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Implementation Guidelines for Seismic PSA

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Objectives


- Develop a ("how to do") document called Implementation Guidelines for S-PSA, observing IAEA NS-G-2.13 and ASME/ANS standard RA-Sa-2009 technical requirements for capability category 2.
- Maintain compatibility with Internal Events PSA aimed to integrate all internal and external events in one PSA model
- Incorporate recent enhancements that will contribute to meet capability category 2 technical requirements



General Structure of the IAEA Technical Document

The Implementation Guidelines for S-PSA addresses the main tasks of the S-PSA using the following structure for each task:


- Objective and scope of the task
- Applicable Technical Requirements
- Input data
- Description of the task work/process
- Results of the task (outcome)
- Interface with other tasks



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Workflow process for developing S-PSA


- The main steps and workflow process for developing the S-PSA illustrative examples:
 - Define the scope of the S-PSA and Initial assumptions
 - Observe the ASME, Standard RA-S-2009 Requirements
 - Review the Internal Event PSA (generic mode available)
 - Review the PSHA results
 - Review internal IE for seismic considerations and establish the link between Seismic Hazard impact for different acceleration ranges and Internal IEs
 - Develop Seismic Initiating Events (S-IE) and calculate S-IE frequencies
 - Develop S-IE – versus Fault trees matrix



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Workflow process for developing S-PSA

- Develop Seismic Equipment List (SEL):
 - Observe Applicable Technical Requirements (e.g. ASME, Standard RA-Sa-2009)
 - Set criteria for screening and grouping of the internal PSA Basic Events (BE)
 - Review the Internal PSA BE list
 - Set Seismic BE boundary conditions
 - Develop seismic screening criteria and screening limits, based on the applicable seismic hazard curve(s).
 - Perform SEL Screening (conduct Screening Walkdowns)



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Workflow process for developing S-PSA

- Develop Seismic Fragility parameters for Seismic Basic Events (SEL):
 - Observe applicable technical requirements (e.g. ASME, Standard RA-Sa-2009)
 - Review Seismic Qualification and Design information
 - Review applicable generic seismic capacity data
 - Conduct Seismic Capability Walkdowns
 - Perform Fragility Analysis and derive seismic fragility parameters (A_m , HCLPF, β_c)
 - Consider Correlations between seismic induced failures



Workflow process for developing S-PSA

- System Analysis:
 - Observe applicable requirements (e.g. ASME, Standard RA-Sa-2009)
 - Edit/develop Event Trees (ET):
 - Add seismic ETs and associated S-IE frequencies
 - Edit/develop Fault Trees (FT)
 - Add Seismic Basic Events and associates properties
 - Evaluate and include Human Errors associated to recovery actions



Workflow process for developing S-PSA


- Seismic Quantification:
 - Run the model for all Seismic IEs
 - The plant damage state frequency is obtained by Boolean summation of frequencies of all seismic sequences.
 - First quantification is based on preliminary fragility parameters
 - Identify significant seismic contributors



$$P_r(DS) = 1 - \prod (1 - P_r(C_i))$$

Workflow process for developing S-PSA

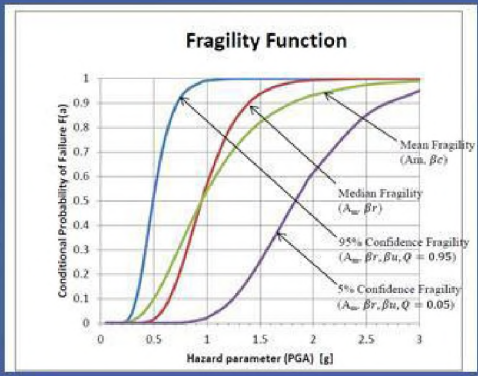
- Develop Final S-PSA Results
 - Refine Fragility Analysis for the major contributors
 - Perform quantification including refined fragilities
 - Perform sensitivity analysis and develop seismic insights.
 - Document the S-PRA




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Fragility Analysis

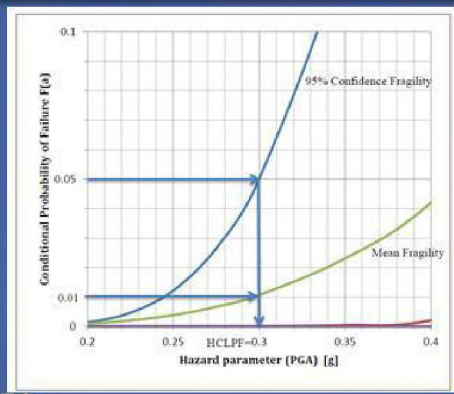





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Fragility Analysis





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Recent Enhancements

- Recover β_r and β_u from the mean plant state fragility based on the properties of the log-normal distribution and definition of the HCLPF:

$$A = 2 \quad B = \frac{\ln\left(\frac{HCLPF}{A_m}\right)}{\phi^{-1}(0.05)} \quad C = \left(\frac{\ln\left(\frac{HCLPF}{A_m}\right)}{\phi^{-1}(0.05)}\right)^2 - \beta_c^2$$

$$\beta_r = \frac{-2B + \sqrt{B^2 - 4AC}}{2A}$$

$$\beta_u = \frac{-2B - \sqrt{B^2 - 4AC}}{2A}$$



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System Analysis / S-PSA Database

