions, as described in this paper, can be implemented in various conventional numerical methods for one-speed X,Y-geometry  $S_N$  criticality calculations, such as the DD method, the step-characteristic method and the discontinuous finite element methods.

For practical applications in nuclear reactor global calculations we intend to work on the multigroup approximate  $S_N$  albedo boundary conditions that are of great interest to account for the neutron energy change in nuclear interactions.

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