Component	Building	Elevation	Internal Event	Open Description	PSA Desc	Seismic Int	Seismic BE	Fragility	SEL ID	Comments
Tag ID	Room #	12.5	SCB-SCCP	Start Of Emergency Control	Fail to Drop	SI	SI-SCB-SCCP	134.04	1	FRG #1
Tag ID	Room #	12.5	SCB-SCCP	Start Of Emergency Control	Fail to Drop	SI	SI-SCB-SCCP	137.04	1	FRG #1
Tag ID	Room #	12.5	SCB-SCCP	Start Of Emergency Control	Fail to Drop	SI	SI-SCB-SCCP	140.04	1	FRG #1
Tag ID	Room #	12.5	SCB-SCCP	Start Of Emergency Control	Fail to Drop	SI	SI-SCB-SCCP	138.02	1	FRG #1
Tag ID	Room #	12.5	SCB-SCCP	Start Of Emergency Control	Fail to Drop	SI	SI-SCB-SCCP	140.02	1	FRG #1



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System Analysis / S-PSA Database

Structure	Component	Structure Desc	Seismic Int	Structure BE	Fragility	SEL ID	Comments
TB-U1	Bas-1	Masonry Wall #W1	S11	S1BW-1	5.00E-03	127	FRG#10
TB-U1	Bas-1		S12	S2BW-1	2.15E-02	127	FRG#10
TB-U1	Bas-1		S13	S3BW-1	1.23E-01	127	FRG#10
TB-U1	Bas-1		S14	S4BW-1	0.75	127	FRG#10
TB-U1	Bas-1		S15	S5BW-1	3	127	FRG#10



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System Analysis / S-PSA Database

Seismic Correlation BE	Seismic IE	Components	Seismic Correlation Description	Fragility	Comments
S1PUMP_ABC	S11	Pumps ABC	Seismic Induced Failure Pumps A,B & C	5.00E-05	Frag #21
S1PUMP_ABC	S12	Pumps ABC	Seismic Induced Failure Pumps A,B & C	2.12E-04	Frag #22
S1PUMP_ABC	S13	Pumps ABC	Seismic Induced Failure Pumps A,B & C	1.27E-03	Frag #23
S1PUMP_ABC	S14	Pumps ABC	Seismic Induced Failure Pumps A,B & C	3.56E-02	Frag #24
S1PUMP_ABC	S15	Pumps ABC	Seismic Induced Failure Pumps A,B & C	1.20E-01	Frag #25

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Recent Enhancements

- Quantification

$$P_F = \int_{a_1}^{a_2} \frac{dH(a)}{da} F(a) da$$

$$P_F = \sum (F(a_{1i}) \times da) \times \frac{H_{int}(a) - H(a)}{da}$$

Risk/PP	Earthquake Fragility Parameters			Item	Acceleration range						PP
	β	μ	σ_a		0.05-0.2	0.2-0.4	0.4-0.6	0.6-1.0	1.0-1.5	1.5-2.2	
0.8	0.6	1.21	Average	0.125	0.9	0.5	0.8	1.25	1.85		
			MAD(MAD)	0.100	9.00E-4	7.40E-5	2.10E-5	1.70E-6	7.20E-7		
			Fit average	7.54E-5	9.90E-9	6.98E-2	2.40E-3	3.19E-1	7.59E-3		
			σ_a frag	1.25E-4	8.22E-3	1.19E-1	4.79E-2	8.10E-1	9.12E-3		
			Approx. Integ.	7.54E-6	8.31E-6	5.15E-6	5.11E-6	1.92E-6	5.46E-7	2.92E-5	
			Num. Integ.	8.00E-7	8.10E-6	4.40E-6	4.50E-6	1.60E-6	5.10E-7	1.71E-5	

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Final Remarks

- The IAEA/ISSC Implementation Guidelines for S-PSA (under development) provides "how to do" guidelines aimed to show the development process for the S-PSA illustrated with various results produced by a generic S-PSA model observing IAEA NS-G-2.13 and ASME/ANS standard technical requirements for capability category 2.
- Practical S-PSA enhancements allow integration of S-PSA with Internal Events PSA model. The authors believes that these enhancements makes S-PSA process very effective and significantly contribute meeting the capability category II requirements of the standard.

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Final Remarks

Traditional "Deterministic" safety analysis approach is characterized by:

- Un-quantified probabilities associated to hazard assessment and potential induced accidents
- Defense in Depth and Safety Margins introduced by design rules (not explicitly quantified)
- Incomplete

Risk based approaches methodologies are characterized by:

- Quantified Probabilities
- Hundreds thousands or millions of accident sequences are considered
- Realistic
- Incomplete

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Final Remarks

There are advantages and disadvantages to both deterministic and probabilistic safety assessment methodologies. These methodologies are complementary:

- first (deterministic approach) is based on the success path approach aimed to prevent occurrence of an accident;
- second (probabilistic approach) consider a large number of combinations of failures and accident sequences that may lead to a accident.
- and together (deterministic complemented by probabilistic safety assessment) seems to provide the best basis for safety and licensing decisions establishing an appropriately balances between defense in depth and risk considerations.
- This risk-informed approach uses the combination of traditional deterministic and risk-based approaches.

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